

**Supplementary Information for:**

**Two-ply Channels for Faster Wicking in Paper-based Microfluidic Devices**

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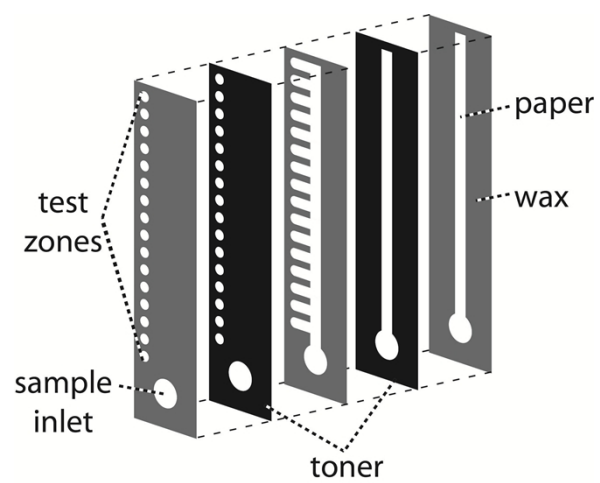
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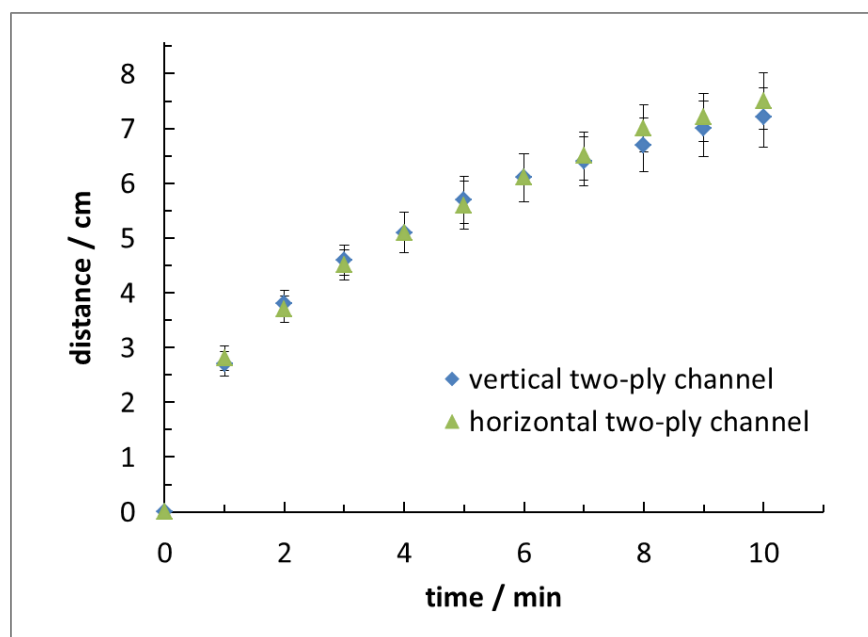
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**Figure S1**



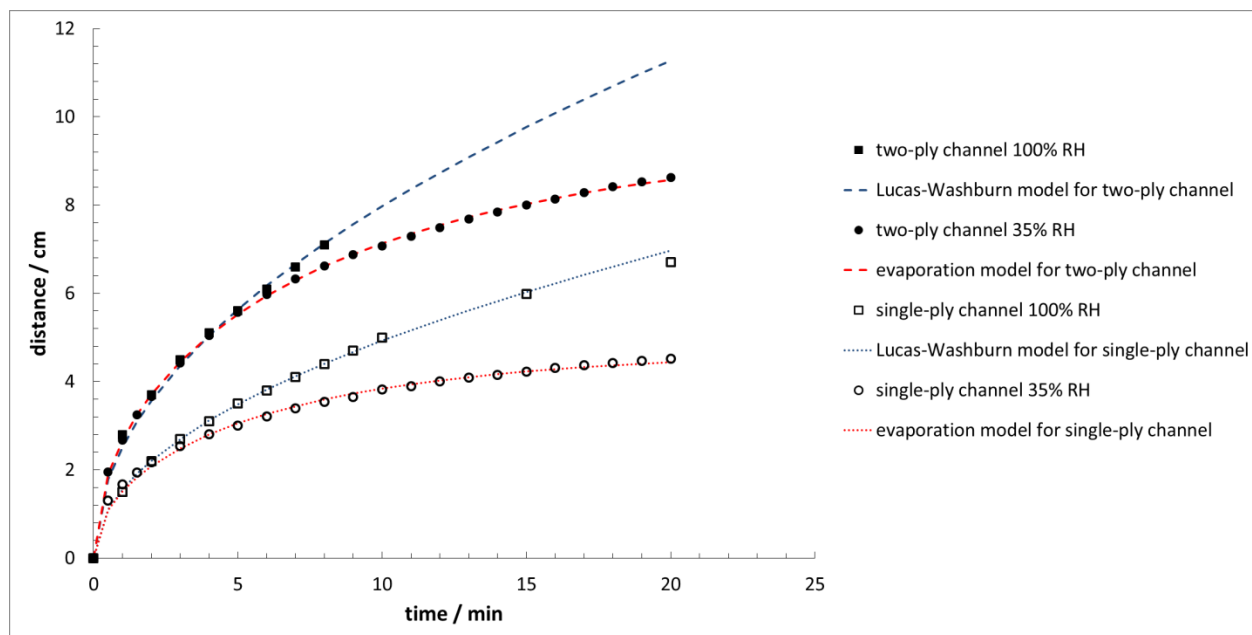
**Figure S1.** Schematic representation of the layers of patterned paper and toner used to fabricate the titration device.

**Figure S2**



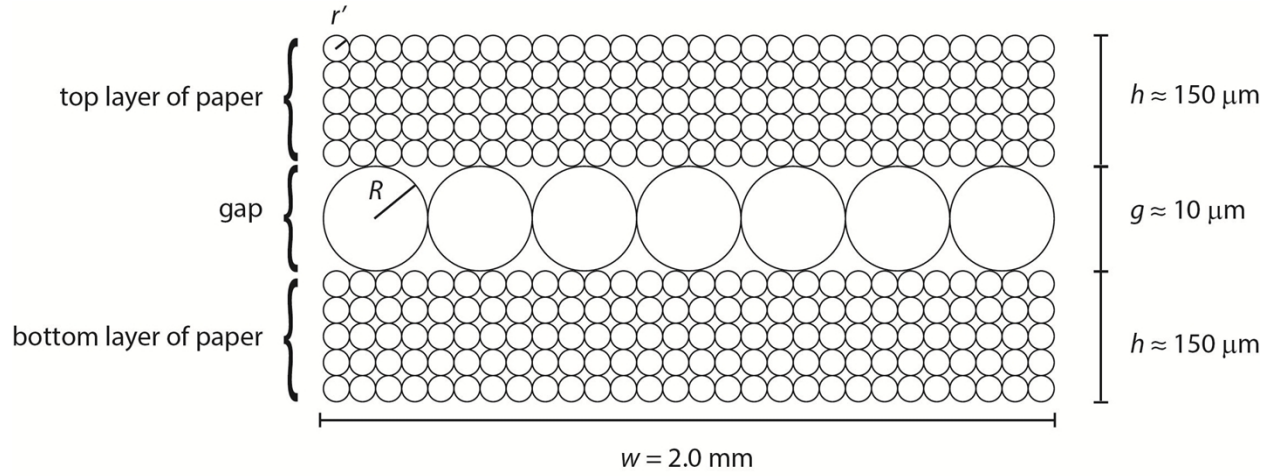
**Figure S2.** Plot of distance wicked by the fluid versus time for two-ply channels that were held either vertically or horizontally as they wicked liquid from a reservoir. Data points represent the mean of nine measurements and the error bars represent one standard deviation from the mean.

**Figure S3**



**Figure S3.** Plot of distance wicked by the fluid versus time for single-ply and two-ply channels under 100% and 35% RH. Data points represent the mean of 9 measurements and error bars were omitted for clarity, but can be seen in Figure 2. The dashed lines represent the modeled results using the magnitudes for  $r$  and  $q_0$  in Table 1.

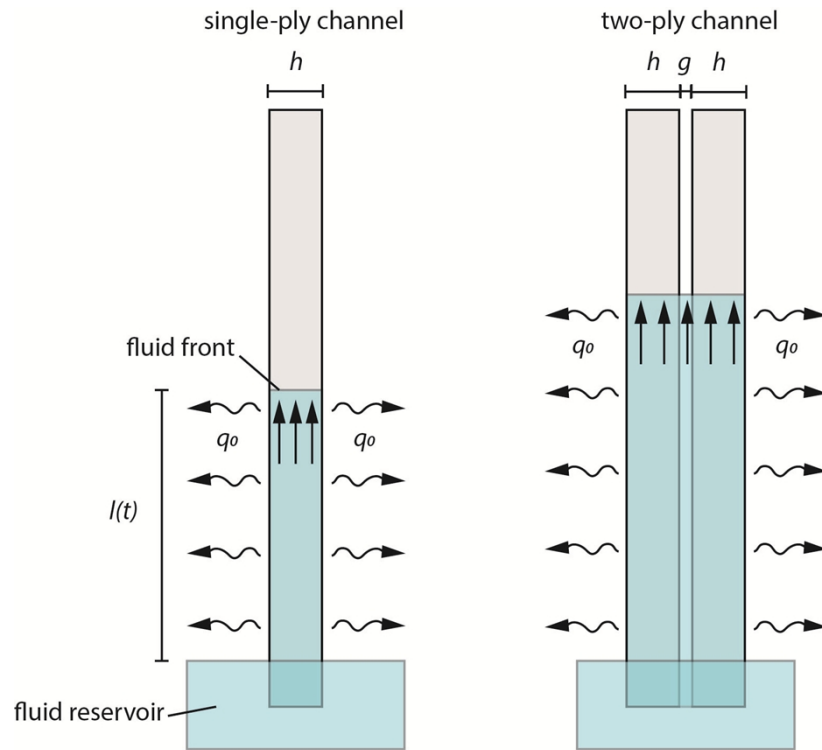
**Figure S4**



For a two-ply channel:  $r = \frac{2r'(hw) + R(gw)}{2hw + gw}$ , and  $R = g/2$

**Figure S4.** Schematic diagram of the cross-section of a two-ply channel modelling the two layers of paper as bundles of uniform capillaries of radius  $r'$  and the gap between the layers of paper as a layer of capillaries of radius  $R$ . The effective pore radius for the two-ply channel  $r$  can be estimated by calculating the cross-sectional-surface-area-weighted average of the capillary radii in each layer of paper and in the gap.

**Figure S5**



**Figure S5.** Schematic of a longitudinal section of single-ply and two-ply channels wicking liquid from a reservoir.

**Derivation of an equation to describe wicking in a paper-based porous channel including a term for loss of fluid due to evaporation.**

Starting with Darcy's law:

$$\frac{\partial P}{\partial z} = -\frac{\mu v}{k} = -\frac{\mu}{k} \times \frac{dl}{dt} \quad (1)$$

where  $P$  is pressure (N/m<sup>2</sup>),  $z$  is distance (m),  $\mu$  is dynamic viscosity (Ns/m<sup>2</sup>),  $v$  is velocity (m/s) and  $k$  is interstitial permeability (m<sup>2</sup>),  $l$  is the position of the fluid front (m) and  $t$  is time (s).

We write conservation of mass as:

$$\frac{\partial v}{\partial z} = -\frac{2q_0}{\phi h} \quad (2)$$

where  $q_0$  (m/s) is loss of fluid due to evaporation in terms of volume per second per unit area from each face of the channel, the factor of 2 accounting for the fact that evaporation is occurring from the two faces of the channel,  $h$  (m) is the cross-sectional thickness of the channel and  $\phi$  is the porosity. For a two-ply channel, the term  $\phi h$  must account for the two layers of paper, with porosity  $\phi$ , and the gap, with a porosity of 1 (Figure S5).

We take the partial derivative of (1) to obtain:

$$\frac{\partial^2 P}{\partial z^2} = -\frac{\mu}{k} \times \frac{\partial v}{\partial z} \quad (3)$$

then substitute (2) into (3) to obtain:

$$\frac{\partial^2 P}{\partial z^2} = \frac{2\mu q_0}{k\phi h} \quad (4)$$

and integrate (4) twice with respect to  $z$  to give:

$$P = \frac{\mu q_0 z^2}{k\phi h} + C_1 z + C_2 \quad (5)$$

where  $C_1$  and  $C_2$  are constants.

We also know that at  $z=0$ ,  $P=0$ , and at  $z=l(t)$ ,  $P=-2\gamma\cos\theta/r$  (from Young-Laplace where  $\gamma$  is surface tension (N/m),  $\theta$  is contact angle and  $r$  is effective pore radius of the capillaries in paper), so we can find  $C_1$  and  $C_2$  in (5):

$$C_1 = -\frac{2\gamma\cos\theta}{rl} - \frac{\mu q_0 l}{k\phi h}; C_2 = 0 \quad (6)$$

We can substitute (6) into (5) to obtain:

$$P(z,t) = \frac{\mu q_0 z^2}{k\phi h} - \left( \frac{2\gamma \cos\theta}{rl} + \frac{\mu q_0 l}{k\phi h} \right) z \quad (7)$$

Next we take the partial derivative of  $P$  with respect to  $z$  in (7) to find speed of the interface  $dl/dt$ :

$$\frac{\partial P}{\partial z} = \frac{\mu q_0 l}{k\phi h} - \frac{2\gamma \cos\theta}{rl} \quad (8)$$

Substituting (1) into (8) gives:

$$-\frac{\mu}{k} \times \frac{dl}{dt} = \frac{\mu q_0 l}{k\phi h} - \frac{2\gamma \cos\theta}{rl} \quad (9)$$

and we rearranged (9) to find:

$$\frac{d}{dt} l^2 + \frac{2q_0}{\phi h} l^2 - \frac{4\gamma k \cos\theta}{r\mu} = 0 \quad (10)$$

Solving (10) we find:

$$l(t) = \sqrt{\frac{2\gamma k \phi h \cos\theta}{\mu r q_0} \left( 1 - e^{-\frac{2q_0}{\phi h} t} \right)} \quad (11)$$

where we have used  $l(0)=0$ .

We also know that for a simple channel, such as a circular pipe, interstitial permeability can be approximated as:<sup>1</sup>

$$k = \frac{r^2}{8} \quad (12)$$

where  $r$  (m) in this case is the effective pore radius of the channels in a piece of paper.

Substituting (12) into equation (11) gives our final equation:

$$l(t) = \sqrt{\frac{\gamma r \phi h \cos\theta}{4\mu q_0} \left( 1 - e^{-\frac{2q_0}{\phi h} t} \right)} \quad (13)$$

For fitting the experimental results in Kaleidagraph, we set  $\gamma = 0.0728 \text{ N/m}$ ,  $\mu = 0.001 \text{ Ns/m}^2$ , and  $\theta = 0$ .

For a single-ply channel, we estimated  $\phi = 0.34$  and  $h = 150 \text{ }\mu\text{m}$ . For a two-ply channel, the term  $\phi h = 2(0.34)(150 \text{ }\mu\text{m}) + 10 \text{ }\mu\text{m} = 112 \text{ }\mu\text{m}$ .

In the limit where  $q_0$  goes to zero, we can use a Taylor series to make the following approximation:

$$\lim_{q_0 \rightarrow 0} e^{-\frac{2q_0}{\phi h} t} = 1 - \frac{2q_0}{\phi h} t \quad (14)$$



Substituting (14) into (13) gives:

$$l(t) = \sqrt{\frac{\gamma \cos \theta r t}{2\mu}} \quad (15)$$

which is the Lucas-Washburn equation.

## References.

1. H. A. Stone, in *CMOS Biotechnology*, 2007, pp. 5–30.