

# Optimizing LLRF Parameters in the Electron-Ion Collider

A Senior Project

By

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March 15, 2020

Approval Page

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**Date Submitted: March 14, 2020**

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**3/17/2020**

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Date

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# 1 Introduction to Particle Accelerators and the EIC

Ernest Orlando Lawrence won the 1939 Nobel Prize in Physics for inventing the first particle accelerator, the cyclotron, which accelerates particles to high speeds without using high voltage. Scientists initially employed the cyclotron to study the structure of matter, later using it in other experiments when searching for new elements and particles. This technology led to innovations in other fields such as medicine, where Ernest's brother, John Lawrence, pioneered the field of nuclear medicine by treating leukemia and polycythemia patients with radioactive phosphorus.

Modern particle accelerators follow either a linear (LINACs) or circular (synchrotrons) structure, depending on the application. Synchrotrons use an electric field to accelerate a particle and a magnetic field to steer it. By adjusting the magnetic field strength, the particle orbit stays the same as the particles accelerate. This leads to an increased particle collision frequency, providing researchers with more abundant data compared to experiments using LINACs.

This report will discuss the design of the acceleration system's feedback loops for the Electron-Ion Collider (EIC) which accelerates electrons and ions at high speeds in a circular fashion. Experiments will run at the EIC for years at a time with occasional maintenance and upgrade periods. Brookhaven National Laboratory (BNL) will build the EIC to:

- Capture the three-dimensional structure of protons and nuclei
- Study the mystery of proton spin
- Search for gluon saturation and the color glass condensate
- Solve the quark and gluon confinement problem

## 2 The Acceleration System

Synchrotrons utilize an electric field to accelerate the particles and a magnetic field to bend them. Due to the effects of radial acceleration from the magnetic force, particles lose energy each turn around the accelerator through electromagnetic radiation emission. A radio frequency (RF) system compensates the lost energy through cavity structures that build up large voltages at their resonance.

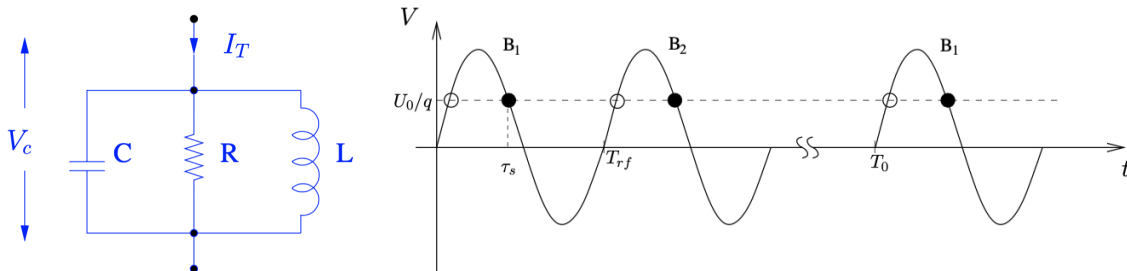
We used feedback loops to regulate the accelerating voltage that acts on the beam of particles. Coupling the beam and cavity interaction allowed us to study and optimize this system.

To energize particles optimally, the molecules must arrive in the RF cavities at a proper time known as the synchronous position. Occurring at an equilibrium point, a black dot represents the synchronous position in Figure 1b. The stable region around the synchronous position, referred to as the RF bucket, contains billions of particles that follow a normal distribution.

To summarize, the RF system serves three purposes:

- Add energy to the beam
- Compensate lost energy from radiation
- Create an RF bucket

RF cavities function as RLC circuits, building up large voltages at their resonance. The field inside the cavity oscillates at resonant frequency. Beam particles must arrive at the proper time to feel the effects of the RF cavity.

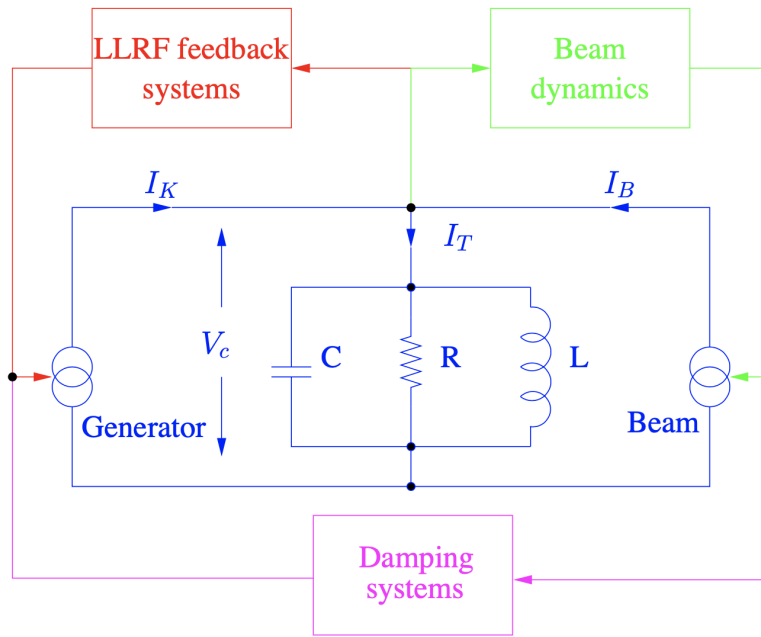


(a) RF Cavity representation as a RLC circuit. (b) Beam pattern delineated as a sine wave. Particles must arrive within the RF bucket, a potential well existing around the stable equilibrium point.

**Figure 1:** Contextual information surrounding RF cavities [1].

Defined as the return to the input of a part of the output of a machine, system, or process [2], feedback allowed us to regulate the RF system of the EIC through implementation of Low Level RF (LLRF) feedback systems. Current from the beam creates an additional and perturbing voltage through the cavity fundamental impedance. The feedback system will try to cancel this perturbation by driving a generator (known as the klystron) to generate a compensating current in the cavity. The cavity voltage modulates

the beam energy, affecting the beam dynamics. Therefore, the beam's current directly impacts the cavity voltage, prompting coupled-bunch instabilities.



**Figure 2:** Components of the accelerating system [1].

The LLRF system contains three components.

- Beam parameters
- High Level RF settings
- LLRF parameters

BNL will set beam parameters for the EIC based on the theoretical limits and goals of the project. To optimize the operation, we adjusted high level RF settings such as the detuning, quality factor  $Q$ , cavity voltage, and klystron forward power. These settings directly impact LLRF parameters, such as direct loop gain, phase, and delay.

We investigated different LLRF topologies by examining the klystron power and beam phase for each case. The first case, direct feedback, takes the error in the output and implements necessary changes within the subsequent input. The second case, a one turn feedback loop (OTFB), increases the effective

feedback gain by acting on the revolution harmonics. For both of these cases, the feedback systems sample the cavity voltage and act back on it through the klystron. The last case investigated, feedforward, samples beam position instead of the voltage, acting on the cavity voltage through the klystron.

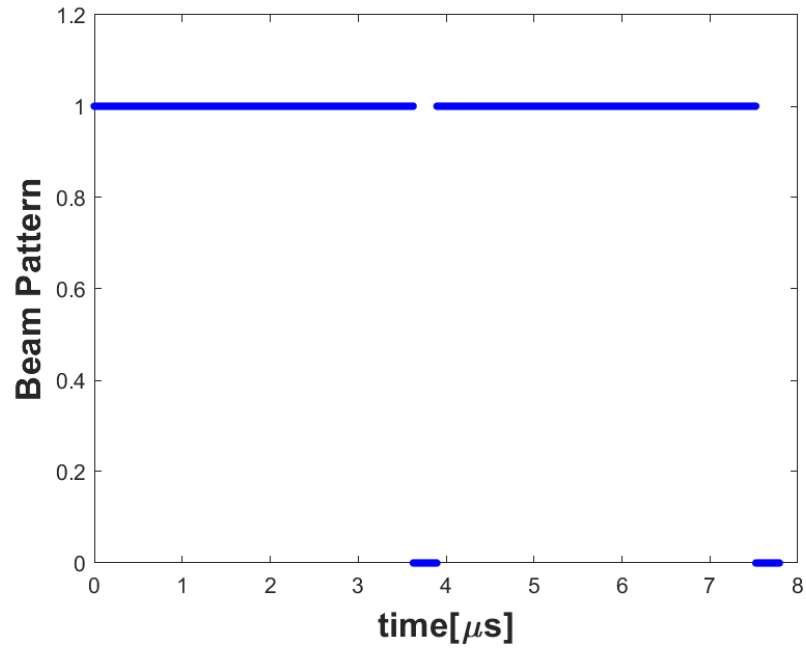
We also examined the effect of the cavity reference voltage phase modulation on the feedback system. In the EIC, phase modulation reduces klystron power by modulating the cavity phase according to the beam transient beam loading [3].

### **3 EIC Motivation**

Optimizing the LLRF parameters in the EIC involves analyzing the trade-off between performance and stability of the beam.

The EIC contains two rings: one for ions and the other for electrons. The particle clouds follow the beam pattern shown below in Figure 3 rather than holding a continuous arrangement. The two gaps in the beam pattern lead to significant perturbations (“gap transients”) in the accelerating voltage. Due to the dissimilarity of the two rings (number of particles, strength of accelerating voltage and more), the gap transients emerge asymmetrical resulting in some particles missing one another at the interaction point. Further investigation produces various remedies that will match the gap transients in the two dissimilar EIC rings.



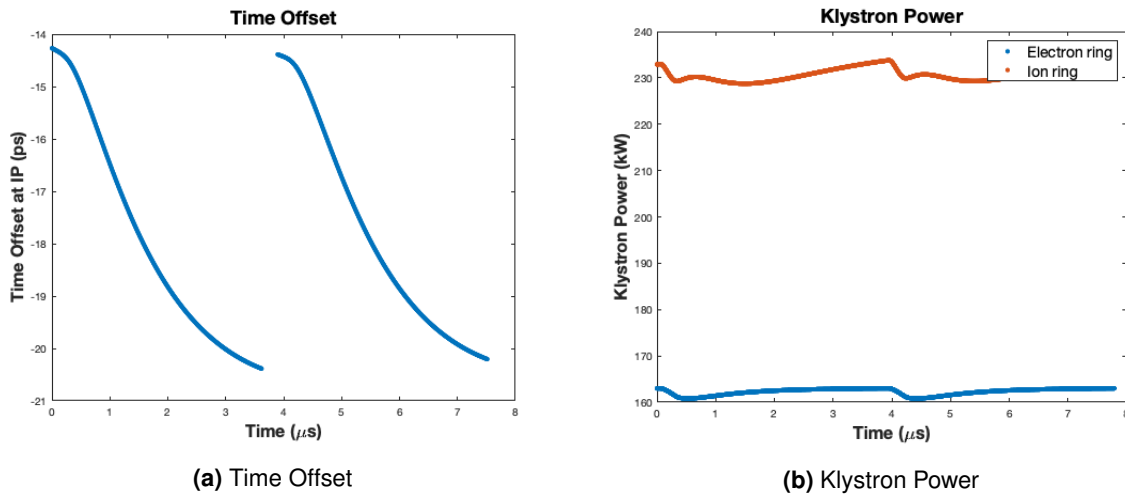


**Figure 3:** Beam Pattern

## 4 Simulation Results

### 4.1 Direct Feedback

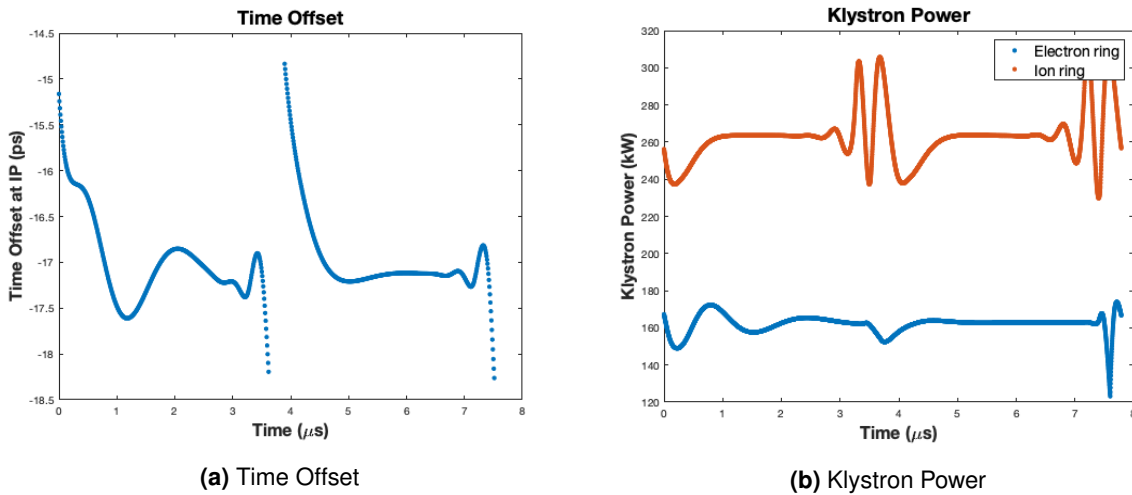
Direct feedback compares the accelerating voltage to a reference value and compensates for the error. A delay of 320 ns in the electron ring simulates realistic settings for the EIC. Figure 4 shows the peak-to-peak time offset (6.1 ps with a standard deviation of 1.9 ps) at the interaction point and the required power.



**Figure 4:** Results of a direct feedback system.

## 4.2 One Turn Feedback

We incorporated a OTFB into the system that increases the gain around the revolution harmonics. This reduces the transient beam loading and effective cavity impedance [4]. Introducing a realistic klystron bandwidth does not change the performance of the passive RF feedback because a closed loop cavity response filters the beam transient. Figure 5 shows the peak-to-peak time offset (3.4 ps with a standard deviation of 0.48 ps) and the required power.



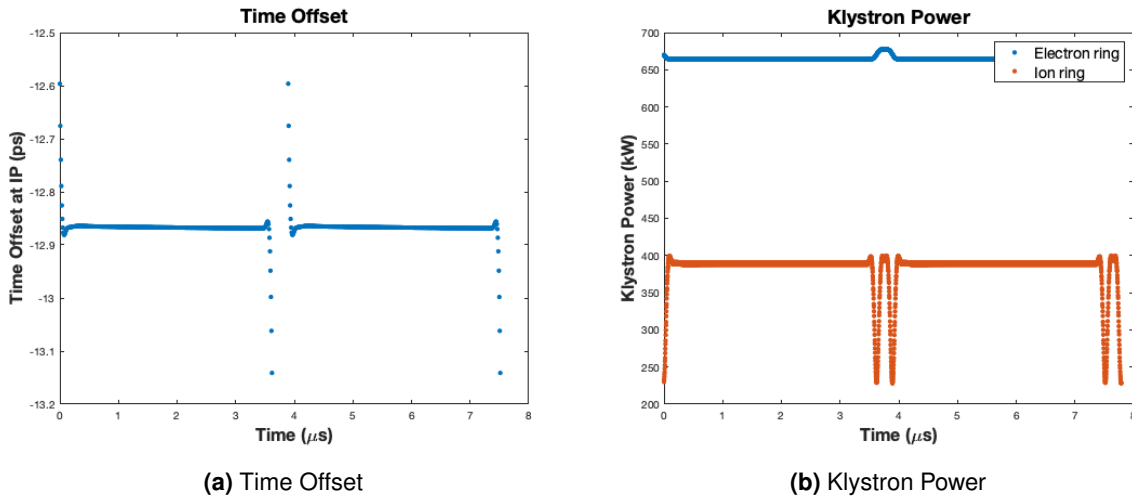
**Figure 5:** Results of a one turn feedback system.

### 4.3 Feedforward

The feedforward system samples the position of the particles instead of the accelerating voltage. It then adjusts the accelerating voltage to minimize any excursions from the ideal position. In the EIC, feedforward performs better than direct feedback and OTFB but at a higher power cost.

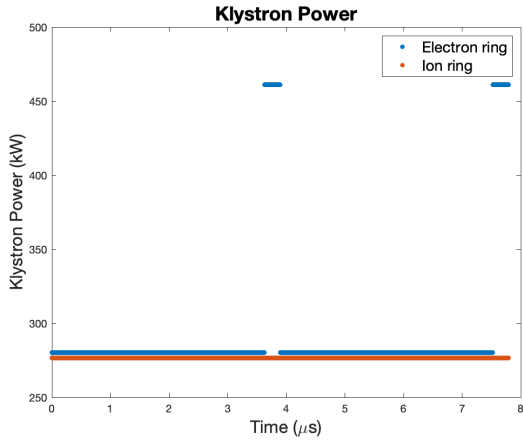
The initial study used an ideal klystron, responding instantaneously to the feedback drive. In reality the klystron response will be defined by the klystron 3 dB bandwidth of about 4 MHz. Considering a short time scale of interest, the bandwidth will affect the wideband klystron. We introduced a realistic klystron bandwidth in the simulations for a more accurate representation.

Figure 6 reveals the peak-to-peak time offset (0.54 ps with a standard deviation of 0.0253 ps) and the required power. Using the same algorithm as the previous systems to find optimal detuning leads to a gap in the beam that requires much more power than expected. Through manual checking, we found an optimal detuning value of -15.4 kHz minimizes energy usage.

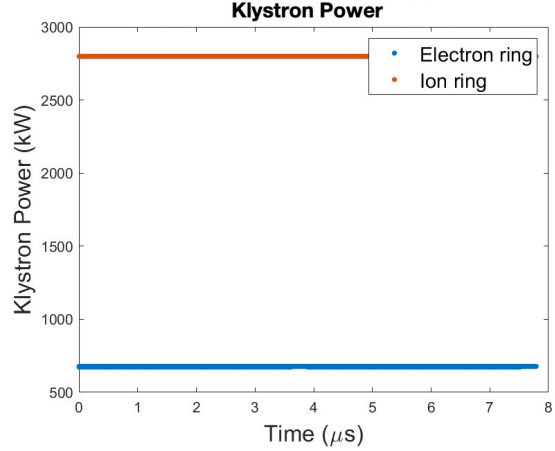


**Figure 6:** Results of a feedforward system.

To see how the optimal detuning value affects the klystron power, Figure 7 displays the energy plots without introducing a klystron bandwidth. Figure 7a shows the optimal detuning value of -15.4 kHz generated from the algorithm used in previous systems. Figure 7b presents the klystron power generated after manually finding the optimal detuning value, -13 kHz.



(a) Algorithm Optimal Detuning



(b) Manual Optimal Detuning

**Figure 7:** Comparing the klystron power of algorithm detuning and manual detuning.

#### 4.4 Summary Table of Results

	IP offset pk-pk (ps)	IP offset $\sigma$ (ps)	Peak power electrons (kW)	Peak power ions (kW)
Direct Feedback	6.11	1.97	1.63e5	2.33e5
One Turn Feedback	3.42	0.4831	1.73e5	3.10e5
FeedForward	0.5448	0.0253	1.63e5	3.99e5

#### 4.5 Conclusion: Return on Investment

Three possible remedies were presented to mitigate gap transients in the EIC. Section 4.4 summarizes the results for each feedback system. The direct feedback system performs similarly to the OTFB, at a reduced power cost. The feedforward system achieves better performance, but at a greater power requirement.

### 5 Results: Detuning Optimization

The klystron provides the power to regulate the cavity voltage. Parameters such as the loaded Q, filling time, desired voltage, or detuning of the cavity affect the peak and average klystron power. The most feasible modifications involve optimizing the detuning and loaded Q values.

We investigated the relationship between power and detuning to minimize the klystron power consumption.

To calculate power with detuning, we used [5]

$$P_g = \frac{1}{2}(R/Q)Q_{ext} |I_g|^2. \quad (1)$$

$I_g$  represents the instantaneous beam current, dependent on detuning. Its value will vary based on phase modulation usage in the accelerating system. We examined the cases of no phase modulation and phase modulation in Section 5.1 and Section 5.2.

$R/Q$  relates the cavity stored energy to the maximum accelerating voltage of the particle. This value relies on the geometry of the system and exists independently of the RF frequency. The coupler quality factor,  $Q_{ext}$ , transforms the cavity quality factor as experienced by the klystron in the presence of a coupler.

## 5.1 No Phase Modulation

When the beam passes through the klystron, we determined the instantaneous current by

$$I_{g,beam} = \left[ \frac{V_o}{2(R/Q)} \left( \frac{1}{Q_{ext}} + \frac{1}{Q_0} \right) + \frac{I_{peak}}{2} F_b \cos(\phi_b) \right] - i \left[ \frac{I_{peak}}{2} F_b \sin(\phi_b) + \frac{V_o \Delta f}{f_{RF}(R/Q)} \right]. \quad (2)$$

When absent in the klystron, we measured the current through

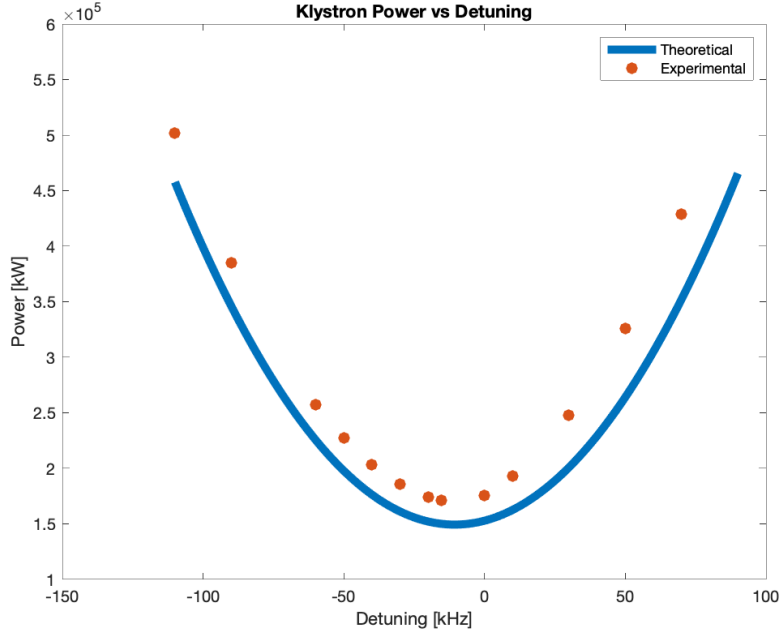
$$I_{g,no\ beam} = \left[ \frac{V_o}{2(R/Q)} \left( \frac{1}{Q_{ext}} + \frac{1}{Q_0} \right) \right] + i \left[ -\frac{V_o \Delta f}{f_{RF}(R/Q)} \right]. \quad (3)$$

The parameters found in Equation 2 and Equation 3 define the klystron current. The cavity voltage,  $V_0$ , modulates the beam energy that affects beam dynamics.  $Q_0$  reflects the cavity quality factor and  $I_{peak}$  signifies the peak current of the beam. The relative bunch form factor,  $F_b$ , relates to the bunch spectrum component at the RF frequency. Figure 1b displays the phase we want the beam to arrive within the RF bucket,  $\phi_b$ . Known as the synchronous phase angle, it relates to the bunch energy loss.  $f_{rf}$  denotes the RF frequency, dependent on the particle (electron or ion) the system accelerates.

In Equation 2 and Equation 3,  $\Delta f$  represents the detuning. We detuned the cavity halfway, corresponding to half of the RF component of the current or a fourth of the peak current.

$$\Delta f = -\frac{I_{peak} F_b \sin(\phi_b) f_{RF} R / Q}{4V_o} \approx 9 \text{ kHz} \quad (4)$$

This keeps the generator current amplitude constant throughout the turn, minimizing peak power.



**Figure 8:** Comparing simulated results to expected theory for klystron power without phase modulation.

Due to the transient behavior between periods of beam and no-beam, the power over a turn will never flatten out to a constant value. Instead, Figure 8 illustrates a vertical shift in the experimental power compared to the theoretical value because of the frequent transients during the switch from beam to no-beam. The simulations resemble the actual condition of the EIC since transients will appear.

## 5.2 With Phase Modulation

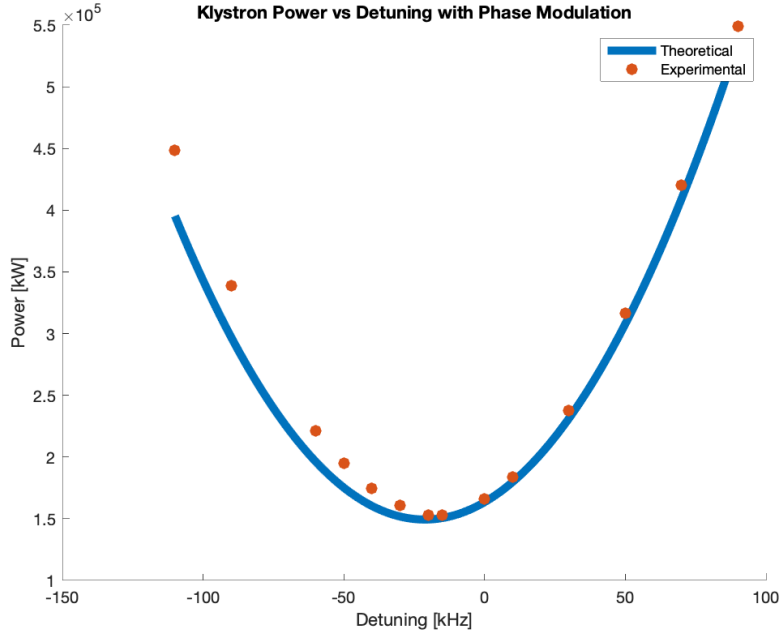
Modulating the cavity voltage phase aids in lowering the klystron power closer to a constant line. The generator current amplitude and phase stays constant while the cavity phase remains modulated. The generator current and optimal detuning expressions differ because we detuned the cavity for a constant current,  $I_{dc}$ .

$$I_g = \left[ \frac{V_o}{2(R/Q)} \left( \frac{1}{Q_{ext}} + \frac{1}{Q_0} \right) + I_{dc} F_b \cos(\phi_b) \right] + i \left[ I_{dc} F_b \sin(\phi_b) - \frac{V_o \Delta f}{f_{RF}(R/Q)} \right]. \quad (5)$$

Similarly, the optimal detuning value slightly changes,

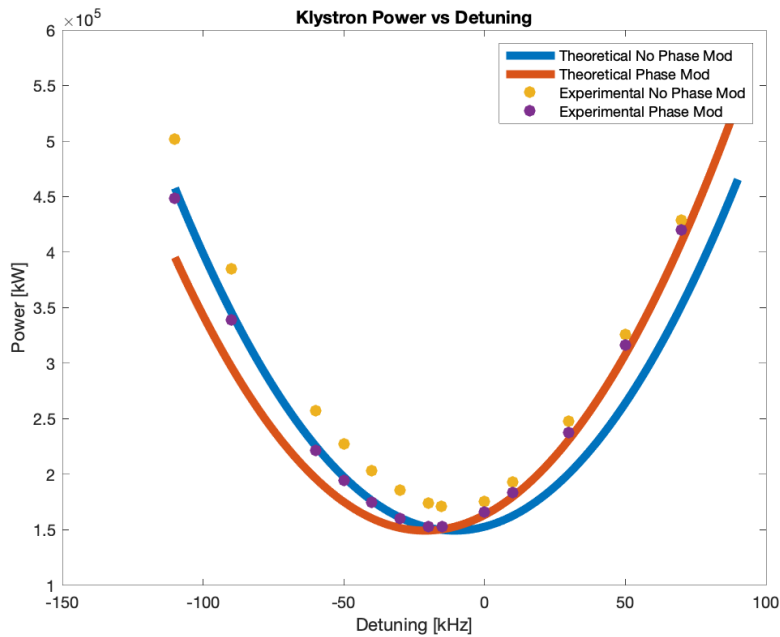
$$\Delta f = -\frac{I_{dc} F_b \sin(\phi_b) f_{RF} R/Q}{V_o} \approx -17 \text{kHz}. \quad (6)$$

Plotting the results,



**Figure 9:** Comparing simulated experimental results to expected theory for klystron power in presence of phase modulation.

To confirm the theoretical basis that phase modulation calculates a more optimal detuning value, we overlaid theoretical and experimental results for both cases. Figure 10 reaffirms the theory, and the experimental optimal detuning approximates to about -20 kHz. This value stands slightly higher than the calculated theoretical value of -17 kHz due to the transient behavior during beam and no-beam segments.



**Figure 10:** Theoretical and experimental results with and without phase modulation.

## 6 Conclusions

The EIC will collide electrons and ions at high energies. Precise control of the accelerating voltage and thus particle beam is essential and motivated this work. We investigated different feedback implementations to control the accelerating voltage and examined the klystron power and beam phase for each case. Enacting feedforward yielded the best interaction point peak-to-peak time offset and highest power consumption. Direct feedback and OTFB performed similarly, with the latter using slightly more power.

We studied the reduction of klystron power consumption through detuning optimization. As shown in Figure 10, cavity phase modulation reduced power usage. This plot also visualizes the relationship between our experimental data with the theoretical models derived in Section 5.

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