

# Culminating Project Report

## Warren J. Baker Center for Science and Mathematics San Luis Obispo, California



Prepared by Blake Johnson

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## **Abstract**

This report analyzes the fire protection features of the Warren J. Baker Center for Science and Mathematics on the Cal Poly San Luis Obispo campus in San Luis Obispo, CA. The prescriptive analysis of the structural fire protection, egress, fire suppression, and fire alarm, detection, and communication systems shows that the building meets the requirements of current codes and standards. The performance based analysis includes simulating design fire scenarios in the atrium using computer modeling (CFAST, FDS) and the results of these models show that the atrium meets the tenability criterion for the calculated evacuation time of occupants.



## **Project Information**

### **Purpose**

The purpose of this project is to select a building and report on its compliance with current fire codes and standards by analyzing the design of the fire protection features present. The fire protection features analyzed are the building's structural fire protection, egress, fire suppression, and fire detection, alarm, and communication systems. Each system is analyzed using a combination of the codes and standards listed below.

- International Building Code (IBC) 2012
- NFPA 101 Life Safety Code Handbook (LSC) 2012
- NFPA 13 Automatic Sprinkler Systems Handbook 2013
- NFPA 72 National Fire Alarm and Signaling Code 2013
- NFPA Fire Protection Handbook, 20<sup>th</sup> edition
- SFPE Handbook of Fire Protection Engineering, 4<sup>th</sup> edition
- NFPA 25 Standard for the Inspection, Testing, and Maintenance of Water-Based Fire Protection Systems 2014

### **Selected Building**

The building selected to be analyzed for this project is the Warren J. Baker Center for Science and Mathematics, located on the Cal Poly campus in San Luis Obispo, CA. The codes and standards, relevant to the analysis in this report, the building was designed to are listed below.

- California Building Code (CBC) 2007
- NFPA 101 Life Safety Code (LSC) 2006
- NFPA 70 National Electric Code 2005
- California Fire Code (CFC) 2007

### **Building Information**

The building is the second largest on campus with a total square footage of 188,372 and a height of 108 feet. It is a six-story, non-high-rise, steel structure located at the center of the Cal Poly campus. There are 64 faculty offices, 44 laboratories, 7 studio classrooms, and 8 lecture halls; these spaces can accommodate about 1650 students. A number of ground level entrances/exits exist on floors 1 through 3, with the main entrances/exits located at the end of the West wing on level 1, East wing on level 3, and the North and South sides of the centrally located atrium on level 2.

Proposed in 2010 and opened in Fall 2013, the building was constructed to replace the adjacent aging science building on campus.



## **Prescriptive Analysis**

The following sections of this report cover the prescriptive, code requirements for this building. These sections analyze the building's structural fire protection, egress, fire suppression, and fire detection, alarm, and communication systems prescriptive requirements based on current codes and standards. Each section summarizes the results of the prescriptive analysis of that particular system and lists any discrepancies found in the design. The prescriptive sections are listed below.

- Structural Fire Protection Analysis
- Egress Analysis
- Fire Suppression System Analysis
- Fire Alarm, Detection, and Communication Systems Analysis

These prescriptive sections use a combination of current codes and standards for the design analysis, which are listed below.

- International Building Code (IBC) 2012
- NFPA 101 Life Safety Code Handbook (LSC) 2012
- NFPA 13 Automatic Sprinkler Systems Handbook 2013
- NFPA 72 National Fire Alarm and Signaling Code 2013
- NFPA Fire Protection Handbook, 20<sup>th</sup> edition
- SFPE Handbook of Fire Protection Engineering, 4<sup>th</sup> edition
- NFPA 25 Standard for the Inspection, Testing, and Maintenance of Water-Based Fire Protection Systems 2014

The building may or may not meet the requirements of these current codes and standards because the building was designed using prior editions of some of these codes and standards. The codes and standards, relevant to the analysis in this report, the building was designed to are listed below.

- California Building Code (CBC) 2007
- NFPA 101 Life Safety Code (LSC) 2006
- NFPA 70 National Electric Code 2005
- California Fire Code (CFC) 2007



## **Structural Fire Protection Analysis**

This section covers the analysis of the structural fire protection requirements using the International Building Code (IBC) 2012 and details of this analysis can be found in the sections listed below.

- Building Design
- Structural Fire Protection

## **Analysis Summary**

The elements analyzed in the Center for Science building comply with the IBC requirements for Type I-B fully sprinklered construction, suitable for primarily Group B occupancy. Many of the details in the plans call out a UL Design No. as a basis for fire protection in the design and all UL Design No. meet required fire ratings. The actual thickness of SFRM was never specifically given in the plans for the structural steel, but the UL Design No. was called out.

The design and construction of the Center for Science meets the IBC 2012 requirements for this construction type and occupancy.



## **Building Design**

### **Occupancy Classifications**

The main occupancy for the building is Group B. The classrooms are Group B and account for the majority of the floor area on levels 2 through 6. Group B occupancy is described in IBC Section 304.1. There are other occupancy Groups in this building that are on different levels of the building. The other Groups are A-3, H-3, S, S-1, and S-2.

The seminar rooms (occupant load greater than 50) belong to Group A-3. The seminar rooms account for the majority of the floor area on level 1, but are also present on levels 3 through 6. Group A-3 occupancy is described in IBC Section 303.4.

Storage rooms, mechanical rooms, electrical rooms, and hazardous belong to Groups S, S-1, S-2, and H-3, respectively. These rooms make up a small part of the total area and are present on only a few different levels. Groups S, S-1, S-2, and H-3 occupancy is described in IBC Sections 311.1, 311.2, 311.3, and 307.5, respectively.

There are special requirements for Group H-3 in IBC Section 415.9. These requirements are not related to structural fire protection, but they cover fire requirements of flammable and combustible liquids, gas rooms, floors in storage rooms, and separation of highly toxic solids and liquids. Depending on the actual materials stored in this occupancy Group, it is likely that a minimum of 1-hour fire barriers between all other areas is required. These fire barriers are covered in IBC Sections 707 and 711.

### **Construction Type**

The building plans specify the building as Type I-B construction fully sprinklered. Although the building was designed using the CBC, the IBC can also be used to determine the construction type. Using IBC Table 503, the building height of 108 feet limits the construction type to Type I. IBC Section 504.2 to increase the maximum allowable height of a fully sprinklered building would not be enough to allow for Type II construction.

Both Type I-A and I-B are allowed for this building. Type I-B was selected most likely because it is less expensive than Type I-A.



## Structural Fire Protection

### Fire Resistance Requirements

IBC Table 601 gives the fire resistance requirements for Type I-B construction. The required fire resistance rating for the structural frame and exterior and interior bearing walls is 2 hours. Floor construction and secondary members must have a fire resistance rating of at least 2 hours. Roof construction and secondary members must have a fire resistance rating of at least 1 hour. Non-load bearing interior walls and partitions are not required to have a fire resistance rating and non-load bearing exterior walls and partitions are not required to have a fire resistance rating if separation distance is over 30 feet, otherwise the exterior walls and partitions must have a fire resistance rating of at least 1 hour per IBC Table 602. The separation distance is over 30 feet because the nearest building is about 36 feet to the east of the Center for Science. Additionally, the fire resistance rating for the structural frame and interior bearing walls may be reduced to 1 hour if these elements support only the roof. These requirements are summarized on Table 1a.

Table 1a – Structural Fire Resistance Requirements

Structural Element		Hourly Rating
Structural Frame		2 or 1
Bearing walls	Exterior	2
	Interior	2 or 1
Non-bearing walls		0
Floor		2
Roof		0 or 1

This building also has more than one type of occupancy so IBC Table 508.4 must be used to determine the required separation of occupancies. The applicable separations for this building are B to all others Groups, S-1 to S-2, and S-2 to H-3. The separation required between the occupancies is 1-hour except between B and S-1 where there is no separation requirement and there is no separation requirement between occupancies of the same Group. These occupancy separation requirements are summarized on Table 1b.

Table 1b – Hourly Separation of Occupancies

	S-1	S-2	H-3
B	0	1	1
S-1	-	1	1
S-2	-	-	1



## **Structural Frame**

The structural frame of the building is typical steel construction with steel wide flange beams used as girders, beams, and columns. The elevator shafts are supported with rectangular hollow steel sections along their heights. The steel structural frame is protected from fire by spray applied fire resistive material (SFRM). W-shaped beams are fireproofed to the UL Design No. 917 specification and W-shaped columns are fireproofed to the UL Design No. X772 specification. For aesthetics and durability of the SFRM, the columns and beams are boxed with steel channels and gypsum wallboard.

## **Floor and Roof Assemblies**

The floor and roof assemblies are 3" thick 20 gauge composite metal decks with 3-1/4" light weight concrete fill. The concrete is reinforced with 6x6-W2.0xW2.0 welded wire fabric with 3/4" clear. The deck is supported by steel wide flanged beams and headed shear studs join the beam and deck compositely. The assemblies are rated for 2 hours by using IBC 721.2.2.1.3 to obtain the equivalent thickness of 3.75" then using IBC Table 721.2.2.1 to meet the required thickness of 3.6" for a lightweight concrete slab.

## **Exterior Walls**

The exterior walls are either load bearing concrete retaining walls or non-load bearing concrete masonry walls. The east sides of level 1 and 2 have 16" thick concrete retaining walls, but all other walls are non-load bearing concrete masonry walls. Using IBC Table 721.1(2), the fire rating for the concrete retaining wall is well beyond the required 2 hours and the masonry walls are required to be between 3.2" and 4.2" thick, depending on the type of fill. The minimum wall thickness specified on the CMU wall reinforcing schedule is 4" so it is possible that the wall is not quite thick enough if the improper fill was used with a 4" thick block. However, since the building is 108 feet tall with 6 stories, the average height per story is 18 feet; allowing about 2 to 3 feet for the floor slab and steel beam, a wall will need to be at least 15 feet high, so a minimum wall thickness of 8" is needed, which satisfies the required fire resistance rating.

## **Interior Walls and Partitions**

The interior walls and partitions are non-load bearing and are either concrete masonry walls or steel stud walls. The different wall details are shown in the appendix on sheet A8.01. Fire ratings and UL Design No. are given for each detail, if applicable. The plans also call out some interior walls to be 2-hour rating fire walls. The walls around the elevator and stair shafts and the walls separating the atrium from control areas 1 and 2, the East and West wings of the building respectively, are designated as 2-hour fire rated wall assemblies.



## **Egress Analysis**

This section covers the analysis of the requirements for egress using the requirements of the Life Safety Code (LSC) 2012 and the International Building Code (IBC) 2012; the details of this analysis can be found in the sections listed below.

- Occupancy
- Means of Egress
- Fire Rating Requirements
- Occupancy/Egress Maps

Standards referenced in this section are NFPA Fire Protection Handbook, 20<sup>th</sup> edition and SFPE Handbook of Fire Protection Engineering, 4<sup>th</sup> edition for calculating total evacuation time.

## **Analysis Summary**

The Center for Science has an occupant load of almost 3000 and several exits on each level that meet or exceed the minimum width requirements of the LSC. The estimated total evacuation time of the entire building is about 13 and a half minutes, based on pre-movement time, travel time, and exit queuing. The fire resistance rating for the stairway enclosures is 2-hour, which meets or exceeds the requirements of the LSC. The performance based smoke analysis of the atrium shows that fire barriers are not required at the offices on levels 4, 5, and 6 that exit directly to the atrium, the details of this analysis can be found in the atrium analysis section of this report.

The design of the Center for Science meets the LSC 2012 requirements for occupancy, means of egress, and fire resistance ratings.



## **Occupancy**

### **Occupancy Classifications**

The building has more than one type of occupancy, so it is considered a multiple occupancy building, per LSC Section 6.1.14.2.1. The occupancies, which are discussed below, share common paths of travel, so the building is classified as a mixed occupancy building defined in LSC Section 6.1.14.2.2. Due to the mixed occupancy classification, the building shall comply with the most restrictive requirements of the occupancies involved, per LSC Section 6.1.14.3.

The most common occupancy in the building is Group B. There are many different uses for Group B in this building and it accounts for the majority of the floor area on levels 2 through 6. Group B occupancy is described in IBC Section 304.1. The other occupancy Groups found in this building, on various levels, are A-3, H-3, S, S-1, and S-2.

The seminar rooms (occupant load greater than 50) and terraces belong to Group A-3. The seminar rooms account for the majority of the floor area on level 1 and one room on level 3. The terraces are present on levels 4, 5, and 6. Group A-3 occupancy is described in IBC Section 303.4. Generally, Group A-3 has the most restrictive requirements of the occupancies in this building.

Storage rooms, mechanical rooms, electrical rooms, and hazardous belong to Groups S, S-1, S-2, and H-3, respectively. These rooms make up a small part of the total area and are present on only a few different levels. Groups S, S-1, S-2, and H-3 occupancy is described in IBC Sections 311.1, 311.2, 311.3, and 307.5, respectively.

There are special requirements for Group H-3 in IBC Section 415.9. These requirements are not related to egress, but cover fire requirements of flammable and combustible liquids, gas rooms, floors in storage rooms, and separation of highly toxic solids and liquids.

### **Occupant Loads**

The occupant load for each space is calculated by dividing the net floor area, defined in LSC Section 3.3.21.2.2, by the appropriate occupant load factor in LSC Table 7.3.1.2 for its intended use. The attached plans give the floor area and occupancy group, load factor, and load for each room. The 300 square feet per person factor used in the plans for the mechanical and storage rooms indicate that the plans use IBC Table 1004.1.2 for determining load factors because LSC Table 7.3.1.2 would give 500 square feet per person as a load factor for storage use in this building. For all other occupancies in this building, the IBC and LSC give the same load factor. There are minor discrepancies in the calculations where some storage space occupant loads are 1 occupant lower than they should be due to rounding.



The differences in load factors and rounding are not major issues for the analysis or design of the structure because these occupancies make up a small portion of the total building area and occupancy. The total occupant load for each level is given in Table 2a and it includes subtotals for the West and East wings on either side of the atrium as well as the atrium area itself, labeled as Center.

Table 2a – Total Occupant Load per Level

Level	Occupant Loads (Persons)			
	West	Center	East	Total
1	703	-	-	703
2	262	77	184	523
3	312	155	234	701
4	179	65	221	465
5	-	67	196	263
6	-	68	183	251
<b>Total</b>	<b>1456</b>	<b>432</b>	<b>1018</b>	<b>2906</b>

It is worth noting that occupant load factors, and therefore occupant loads, are based on use and not occupancy type. For example, the Business occupancy on level 1 uses a load factor of 15 square feet per person because it is used for assembly. Since the occupant load is below 50 persons and the area is less than 750 square feet, the space is not considered Assembly occupancy due to IBC Section 303.1.2.

### Occupant Behavior

The occupants will primarily be adults that are students and professors that come and go at different times of the day. Occupants come and go between classes that usually last an hour, but some classes may last longer and some occupants may stay for a longer period within the building to study or do work. All occupants should be awake and alert.

An occupant's reaction to an alarm, the recognition time, should be almost immediate. Once an occupant hears an alarm, they should stop what they are working on, grab their books and/or backpacks, and begin proceeding to the nearest exit, the time the occupant takes for these actions is the response time.

The sum of the recognition time and the response time is the pre-movement time. The pre-movement time for occupants should be relatively quick and can be estimated using SFPE Handbook Table 3-12.2. Considering this building as a mid-rise office building, the average pre-movement time for occupants on a warm day is 36 seconds. This number is important for calculating the total evacuation time of the building and for the tenability analysis of the atrium.



## Means of Egress

### Egress Capacity

Egress capacity is based on stairway capacity and doorway capacity, which can be calculated using capacity factors found in LSC Table 7.3.3.1. However, the plans do not use LSC Table 7.3.3.1, but rather IBC Sections 1005.3.1 for stairs and 1005.3.2 for doors. The difference between the requirements of LSC and IBC is the LSC uses factors of 0.3 for stairs and 0.2 for doors while an exception in the IBC allows factors of 0.2 for stairs and 0.15 for doors. The provided width of the doors and stairs still exceed the required width calculated using the LSC, results for each component are shown on Table 2c on the next page. Component labels on Table 2c match those on Figures a-f on pages 16-21.

### Number of Exits

The number of exits required from any floor is given in LSC Sections 7.4.1.1 and 7.4.1.2. Levels 1, 2, and 3 all have a total occupant load greater than 500, but less than 1000, so 3 exits are required. Levels 4, 5, and 6 all have a total occupant load less than 500, so 2 exits are required. The total number of exits for each level are listed alongside the required number of exits for each level on Table 2b.

Table 2b – Total Number of Exits per Level

Level	Total Number of Exits	
	Provided	Required
1	3	3
2	7	3
3	4	3
4	3	2
5	2	2
6	2	2

### Exit Arrangement

The exits in this building, on each level and for each space, are reasonably remote per LSC Section 7.5.1.3. Since the building is protected by a sprinkler system throughout, LSC Section 7.5.1.3.3 applies to reduce the exit remoteness to one-third the diagonal distance of the area served by an exit. Neither the common path of travel or dead end distance limits is exceeded in any space on any level of this building. Some common path of travel distances are shown on the attached plans. Other locations were also checked to ensure that the distance requirements were satisfied. Maximum common path of travel distances are found in LSC Sections 12.2.5.1.2, 38.2.5.3.1, and 42.2.5 for Assembly, Business, and Storage occupancies, respectively. Dead end corridor distances must comply with LSC Section 7.5.1.5 and permitted dead end distances are found in LSC Sections 12.2.5.1.3, 38.2.5.2, and 42.2.5 for Assembly, Business, and Storage occupancies, respectively.



Table 2c – Egress Capacity per Component

Level	Component	Load (persons)	Factor (in/person)	Width (in)		Meets Required?
				Required	Provided	
1	Door Main	352	0.2	71	216	Yes
1	Door Back	352	0.2	71	96	Yes
1	Door 4	160	0.2	32	36	Yes
2	Stair 5	74	0.2	15	48	Yes
2	Door 5	74	0.3	23	36	Yes
2	Stair 4	74	0.2	15	48	Yes
2	Door 4	74	0.3	23	36	Yes
2	Door West	74	0.2	15	72	Yes
2	Door Main N	74	0.2	15	144	Yes
2	Door Main S	234	0.2	47	144	Yes
2	Door East a	74	0.2	15	72	Yes
2	Door East b	74	0.2	15	72	Yes
3	Stair 5	160	0.3	48	48	Yes
3	Door 5	160	0.2	32	36	Yes
3	Stair 4	160	0.3	48	48	Yes
3	Door 4	160	0.2	32	36	Yes
3	Stair 3	160	0.3	48	48	Yes
3	Door 3	160	0.2	32	36	Yes
3	Door East	160	0.2	32	36	Yes
4	Stair 4	155	0.3	47	48	Yes
4	Door 4	155	0.2	31	36	Yes
4	Stair 3	155	0.3	47	48	Yes
4	Door 3	155	0.2	31	36	Yes
4	Stair 1	155	0.3	47	48	Yes
4	Door 1	155	0.2	31	36	Yes
5	Stair 3	132	0.3	40	48	Yes
5	Door 3	132	0.2	27	36	Yes
5	Stair 1	132	0.3	40	48	Yes
5	Door 1	132	0.2	27	36	Yes
6	Stair 3	126	0.3	38	48	Yes
6	Door 3	126	0.2	26	36	Yes
6	Stair 1	126	0.3	38	48	Yes
6	Door 1	126	0.2	26	36	Yes



## **Travel Distance**

Travel distance to exits is shown on the attached life safety plans for some spaces and travel distance is sufficient for all spaces and occupancies per LSC Section 7.6 and LSC Sections 12.2.6.2 and 38.2.6.3, and 42.2.6 for Assembly, Business, and Storage occupancies, respectively.

## **Exit Sign Placement**

The requirements of exit signs are given in LSC Section 7.10 and illumination requirements are given in LSC Section 7.8. Exit signs and illumination are required by all occupancies present in this building and are listed in the individual occupancy sections of the LSC in Subsection \_\_.2.10 and \_\_.2.8, respectively. The placement of exit signs are shown in the attached life safety plans and the placements meet the requirements of the LSC, there are exit signs placed at every exit and exit signs help to guide occupants to those exits. The number of exit signs in the corridors could be reduced in accordance with LSC Section 7.10.2.1 and recommendations for minimum exit sign placement are shown in the attached occupancy and exit location map.

## **Estimated Total Evacuation Time**

The method to predict egress time for a building is explained in the NFPA Fire Protection Handbook Chapter 4-2. The time to evacuate all levels of the entire building can be estimated by determining the flow of people passing through egress components. The egress component with the lowest flow will control the time taken on sets of components in series, for example a narrow door would control flow even if it leads to a wide stairway with greater capacity. Queuing is assumed to take place so that flow will control the travel time. In this analysis, travel time within a stairway is considered, but the travel time to the stairway is not considered.

To calculate the time taken on the stairs some dimensions are needed. Floor-to-floor height is 16 feet, stair risers are 6.86 inches (7 inches used in calculations), and each landing has about 10 feet of travel distance. The travel distance on the stairs and both landings to one level below is 50 feet. Assuming an optimal density of 0.175 persons per square foot due to queuing and using Equation 1 in NFPA Section 4-2, the travel speed down the stairs is 105 feet per minute (see calculation on next page). The travel time for an occupant moving with the flow is 0.48 minutes per floor. The calculated flow for stairways 1 and 5, stairways 3 and 4, and the stairway doors is 59.35, 55.5, and 48 persons per minute, respectively. Stairways 3 and 4 are enclosed stairways that have their flow limited to 48 persons per minute by the exit door at the bottom of the stairways. Stairways 1 and 5 are outside stairways with no exit door so the flow is limited by the stairs to 59.35 persons per minute since flow from all the entrance doors is cumulative. The total occupant load from each level on each stairway must also be considered when estimating total evacuation time. Table 2d on the next page summarizes the flow, occupant load, travel time, and total evacuation time, including the pre-movement time of 36 seconds, for each stairway.



Calculation of travel speed down the stairs:

$$S = k - akD$$

$$S = (212) - ((2.86)(212)(0.175))$$

$$S = 105 \text{ ft/min}$$

Table 2d – Limiting Egress Component Flow and Travel Times

Stair #	Limiting Component	Flow (persons/min)	Total Load (persons)	Travel Time (min)	Total Time (min)
1	Stair	59.35	413	0.48	8.04
3	Door	48	573	0.48 + 0.26	13.28
4	Door	48	389	0.48	9.18
5	Stair	59.35	234	0.48	5.02

Stairway 3 exits into the atrium on level 2 so the travel distance from the stairway exit to the nearest exit, Door Main S, must be accounted for. The travel distance from the exit of stairway 3 to Door Main S is about 60 feet. The atrium where stair 3 exits is quite large so speed is assumed to be at its maximum, where density is assumed to be 0.05 persons per square foot; using Equation 1 in NFPA Section 4-2 the travel speed from the exit of stairway 3 to Door Main S is 235 feet per minute (see calculation below). The time taken for an occupant to travel 60 feet is 0.26 minutes. Exit discharge into an atrium is allowed per LSC Section 8.6.7(2).

Calculation of travel speed from stair 3 to south exit in atrium:

$$S = k - akD$$

$$S = (275) - ((2.86)(275)(0.05))$$

$$S = 235 \text{ ft/min}$$

Travel time to the stairway is ignored in the calculation because the analysis assumes queuing will occur immediately upon completion of pre-movement time. The basis of this assumption is since the estimated pre-movement time is the average of all occupants, half the occupants have already completed their pre-movement time and begun their travel time, and occupants initially closer to the exits may have already reached the exits and started the queue.

The estimated total evacuation time is 13 minutes and 17 seconds, which is based on the time for occupants to travel through stairway 3.



## Fire Rating Requirements

### Fire Resistance Ratings

Stair enclosures that connect three or fewer stories are required to have a minimum 1-hour fire resistance rating and stair enclosures that connect four or more stories are required to have a minimum 2-hour fire resistance rating, per LSC Section 7.1.3.2.1. Table 2e shows which levels are connected by each stairway, the total number of levels each stairway connects, the minimum fire resistance rating, and the fire resistance rating on the plans. Stairways 1 and 5 require a minimum 1-hour fire resistance rating and stairways 3 and 4 require a minimum 2-hour fire resistance rating. The plans specify that stairways 1, 3, 4, and 5 are protected with a 2-hour fire resistance rating, so the LSC requirements are satisfied.

Table 2e – Stairway Fire Resistance Ratings

Stair #	Level						Total	Fire Resistance Rating	
	1	2	3	4	5	6		Required	Provided
1				x	x	x	3	1-hour	2-hour
3		x	x	x	x	x	5	2-hour	2-hour
4	x	x	x	x			4	2-hour	2-hour
5		x	x				2	1-hour	2-hour

The requirements for the atrium located at the center of the building are listed in LSC Section 8.6.7. The atrium meets these requirements, except the offices connected to the atrium on levels 4 through 6 must be protected by a 1-hour fire barrier per LSC Section 8.6.7(1) or the results of an engineering analysis must show that enclosure is not required per LSC Section 8.6.7(1)(b). To meet code requirements, an engineering analysis must be performed per LSC Section 8.6.7(5) to eliminate the need for the 1-hour fire barrier. The engineering analysis performed for the atrium is discussed in the atrium analysis section of this report.

### Interior Finish

Interior finish requirements for Assembly, Business, and Storage are provided in LSC Sections 12.3.3, 38.3.3, and 40.3.3, respectively. Since the building is protected throughout by an automatic sprinkler system, the interior finish requirements may be reduced by one step per LSC Sections 10.2.8.1 and 10.2.8.2. The most restrictive requirements are for the Assembly occupancy present in this building so the finish requirements should be based on that occupancy.

Using LSC Sections 12.3.3, 10.2.8.1, and 10.2.8.2, the interior wall and ceiling finishes for the corridors, lobbies, and assembly areas must be Class A, Class B, or Class C and the enclosed stairways must be Class A or Class B. Interior floor finishes in all areas must be Class I or Class II or must comply with LSC Section 10.2.7.2.



## **Occupancy Maps**

Figures a, b, c, d, e, and f are on the following 6 pages. Each figure is a color-coded map of the occupancy and usage for each space on a particular level of the building. Primary exit locations and suggested minimum exit sign placement are also shown on the maps. There are more uses for the occupancies than could be labeled in the maps so only the most common uses were labeled. The uses for each space were labeled based on the title of each space and some spaces did not fit well with any defined use and were left labeled as the occupancy, for example the woodshop was left as Business occupancy. The occupancy titles for each space can be found on the plans in the appendix of this report.



## Level 1

### Legend

- |                 |                       |
|-----------------|-----------------------|
| ■ Assembly      | ■ Storage             |
| ■ Lecture Halls | ■ Mechanical          |
| ■ Terrace       | ■ Electrical          |
| ■ Business      | ■ Hazardous           |
| ■ Atrium        | ■ Restrooms           |
| ■ Classroom     | ■ Corridors           |
| ■ Labs          | ■ Elevator Shafts     |
| ■ Office        | ■ Exit Stairs         |
| ■ Workspace     | ● Exit Sign Placement |

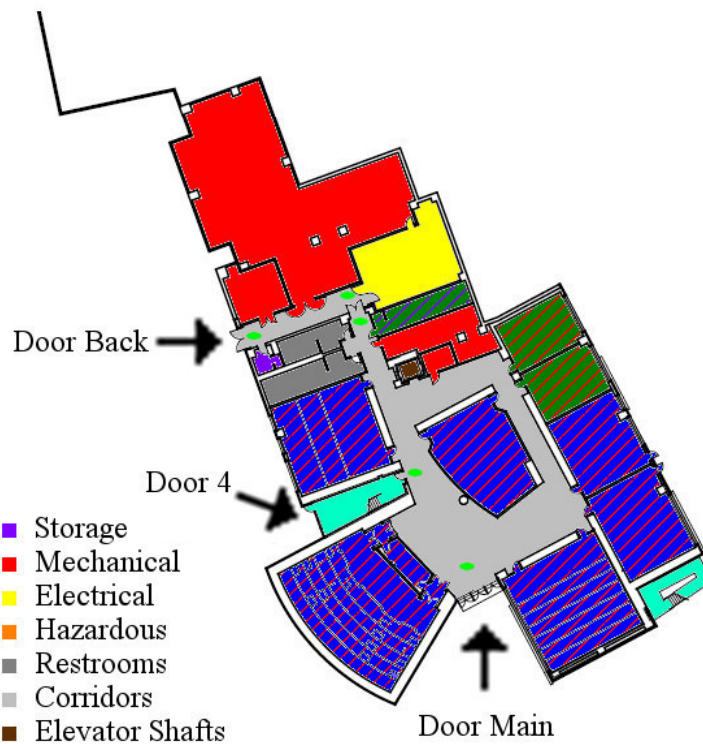


Figure a – Level 1 Occupancy Map



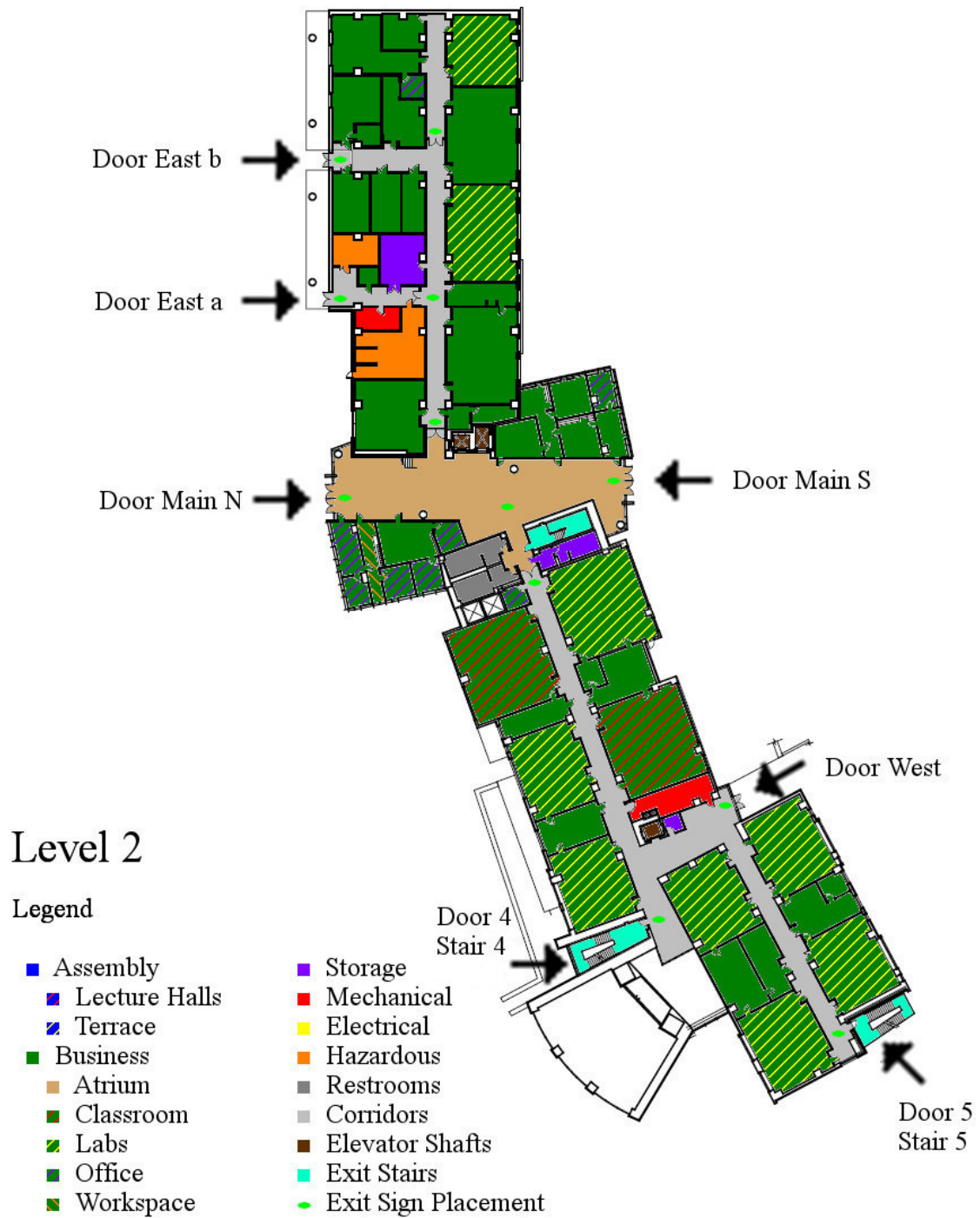


Figure b – Level 2 Occupancy Map



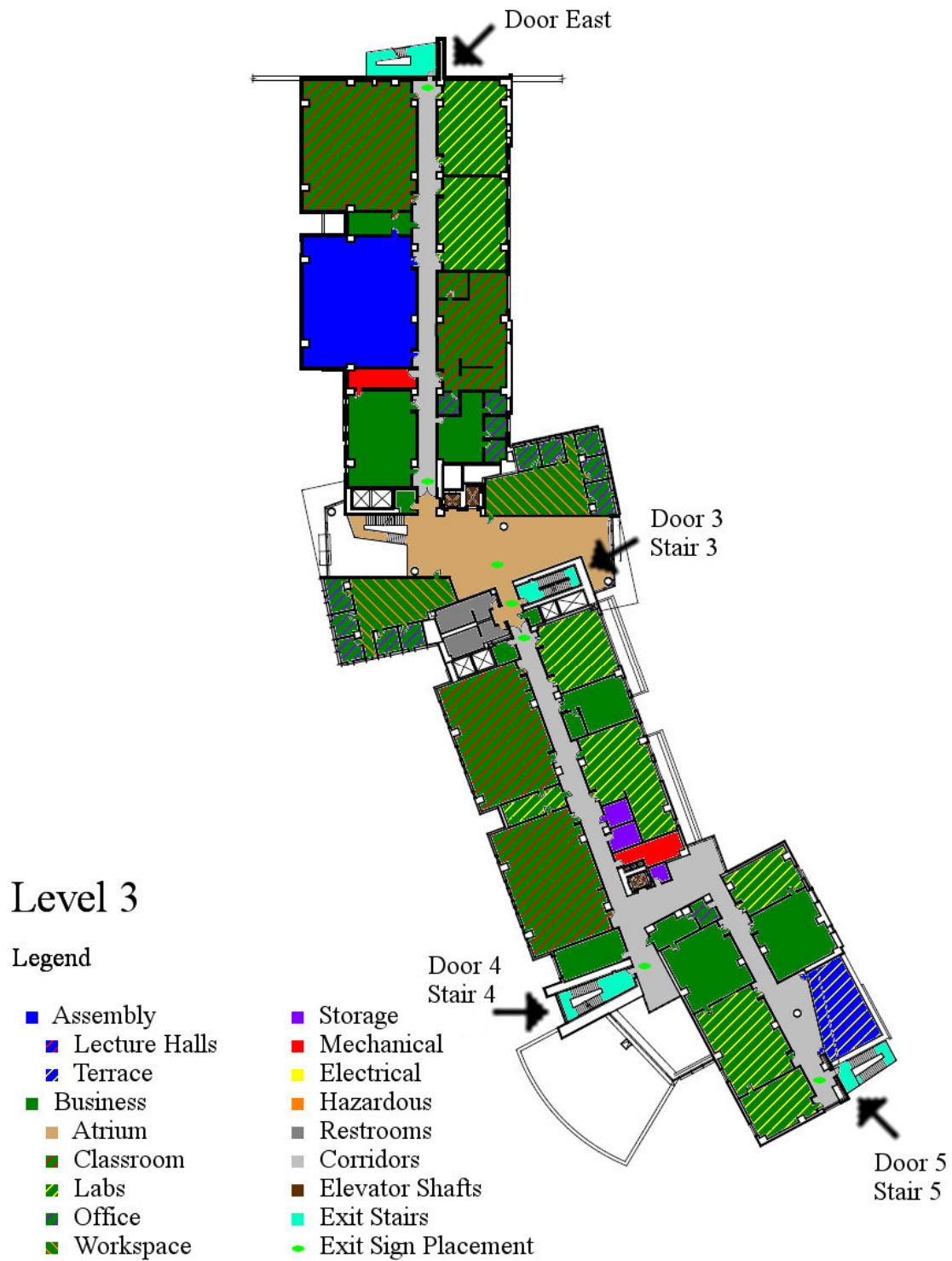


Figure c – Level 3 Occupancy Map



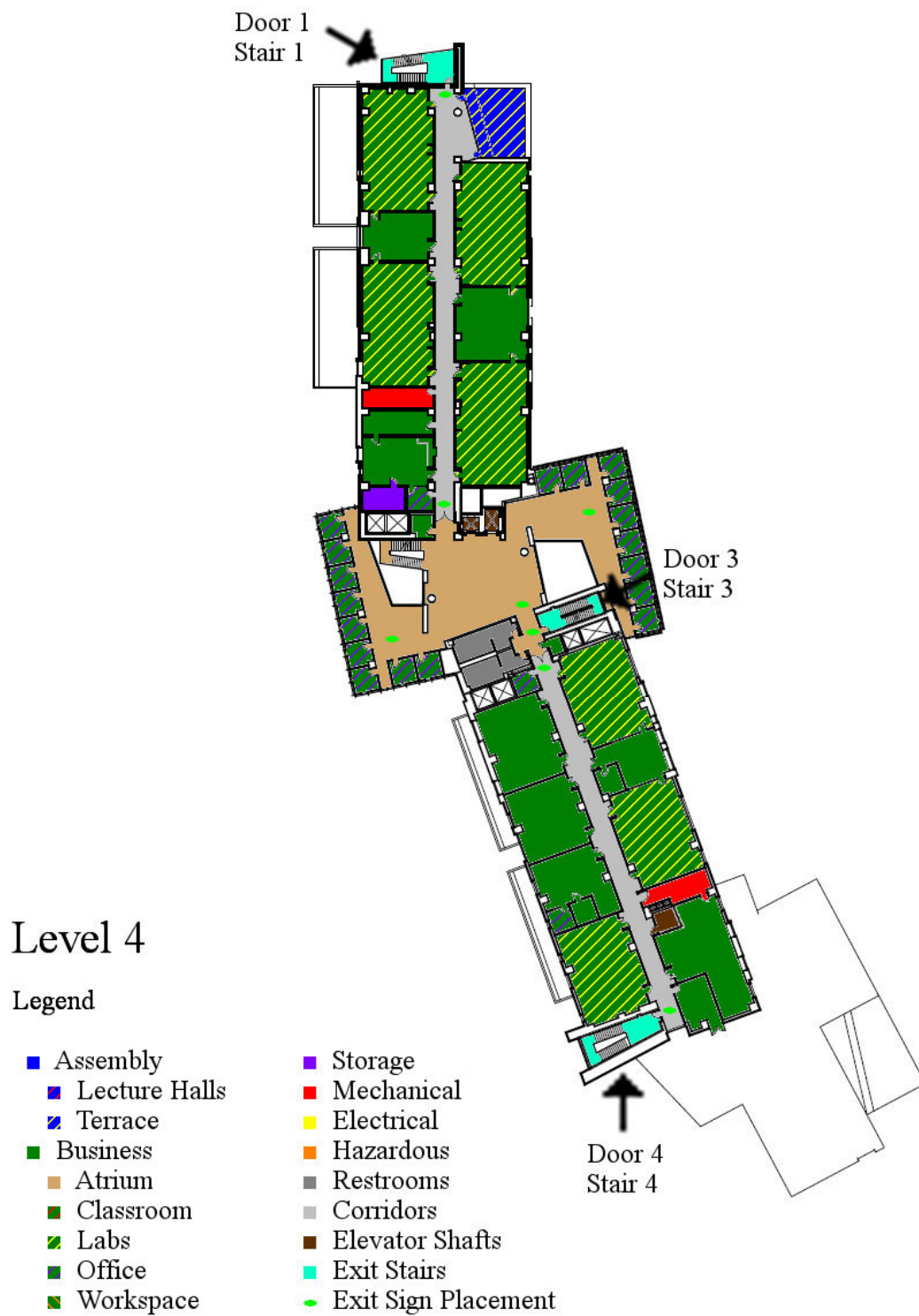


Figure d – Level 4 Occupancy Map



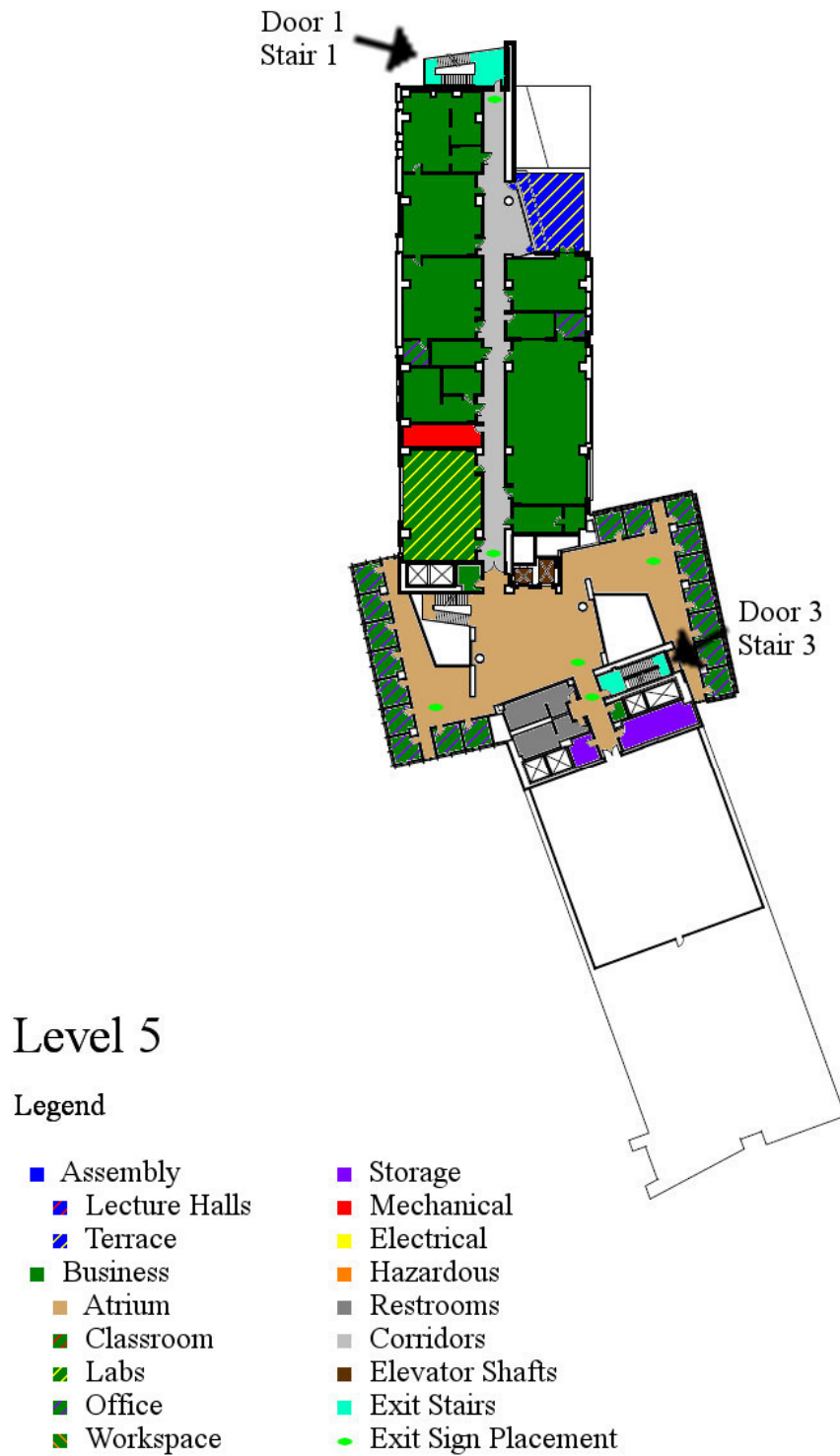


Figure e – Level 5 Occupancy Map



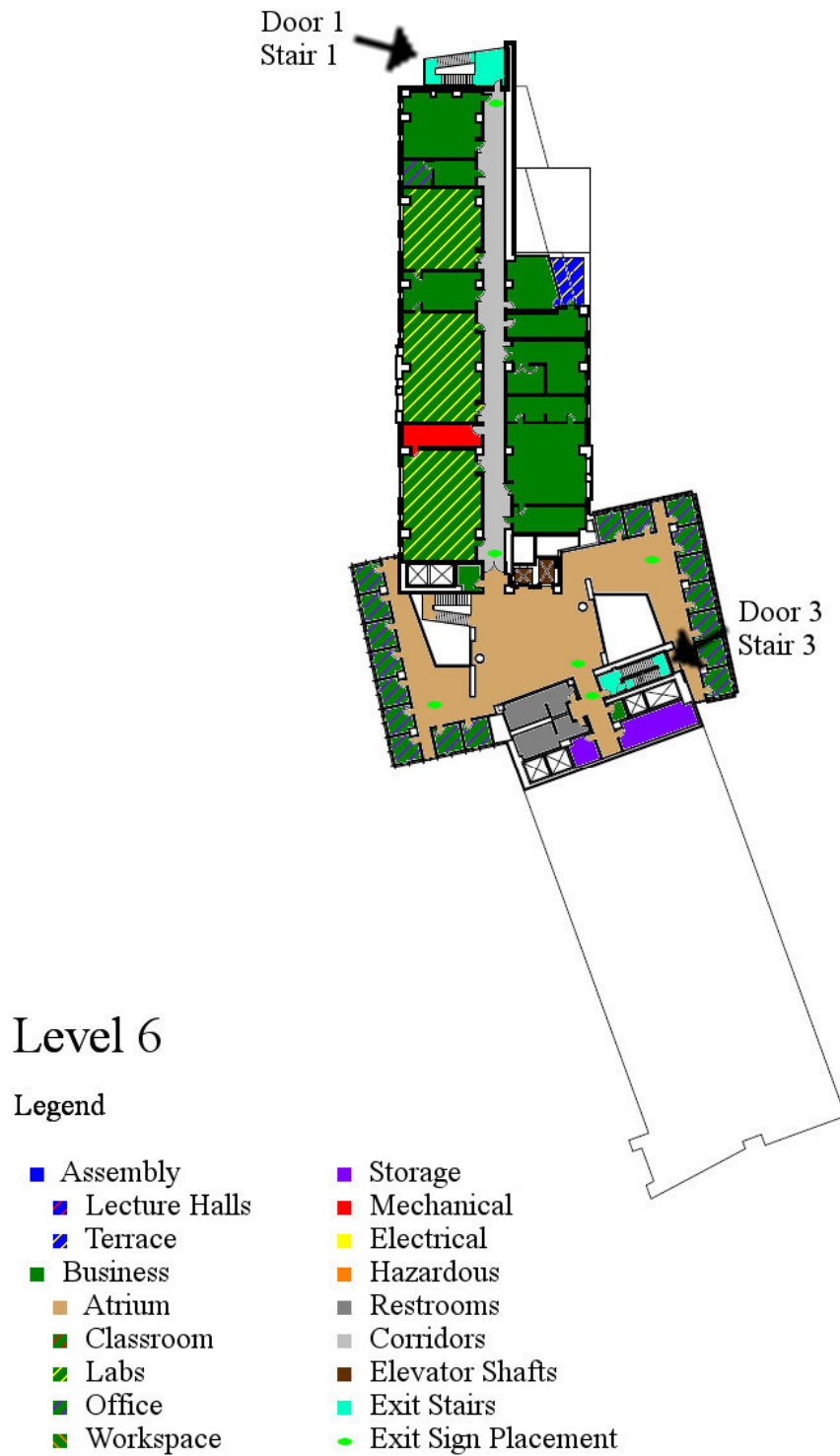


Figure f – Level 6 Occupancy Map



## **Fire Suppression System Analysis**

This section covers the analysis of the fire suppression system requirements using NFPA 13 Automatic Sprinkler Systems Handbook 2013 and NFPA 25 Standard for the Inspection, Testing, and Maintenance of Water-Based Fire Protection Systems 2014; the details of this analysis can be found in the sections listed below.

- System Design Criteria
- Water Supply
- Occupancy
- System Specification
- Hydraulic Calculations
- Inspection, Testing, and Maintenance

### **Analysis Summary**

The Center for Science is protected with a wet pipe sprinkler system throughout, designed to NFPA 13 2007. The occupancy classification of the building is primarily light hazard with a sprinkler density of  $0.10 \text{ gpm/ft}^2$ , but labs and utility spaces are ordinary hazard group 1 with a sprinkler density of  $0.15 \text{ gpm/ft}^2$ . The water supplied to the system is 914 gpm at a residual pressure of 55 psi, 60 psi static. The highest pressure demand at the base of the riser is 168 psi so a pump is required to meet the pressure demand. The fire pump is an in-line pump rated at 750 gpm, 113 psi, 58.1 HP, and has an efficiency of 85.3%; a pressure reducer is required for level 1. Water enters the system on each level through the riser located in the central portion of the building in stairway 3. The sprinklers are quick-response with a K-factor of 5.6 and are mostly pendant type with some upright type sprinklers in utility spaces. The sprinkler system is supported by hangers and braced against seismic motion using TOLCO braces. The system should be inspected, tested, and maintained following the procedures of NFPA 25 to ensure proper operation of the system.

The design of the fire suppression system in the Center for Science meets the NFPA 13 2013 requirements for a wet pipe sprinkler system to protect the types of occupancies present, light hazard and ordinary hazard group 1.



## **System Design Criteria**

### **System Type**

The fire suppression system installed in this building is a water-based sprinkler system. The system is a wet pipe sprinkler system where most of the system is concealed with a finished ceiling, but some portions are exposed. The requirements for wet pipe systems are covered in NFPA 13 Chapter 7.1.

### **Design Criteria**

Several design criteria must be met for the proper operation of a sprinkler system. The design criteria include the water supply and water demand, sprinkler spacing, location, and placement, system components and materials, and the support and bracing of the system. The sprinkler system was designed to NFPA 13 2007 standards, but it is analyzed in this report using NFPA 13 2013.

The water supply must be adequate for the sprinkler system. The flow rate and pressure of the water supply must meet or exceed the water demand of the system, fire pumps may be required to increase the pressure of the water supply. The water supply must also always be available in the event of a fire. On-site water storage, such as a water tank, may be required if the water supply lacks sufficient flow rate. Water supply information can be found in NFPA 13 Chapter 23.2 and water demand must be calculated for an individual system.

Sprinklers must be spaced properly so as not to exceed their maximum protection area. Sprinklers must be positioned so they are activated and water is distributed properly, obstructions may affect sprinkler activation and water distribution. Installation requirements for sprinklers are covered in NFPA 13 Chapter 8.

Proper materials must be used in the installation of a sprinkler system. Every component of a sprinkler system must be approved by a testing agency, such as ANSI, UL, or FM. Requirements of the components of a sprinkler system are listed in NFPA 13 Chapter 6.

A sprinkler system must be supported with restraints and braces. Support of the system is to prevent structural collapse of the piping and to increase the survivability of the system when there is building movement, such as in the event of an earthquake. The support of sprinkler systems is covered in NFPA 13 Chapter 9.



## Water Supply

The sprinkler system in this building is supplied by city water. Pressure was found at a nearby existing fire hydrant and flow was found at a different nearby fire hydrant. The static pressure was found to be 60 psi, the residual pressure was 55 psi, and the flow was 914 gpm (2270 gpm at 20 psi). The water supply has adequate flow rate, but the pressure is too low, so a fire pump is required. See appendix for locations of hydrants. The flow test summary is shown in Figure g.

<b>FLOW TEST SUMMARY</b>	
STATIC PSI	<u>60</u>
RESIDUAL PSI	<u>55</u>
PITOT PSI	<u>35</u>
ORIFICE DIAMETER	<u>2 1/2</u>
COEFFICIENT OF DISCHARGE	<u>0.9</u>
GPM	<u>914</u>
DATE <u>8-19-2011</u>	
LOCATION <u>N. POLY VIEW DRIVE</u>	
BY WHO <u>FLUID RESOURCE MANAGEMENT, INC.</u>	
<b>ADJUSTED FLOW 10 % REDUCTION</b>	
STATIC PSI	<u>54</u>
RESIDUAL PSI	<u>49</u>
GPM	<u>914</u>
<b>STATIC &amp; RESIDUAL TAKEN FROM HYD. # 63</b> <b>FLOW TAKEN FROM HYD. # 64</b>	

Figure g – Flow Test Summary



## **Occupancy**

### **Classifications**

Most areas of the building are considered light hazard occupancy as defined in NFPA 13 Chapter 5.2. The labs, storage, and utility rooms are considered ordinary hazard group 1 as defined in NFPA 13 Chapter 5.3. The storage occupancies on each floor are incidental and are therefore considered miscellaneous storage as defined in NFPA 13 Chapter 3.9.1.18. The actual commodity classifications for the storage occupancies are unclear in the plans, but if the system was designed properly the commodities could be Classes I or II from NFPA 13 Table 13.2.1 because the design curve used is ordinary hazard group 1.

### **Sprinkler Design Criteria**

The sprinkler density for the light and ordinary hazard is 0.10 and 0.15 gpm/ft<sup>2</sup>, respectively, with a design area of 1500 square feet. The chosen sprinkler area and density satisfies the design curves in NFPA 13 Figure 11.2.3.1.1. The hose stream allowance of 100 gpm for light hazard and 100 gpm inside and 150 gpm outside for ordinary hazard meet the requirements of NFPA 13 Table 11.2.3.1.2.



## **System Specifications**

All components of the system are shown in the sprinkler drawings in the appendix.

### **Fire Pump**

A fire pump is required in this building to meet the hydraulic demand of the sprinkler system, see Hydraulic Calculations. The fire pump is an in-line pump with a rated flow of 750 gpm, rated head of 113 psi, rated power of 58.1 hp, and rated efficiency of 85.3%. Due to the high pressure from the fire pump, a pressure reducer is required for level 1.

### **Stand Pipes and Risers**

There are a total of three stand pipes and one riser in this building. The standpipes are in stairways 1, 4, and 5 and the riser is in stairway 3, all of these pipes are concealed inside a wall. Stand pipe 1 and the riser are 6" Schedule 10 and standpipes 4 and 5 are 4" Schedule 10.

### **Cross Mains and Branch Lines**

The cross mains in this building are generally found above corridors that run along the building's center with branch lines running perpendicular to the corridors, passing into rooms to pass water to the sprinklers. This pattern allows for simple layout of branch lines and easy access for maintenance of the cross mains should the need arise. The cross mains are 2½" Schedule 10, but one section of the cross main on level 1 is 3" Schedule 10 as it leaves the pump room and splits into two cross mains. The branch lines range between 1" and 1¼" Schedule 10, depending on hydraulic demand.

### **Sprinklers**

In the areas of this building with a finished ceiling the sprinklers are pendant type and most utility spaces and some labs have upright type sprinklers. All sprinklers are quick response and have a K-factor of 5.6.

### **Hangers and Seismic Bracing**

The sprinkler system is supported by hangers and braced using TOLCO seismic braces. The seismic design category for this building is D and the site has a soil profile of type B, the spectral response accelerations are  $S_s$  of 1.26 and  $S_1$  of 0.481, and the seismic coefficient  $C_p$  is 0.61.



## Hydraulic Calculations

The hydraulic calculations performed for this building are nearly 200 pages long so only some of these calculations are in the appendix. Calculations for the fire pump, pressure reducers, and, for brevity, only the remote area with the highest hydraulic demand are in the appendix. Blank pages and pages that were not used for final design values, such as pages with only crossed out graphs for the pressure reducer, are omitted from the calculations.

The water demand at the base of the riser depends on which remote area is chosen. The system should be designed to meet the highest pressure demand, which is 168 psi. Table 3a summarizes the results of the remote area hydraulic calculations and highlights the maximum demand.

Table 3a – Remote Area Pressure Calculation Summary

Remote Area		Pressure (psi)		
Level	No.	Demand	Safety	Outlet
1	1	130.2	45.8	176.0
	<b>2</b>	<b>167.6</b>	<b>7.2</b>	<b>174.8</b>
3	1	122.0	53.2	175.2
	2	126.6	48.8	175.4
6	1	135.3	40.1	175.4
	2	71.6	105.1	176.7
	3	149.5	25.5	175.0
	4	160.6	13.6	174.2

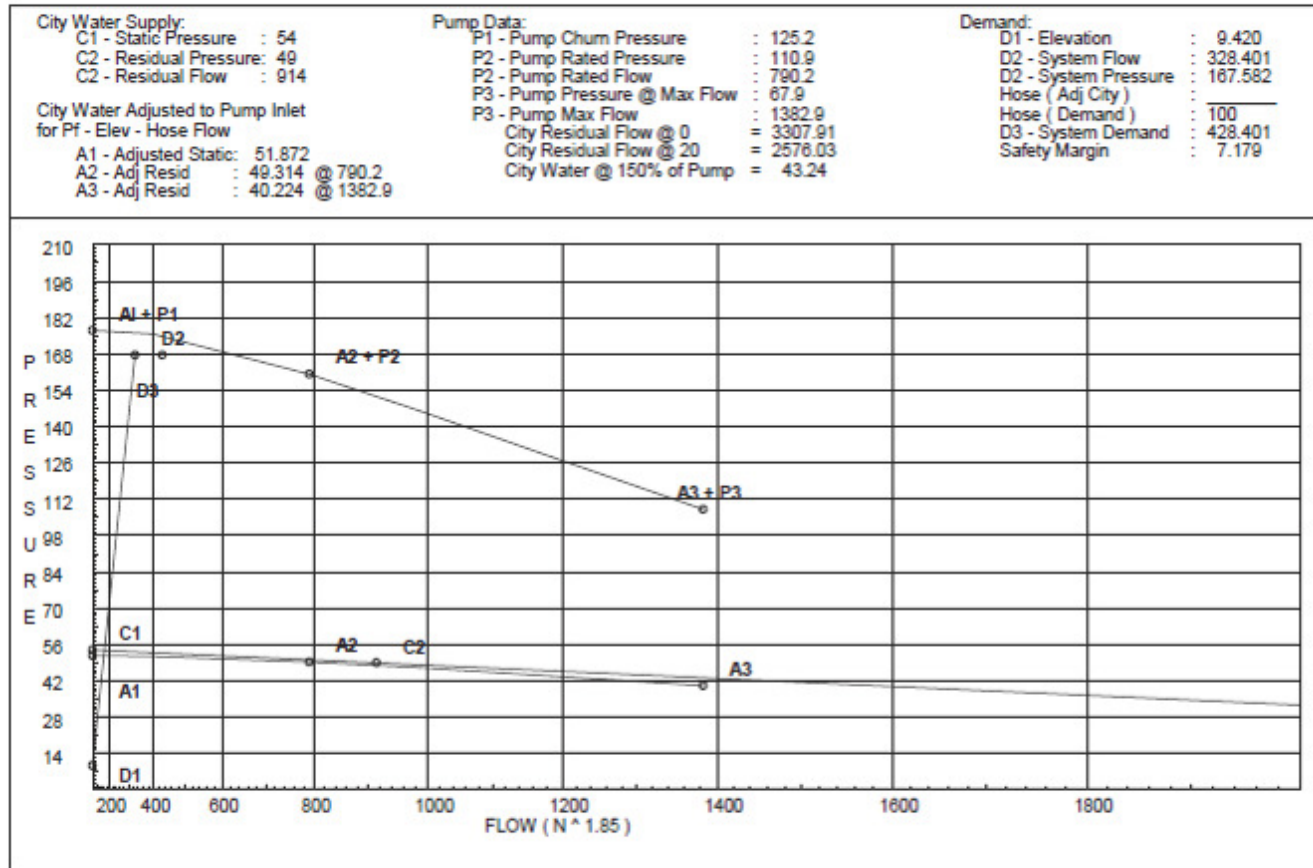
No significant errors were found in the hydraulic calculations for any remote area of the sprinkler system in this building. Figure h on the next page shows the water supply curve for remote area 2 on level 1, the remote area with the highest pressure demand. The pressure of the water supply curve does not exceed the highest pressure demand of the water demand curve, but the pressure of the combined water supply curve, which includes the pressure rise from the fire pump, does exceed the highest pressure demand of the water demand curve for this remote area so the system meets the highest pressure demand.



## Water Supply Curve (C)

Aero Automatic Sprinkler Co.  
Cal Poly Center for Science LVL 1 [R/A=2]

Page 2  
Date 9-25-11



Computer Programs by Hydratec Inc. Route 111 Windham N.H. USA 03067

Figure h – Water Supply Curve of Remote Area with Highest Pressure Demand



## Inspection, Testing, and Maintenance

NFPA 25 Chapter 5 covers the inspection, testing, and maintenance requirements for sprinkler systems. Table 3b summarizes the requirements of NFPA 25 Table 5.1.1.2 for the wet pipe sprinkler system present in this building. The requirements for control valves and fire department connections found in NFPA 25 Table 13.1.1.2 are also included. All chapters referenced are the applicable chapters from NFPA 25.

Table 3b – ITM Requirements

Component	Activity	Frequency	Reference
Control Valves	Inspection	Monthly (tamper switch)	13.3.2.1.1
	Testing	Annually (position and operation)	13.3.3.1
	Maintenance	Annually	13.3.4
Check Valves	Inspection	5 years (interior)	13.4.2.1
Pressure-Reducing Valves	Inspection	Quarterly (sprinkler systems)	13.5.1.1
	Testing	5 years (sprinkler systems)	13.5.1.2
Gauges	Inspection	Quarterly	5.2.4.1
	Testing	5 years	13.2.7.2
Hydraulic Nameplate	Inspection	Quarterly	5.2.6
Hanger / Seismic Bracing	Inspection	Annually	5.2.3
Pipe and Fittings	Inspection	Annually	5.2.2
Sprinklers (Fast Response)	Inspection	Annually	5.2.1
	Testing	At 20 years and every 10 years thereafter	5.3.1.1.1.3
Spare Sprinklers	Inspection	Annually	5.2.1.4
Information Sign	Inspection	Annually	5.2.8
Fire Department Connections	Inspection	Quarterly	13.7.1
Obstruction, internal inspection of piping	Inspection	5 years	14.2
Main Drains	Testing	Annually/Quarterly	13.2.5 13.2.5.1 13.3.3.4
Obstruction	Investigation	Per Chapter 14.3	14.3



## **Fire Alarm, Detection, and Communication Systems Analysis**

This section covers the analysis of the fire alarm, detection, and communication systems requirements using NFPA 72 National Fire Alarm and Signaling Code 2013 and the International Building Code (IBC) 2012; the details of this analysis can be found in the sections listed below.

- Fire Alarm System
- Fire Detection System
- Inspection, Testing, and Maintenance

The NFPA Fire Protection Handbook, 20<sup>th</sup> edition is also referenced in this section concerning audible signaling.

### **Analysis Summary**

The Center for Science has a fire alarm system with in-building EVACS and a smoke detection system. The alarm system covers all spaces in the building and consists of audible and visual alarm devices. Initiation devices for the alarm system include manual pull stations, waterflow alarm devices, and the smoke detection system. The smoke detection system relies on duct smoke detection for most spaces of the building and the sprinkler system, present throughout the building, will trigger a waterflow alarm independent of smoke detection. Batteries for secondary power ensure the system will continue to function for 24 hours in standby and 15 minutes in alarm if there is a power loss. A fire scenario was selected using the probabilistic approach by using statistical data on fires that occurred in similar buildings. Regular inspection, testing, and maintenance schedules should be followed to ensure the proper operation of the system.

The design of the fire detection, alarm, and communication systems in the Center for Science meets the NFPA 72 2013 requirements for a fire alarm system and smoke detection system.



## **Fire Alarm System**

### **System Type**

The fire alarm system installed in this building is a fire alarm with in-building fire emergency voice alarm communication system (EVACS). There is no mass notification system (MNS) present in this building.

### **Device Design Criteria**

In a fire scenario, occupants must be able to hear or see alarm indicating devices over ambient audible or visual noise in a space. The audible/visual devices in this building are wall mounted speakers and strobes. The EVACS should be designed to alert all occupants during an emergency situation and inform them of necessary actions.

Audibility requirements found in NFPA 72 Section 18.4.3 state that the audible devices must have a sound level at least 15 dB above the average ambient sound level. Average ambient sound levels by occupancy are found in NFPA 72 Table A.18.4 and for this building, which is primarily Assembly and Business occupancies, it is 55 dBA. Using these two references, the minimum sound level for speakers in this building is 70 dBA.

Audible device location criteria is found in NFPA 72 Section 18.4.8 and states that wall-mounted appliances must be 90 inches or more above the finished floor and 6 inches or more below the finished ceiling. Mounting details for the speakers (without strobes) in this building are not shown in the plans.

Visible signaling requirements are found in NFPA 72 Section 18.5. Visible devices must have a minimum light output based on the room size per NFPA 72 Table 18.5.5.4.1(a) for wall-mounted devices.

Visual device location criteria is found in NFPA 72 Section 18.5.5 and states that wall-mounted appliances must not be less than 80 inches and not greater than 96 inches above the finished floor. This location criterion is properly shown in the details for the wall strobe and wall speaker strobe installations.

The EVACS requirements are found in NFPA 72 Section 24.4.2. The location of the paging microphone station at the FACU seems to be adequate for the requirements of NFPA 72 Section 24.4.2.5. No other information about the EVACS is given in the plans so it may or may not meet all NFPA 72 requirements for an EVACS.



## System Devices

The fire alarm control panel (FACP) is located in the main electrical / transformer room on the first level (room 122) and there are fire alarm terminal cabinets (FATC) on floors 2, 3, 4, and 5 located in utility spaces (electrical or telecommunication rooms). The FACP manufacturer is Honeywell Notifier and its model number is NFS2-640.

The fire alarm system devices consist of 73 strobes, 13 speakers (7 of which are weather proof), 165 speaker/strobes, 29 trouble monitors (non-alarm points), and 7 waterflow alarm devices. There is at least one fire alarm device located in each space in this building. Voltage drop calculations for each circuit and secondary power (battery) calculations from the plans are shown in the appendix.

The EVACS has 1 voice alarm channel, 172 speakers, and 9 speaker circuits with amplification and sound-processing equipment located in the electrical rooms at the FAPS locations and the location of the paging microphone station is at the fire alarm control unit (FACU) in room 122.

For each strobe, the number of candelas in each space is known so NFPA 72 Table 18.5.5.4.1(a) can be used to determine the maximum room size. The square footage of each room can be found on the life safety plans in the appendix so the light output of each strobe can be verified based off of square footage assuming a square-shaped room, which most rooms in this building are nearly square in shape. All strobes meet or exceed the required light output for each room based on square footage.

For each speaker, the wattage is known, but the sound level must be determined from manufacturer specifications for the given model number. The speaker and speaker/strobe model numbers are SPW and SPWS, respectively. The 2 W speaker/strobe has a sound level of 85 dBA and the 1 W speaker/strobe has a sound level of 82 dBA. These sound levels are rated at 10 feet from the device, but it is important that the sound level be at least 70 dBA at every point in a room. Using the 6 dBA rule in the NFPA Fire Protection Handbook, both devices can meet 70 dBA at 40 feet. Since every point in each room is within 40 feet of an audible device, the audible signaling requirements are met for the speaker/strobes. The speakers have a higher dBA rating than the speaker/strobes so they also meet the audible signaling requirements.



**Alarm Signals and Secondary Power**

Signal disposition information for supervisory, trouble, and alarm conditions is found in the sequence of operations matrix on the plans (See FA-0). Each signal is indicated at the fire alarm control unit (FACU) during certain events. The signaling pathways in this building are class B, survivability level 1.

The signaling pathway system as described in the plans must meet the requirements of NFPA 72 Section 12.3.2 to be a class B system. The survivability of the system is level 1 as defined in NFPA 72 Section 12.4.2 because the building is fully protected by an automatic sprinkler system.

Secondary power supply requirements are found in NFPA 72 Section 10.6.7. The battery calculations on the plans meet the requirements of NFPA 72 in that the calculations satisfy NFPA 72 Sections 10.6.7.2.1(1) for a 20 percent safety factor to the calculated amp-hour rating and 10.6.7.2.1(2) for the system is capable of operating in standby for 24 hours and in alarm for 15 minutes.



## **Fire Detection System**

### **System Type**

The building has an automatic fire detection system using smoke detection and sprinklers, which essentially operate as heat detectors which trigger a waterflow alarm upon activation. Smoke detection is limited to ducts, which connect to every space as part of the HVAC system, the atrium, elevator lobbies, and some utility spaces, such as at the FACP. There are no heat detectors, flame detectors, or gas detectors as part of the detection system.

### **Design Criteria**

NFPA 72 does not specify which spaces initiating devices are required in, but refers to other governing laws, codes, or standards in NFPA 72 Section 17.4.5 to give those requirements. Initiating device placement requirements for this building can be found in IBC Section 907.4.

A single smoke detector is required at the FACU per IBC Section 907.4.1. Manual pull station location requirements are in IBC Section 907.4.2.1 and must be placed within 5 feet of any exit and travel distance to any manual pull station must be less than 200 feet. The height requirement of the manual pull stations is in IBC Section 907.4.2.2 and must be at a height between 42 and 48 inches.

The requirements for smoke-sensing fire detectors are found in NFPA 72 Section 17.7. As with other initiating devices, NFPA 72 refers to other governing laws, codes, or standards for the required placement of smoke detectors in NFPA 72 Section 17.7.1.6. Spot-type smoke detector, duct smoke detector, and beam smoke detector requirements are given in NFPA 72 Sections 17.7.3.2, 17.7.5, and 17.7.3.7 respectively.

Spot-type smoke detectors are only installed in certain areas so the spacing requirements in NFPA 72 do not apply. The installation location requirement of NFPA 72 Section 17.7.3.2.1 states smoke detectors must be installed on ceilings or 12 inches from the ceiling if installed on a sidewall. Duct smoke detectors for the control of smoke spread have requirements listed in NFPA 72 Section 17.7.5. Requirements for beam smoke detectors are listed in NFPA 72 Section 17.7.3.7.



**System Devices**

The initiating devices for the detection system for this building consist of 31 manual pull stations, 18 photoelectric smoke detectors, 62 photoelectric duct smoke detectors, and beam smoke detectors (23 transmitters and 15 receivers).

The manual pull stations are located within 5 feet of each exit door in this building, including the exit doors for each stairway, and at stairway 2 on levels 3 through 6. Travel distances to each exit are less than 200 feet so manual pull stations need only be placed at exits, no intermediate placements are required. Manual pull stations are at a height of 48 inches from the floor. The manual pull stations present in this building meet the requirements of the IBC.

Smoke detectors are not evenly spaced throughout this building. Photoelectric spot-type smoke detectors are located on the ceiling at each elevator lobby, at the FACP in room 122, and in some mechanical/electrical utility spaces. Photoelectric duct smoke detectors are installed within HVAC ducts and their placements correlate with the HVAC system to detect smoke from any duct and close dampers to prevent the spread of smoke.

Beam smoke detectors are located in the atrium on multiple floors; from the placements of beam transmitters and receivers, the beams do not appear to go between floors. No mirrors are used for the beams and maximum beam lengths are not exceeded.



## **Inspection, Testing, and Maintenance**

NFPA 72 Chapter 14 covers the inspection, testing, and maintenance requirements for fire alarm systems. The visual inspection requirements are covered in NFPA 72 Section 14.3 and summarized in Table 4a on the next page, which is based on NFPA 72 Table 14.3.1. Sections referenced are the applicable sections from NFPA 72.

Testing requirements are found in NFPA 72 Section 14.4. Testing methods are located in NFPA 72 Table 14.4.3.2, which indicates the frequency and methods for testing all equipment and devices. NFPA 72 Table 14.4.3.2 is too lengthy to be summarized here.

Maintenance requirements are located in NFPA 72 Section 14.5 and are much more general than the inspection and testing requirements. NFPA 72 Sections 14.5.1 through 14.5.3 state that maintenance should be in accordance with the manufacturer's published instructions and the frequency of maintenance and cleaning of system equipment depends on the type of equipment and the local ambient conditions.



Table 4a – Visual Inspection Summary

Component	Frequency	Method	Reference
All equipment	Annually	Ensure there are no changes that affect equipment performance. Inspect for building modifications, occupancy changes, changes in environmental conditions, device location, physical obstructions, device orientation, physical damage, and degree of cleanliness.	14.3.4
Control Equipment Fuses Interface equipment Lamps and LEDs Primary (main) power supply Trouble signals	Annually Annually Annually Annually Semiannually	Verify system normal condition	
Supervising station alarm systems - transmitters Digital alarm communicator transmitter (DACT)	Annually	Verify location, physical condition, and a system normal condition	
In-building fire emergency voice / alarm communications equipment	Semiannually	Verify location and condition	
Batteries Sealed lead-acid (SLA)	Semiannually	Inspect for corrosion or leakage. Verify tightness of connections. Verify marking of the month/year of manufacture.	10.6.10
Remote annunciators	Semiannually	Verify location and condition	
Notification appliance circuit power extenders	Annually	Verify proper fuse ratings, if any. Verify that lamps and LEDs indicate normal operating status of the equipment.	10.6
Initiating devices Duct detectors  Manual fire alarm boxes Smoke detectors Projected beam smoke detectors Supervisory signal devices Waterflow devices	Semiannually  Semiannually Semiannually Quarterly Quarterly	Verify detector is rigidly mounted. Confirm that no penetrations in a return air duct exist in the vicinity of the detector. Confirm the detector is installed so as to sample the airstream at the proper location in the duct.  Verify beam path is unobstructed	17.7.5.5
Notification appliances Audible appliances Visible appliances	Semiannually Semiannually	Verify that the candela rating marking agrees with the approved drawings	18.5.5
Supervising station alarm systems - receivers Signal receipt Receivers	Daily Annually	Verify receipt of signal Verify location and normal condition	



## **Performance Based Analysis**

The following sections of this report cover the performance based analysis. These sections analyze a typical fire scenario and cover the engineering analysis of the atrium. Each section summarizes the results and assumptions of the performance based analysis. The performance based sections are listed below.

- Typical Fire Scenario Selection
- Atrium Analysis

These performance based sections use a combination of current codes and standards for the design analysis, which are listed below.

- International Building Code (IBC) 2012
- NFPA 101 Life Safety Code Handbook (LSC) 2012
- NFPA 72 National Fire Alarm and Signaling Code 2013
- NFPA Fire Protection Handbook, 20<sup>th</sup> edition
- SFPE Handbook of Fire Protection Engineering, 4<sup>th</sup> edition



## Typical Fire Scenario Selection

### Design Methodology

Design methods for establishing fire scenarios are found in NFPA 72 Annex B. NFPA 72 Section B.2.3.2.1.1 gives some examples of analysis techniques used to identify fire scenarios and classifies fire scenarios as either probabilistic or deterministic. Probabilistic approaches can be based on fire statistics, past history, hazard/failure analysis, etc. and deterministic approaches use analysis or engineering judgment based on chemistry, physics, or correlations based on experimental data.

The probabilistic approach is used here to determine likely fire scenarios based on statistical data of fires in buildings of similar use. For this statistical data, the NFPA report “Structure Fire in Educational Properties” (Richard Campbell, 2013) concerning structure fires in college classroom buildings and adult education centers. The data uses an estimated 700 fires involving college classroom buildings and adult education centers per year in 2007-2011.

### Fire Risk

Using Table 4C in the NFPA report, Table 5a was generated and shows the leading causes of fire in college classroom buildings and adult education centers, their contribution to the total percentage of fires and damage, and a risk factor, which is the product of those percentages.

Table 5a – Leading Fire Causes in College Classroom Buildings and Risk Factors

Cause	Fires (%)	Damage (%)	Risk Factor
Cooking equipment	51	2	102
Intentional	10	10	100
Heating equipment	8	8	64
Smoking materials	5	0	0
Electrical distribution and lighting equipment	5	18	90

The risk factor is an attempt to quantify the risk of a fire, which is explained in NFPA 72 B.2.3.1.1.2 by multiplying the probability of occurrence by the consequences (damages) of a fire. Using this simple method, the risk factor can be used to select fire scenarios, where higher risk factors indicate a higher risk fire that should be considered more seriously in the analysis; no fire scenario should necessarily be ruled out by this risk factor, but more attention should be given to higher risk fire scenarios.

A fire could be caused by any of the listed causes or one not included on the chart, but, from the risk factor, the fire scenarios that should be given greater attention are cooking, intentional, and electrical fires. Although a fire caused by heating equipment or smoking materials could occur, their risk factors are lower; further thought about these fire causes can support not selecting them as fire scenarios.



Heating equipment, such as a space heater, is unlikely to be present considering that San Luis Obispo does not get that cold in the winter. There is a risk of smoking materials lighting a fire anywhere in nearly any occupancy, but the statistics indicate that property damage is not high in comparison to the other fire causes, which means these fires do not tend to spread far before being extinguished.

Location of a fire is also important in determining fire scenarios. Using Table 8C in the NFPA report, Table 5b was generated and shows the areas of origin of non-confined fires in college classroom buildings and adult education centers for areas present in this building; their contribution to the total percentage of fires, injuries, and damage; and a risk factor, which is the product of fires percentage and the greater of injuries or damage percentage.

Table 5b – Fire Area of Origin in College Classroom Buildings and Risk Factors

Area of Origin	Fires (%)	Injuries (%)	Damage (%)	Risk Factor
Cooking area	2	16	2	32
Bathroom	2	0	1	2
Laboratory	3	44	18	54
Hallway or corridor	1	0	0	0
Office	2	0	8	16
Duct for HVAC	1	0	0	0
Machinery room	2	0	1	2
Small assembly area (< 100 persons)	1	0	1	1
Terrace	0	0	0	0

The risk factor includes injuries, if applicable, as a way to further quantify the risk of a fire. Although the injuries in the statistics may only be caused by the ignition of a fire, they may also indicate that a fire is more severe, spreading quickly before occupants can escape.

A fire can occur in any area of the building, but the areas at the greatest risk of having a fire that may cause more harm or damage than in other areas are laboratories, cooking areas, and offices.



## Fire Scenario Selection

Combining the likely causes of fires with the likely areas of origin of fires considerably reduces the number of choices for fire scenarios. However, a selection of a fire scenario still must be made. Considering the causes and locations of higher risk fires, two different reasonable fire scenarios that have a high fire risk are a cooking appliance fire in a cooking area and a laboratory equipment fire.

Although this building does not have a kitchen or other designated cooking area, it is possible that a study room, club room, or faculty office may have a small cooking appliance, such as a microwave, toaster, or coffee maker. This building has labs with various types of laboratory equipment, such as oscilloscopes and spectrometers.

Unfortunately, there is no test data for microwaves or other small kitchen appliances nor is there any fire test data for laboratory equipment. The most similar appliance found, for which test data exists, was a television; while not exactly like a microwave or an oscilloscope, it has electronic components encased in a plastic shell.

For the data, the study titled “Burning of Electrical Household Appliances: An Experimental Study” (J. Hietaniemi, J. Mangs, and T. Hakkarainen, 2001) was used. The study generated curves for each of 3 television sets, TV3 was the smallest so its data is used. Assuming the fire is a t-squared curve and using Excel to find a curve to fit the data for the TV3 curve in the study, the fire growth time to reach 1055 kW, defined in NFPA 72 Section B.2.3.2.3.2, is about 3.2 minutes (this time assumes the fire becomes a t-squared fire at 2.5 minutes into the test). TV3 never reached a heat release rate (HRR) of 1055 kW, but it is assumed that the fire would spread to other nearby devices or other objects, continuing to grow until being suppressed.

Using the value of fire growth time with the approximate ceiling height of 10 feet 6 inches and assuming the sprinklers act as heat detectors, since there are no smoke detectors in the labs, spaced at 10 feet with a calculated RTI of  $266 \text{ m}^{1/2}\text{s}^{1/2}$  based on their activation temperature of 155 °F (68.3 °C), the fire will be detected when the waterflow alarm is triggered by sprinkler activation. Using the DETACT model, the calculated time of detection is about 210 seconds and the fire will be about 1300 kW at detection. DETACT results are shown on Table 5c and Figure i on the next page. The DETACT model shows that the gas temperature in the space is 151 °C, which is not approaching flashover temperatures, when the fire is detected so the fire protection in this space is acceptable for this fire scenario.



Table 5c – DETACT Equipment Fire Detection Time

Calculation time (s)	HRR	Gas temp	Det. temp
0	0	20	20
30	26	30	20
60	106	45	22
90	238	62	26
120	423	82	32
150	660	104	41
180	951	127	52
<b>210</b>	<b>1294</b>	<b>151</b>	<b>66</b>
240	1690	176	82
270	2139	203	101
300	2641	231	122
330	3196	259	145
360	3803	288	169
390	4464	319	196
420	5177	350	224
450	5943	381	253
480	6762	414	283

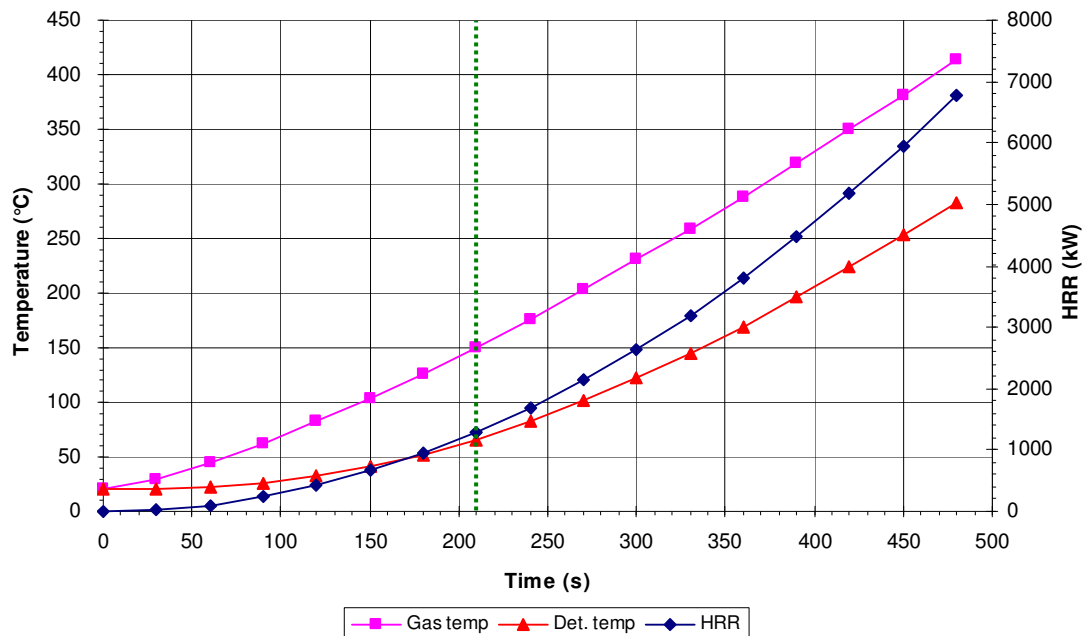


Figure i – DETACT Equipment Fire Room Conditions at Detection



Another important fire scenario for the laboratory, although it is not reflected in the statistical data, is a chemical fire that may be caused intentionally or accidentally from an experiment or demonstration gone awry. There are numerous flammable chemicals that could possibly be in the laboratory and many different fuel configurations so the fire is modeled generally as a t-squared ultrafast developing fire. No maximum is placed on the HRR because the fuel configuration is unknown and would only be assumed to be limited when the sprinklers activate.

Using the DETACT model, with the same spatial parameters as the laboratory equipment fire, the calculated time of detection for the chemical fire is about 115 seconds and the fire will be about 2500 kW at detection. DETACT results are shown on Table 5d and Figure j on the next page. The DETACT model shows that the gas temperature in the space is 222 °C, which is not approaching flashover temperatures, when the fire is detected so the fire protection in this space is acceptable for this fire scenario.



Table 5d – DETACT Chemical Fire Detection Time

Calculation time (s)	HRR	Gas temp	Det. temp
0	0	20	20.0
10	19	28	20.1
20	75	40	20.6
30	169	54	21.6
40	300	69	23.4
50	469	86	26.0
60	675	105	29.6
70	919	124	34.2
80	1200	144	39.8
90	1519	166	46.6
100	1876	188	54.5
110	2269	210	63.6
<b>115</b>	<b>2480</b>	<b>222</b>	<b>68.5</b>
125	2931	246	79.4
135	3418	270	91.3
145	3943	295	104.5
155	4506	321	118.8

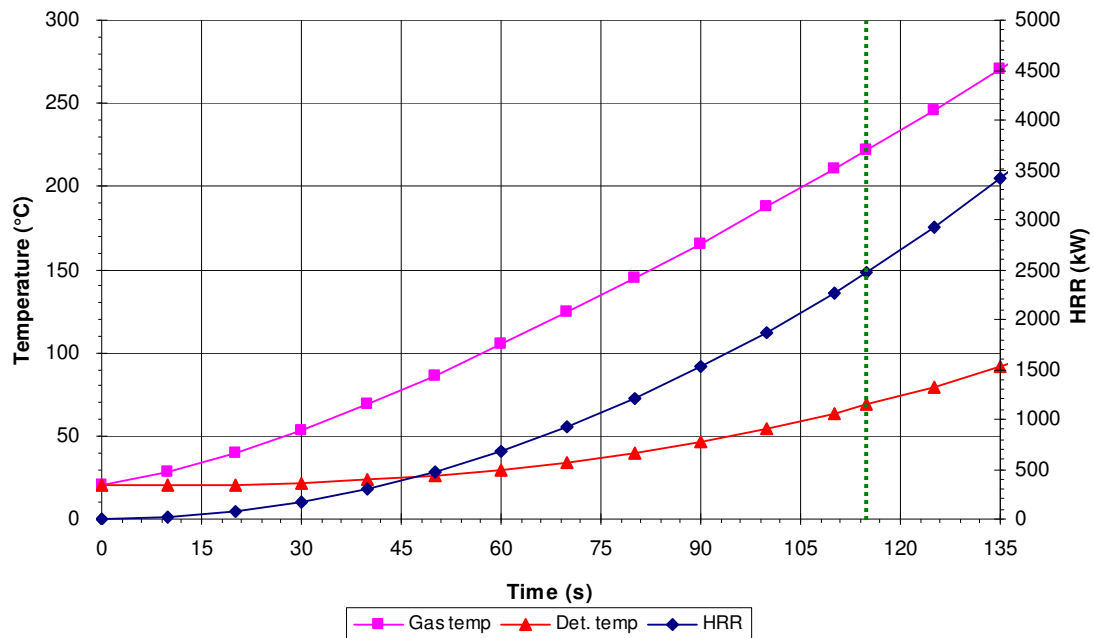


Figure j – DETACT Chemical Fire Room Conditions at Detection



## **Atrium Analysis**

An engineering analysis of the atrium must be performed to meet LSC Section 8.6.7. The goal of this analysis is to show that a tenable environment is maintained for the duration required by the LSC. To accomplish this goal, the Consolidated Model of Fire and Smoke Transport (CFAST) and Fire Dynamics Simulator (FDS) were used to model a fire that impacts the tenability of the atrium. The details of the atrium analysis are covered in the sections listed below.

- Tenability
- CFAST
- FDS

## **Analysis Summary**

The tenability criterion for the atrium is to keep the smoke layer 6 feet above the floor. The atrium is naturally ventilated from roof vents and exterior doors. There are two likely paths occupants can take to exit the building with a required safe egress time for any occupant between 76 and 206 seconds. Two fire scenarios were modeled in CFAST and one in FDS. A t-squared ultrafast 3500 kW office fire was modeled using CFAST and a t-squared medium 700 kW chair fire in the atrium was modeled using both models. A fire in an adjacent office that spills smoke into the atrium will cause a tenability failure earliest at 180 seconds, but occupants of all floors have sufficient available time to safely egress because the EVACS can be used to inform certain occupants to take alternative paths. The chair fire in the atrium is not well modeled in CFAST because a two-zone model does not adequately account for the physics of connected compartments that form a single large open space. The FDS model of the chair fire in the atrium should be considered more accurate than the CFAST model for this chair fire. The FDS model for the chair fire in the atrium shows this fire scenario meets tenability requirements. FDS could give a more detailed analysis of the office fire, but the results from CFAST are adequate for the atrium analysis.

Based on the results of the CFAST and FDS models, the atrium meets the tenability requirements of LSC 2012.



## **Tenability**

### **Smoke Control**

The most general tenability criterion is stated in LSC Section 5.2.2 that any occupant not intimate with ignition shall not be exposed to untenable conditions. For the atrium, the primary tenability concern is to keep the smoke layer interface at least 6 feet above the floor long enough to allow occupants to egress.

The smoke control system in the atrium is a passive natural ventilation system. There are four 120"x60" roof vents and, when a fire is detected, interior hallway doors to the atrium close and the exterior entrance/exit doors to the atrium open.

### **Egress Time**

Occupants must not be exposed to untenable conditions so sufficient time must be allowed for them to exit the building. The available safe egress time (ASET) is the time occupants have before they are likely exposed to untenable conditions and this time must exceed the required safe egress time (RSET), which is how long occupants take to exit the building. ASET is determined in the fire models and RSET can be calculated as the sum of the pre-movement (delay) time and travel time. RSET varies based on where the occupant is in the building and to which exit the occupant travels. A margin of safety should also be applied when comparing ASET and RSET because of the uncertainty in the models and in calculating how people are likely to react in an emergency scenario. Based on values found in the LSC, the margin of safety is taken to be 1.5 in this report.

Using the method in the egress section of this report for calculating total evacuation time, RSET can be calculated. In this calculation, the number of occupants should be limited to only those in and adjacent to the atrium by using the EVACS to route other building occupants away from stair 3 in the atrium. Queuing is assumed to not occur because of the limited number of occupants. The evacuation time for the offices can be determined if the path taken by occupants is known. For the offices above level 2 in the atrium, there are two primary paths occupants could take. Path 1 is from the offices to stair 3, to level 2, then to the exit in the atrium. Path 2 is from the offices to the East or West wings of the building through the hallway doors in the atrium, through which occupants are assumed to have exited the building for the purpose of calculating RSET. The RSET calculations for paths 1 and 2 are summarized in Tables 6a and 6b, respectively, on the next page and do not include the safety factor.



Table 6a – Path 1 Evacuation Time

RSET Action		Time (s)
Delay		36
Travel	to exit stair 3	40
	from level 6 to level G2	114
	to exit door	16
<b>Total</b>		<b>206</b>

Table 6b – Path 2 Evacuation Time

RSET Action	Time (s)
Delay	36
Travel to atrium exit door	40
<b>Total</b>	<b>76</b>



## CFAST

### Model Details

CFAST is a two-zone model that assumes a hot upper gas layer and a cooler lower gas layer in every compartment; the hot upper gas layer is assumed to be the smoke layer. It is not possible to model complex geometries or ventilation conditions in CFAST.

The atrium was modeled in CFAST as 25 individual compartments connected by horizontal and vertical vents. Each level is defined with a single large 12 foot tall rectangular compartment of equal area to that level of the atrium, two smaller 9.5 foot tall compartments to represent the East and West hallways that connect the atrium to the rest of the building, and two 4 foot tall compartments to represent the North and South vertical openings that define the atrium.

Smoke detectors were placed at approximate locations in the atrium of each duct on levels 2 and 3 and in the vertical openings to represent beam smoke detectors, which CFAST. The smoke-temperature correlation is used in the model as the smoke detection basis where a 13 °C rise in temperature activates the detector.

The atrium is naturally ventilated with interior doors to the hallways initially open and exterior doors on level 2 initially closed. When the fire is detected, the interior doors close and exterior doors open, the ducts to the atrium also close.

Two fire scenarios were modeled in CFAST: an office fire on level 6 with the door forced open that spills smoke into the atrium and an upholstered chair fire on the level 2 (ground level) of the atrium.

The office is modeled as another compartment and has a single sprinkler and a duct that is monitored by a duct detector. The fire selected for the office is a 3-panel workstation, which is represented by a t-squared ultrafast developing fire with a maximum heat release rate (HRR) of 3500 kW. The fire is placed on the far wall away from the sprinkler and duct.

The furniture present in the atrium consists of chairs, couches, and tables. From pictures of the space, the chairs and couches appear to have minimal upholstery and the tables appear to be non-combustible. From fire test data similar to the kind of chairs present, the fire selected is a t-squared medium growth rate fire with a maximum HRR of 700 kW. It is assumed that the couches have similar flammability characteristics to the chairs. The fire is placed at a wall where furniture is seen in pictures of the atrium, equal distance from sprinklers, and a significant distance from smoke detectors.



## Results

The office fire was detected after 30 seconds by a duct smoke detector. Figure k on the next page shows a Smokeview rendering of the model at the time of detection. Table 7a below summarizes the results of the office fire simulation at each level and differentiates RSET between paths 1 and 2.

Table 7a – Office Fire Smoke Layer & Tenability

Level	Smoke Layer Height at Detection (ft)	Time at Tenability Failure (s)	ASET (s)	RSET (1) (s)	$\frac{ASET}{RSET}$ (1)	RSET (2) (s)	$\frac{ASET}{RSET}$ (2)
G2	11.3	260	230	52	4.42	52	4.42
3	10.3	180	150	121	1.90	76	1.97
4	10.6	320	290	149	1.54	76	3.82
5	10.5	370	340	178	<b>1.29</b>	76	4.47
6	10.5	600+	570+	206	<b>1.12</b>	76	7.5+

ASET exceeds RSET for all levels so the tenability criterion is met for this office fire simulation. The safety factor for each level should be greater than 1.5, but it is not for levels 5 and 6 when the occupants use path 1. The EVACS should be used to tell the occupants to use path 2 by informing the occupants on levels 5 and 6 to exit the atrium to the East or West wings of the building and then proceed to an exit.

The chair fire was detected after 130 seconds by a beam smoke detector. Figure l on the next page shows a Smokeview rendering of the model at the time of detection. Table 7b below summarizes the results of the chair fire simulation at each level and differentiates RSET between paths 1 and 2.

Table 7b – Atrium Chair Fire Smoke Layer & Tenability

Level	Smoke Layer Height at Detection (ft)	Time at Tenability Failure (s)	ASET (s)	RSET (1) (s)	$\frac{ASET}{RSET}$ (1)	RSET (2) (s)	$\frac{ASET}{RSET}$ (2)
G2	7.1	600+	470+	52	9.0+	52	9.0+
3	<b>2.3</b>	90	<b>n/a</b>	<b>121</b>	<b>&lt; 1.0</b>	76	<b>&lt; 1.0</b>
4	6.2	140	10	<b>149</b>	<b>&lt; 1.0</b>	76	<b>&lt; 1.0</b>
5	7.2	200	70	<b>178</b>	<b>&lt; 1.0</b>	76	<b>&lt; 1.0</b>
6	7.5	250	120	<b>206</b>	<b>&lt; 1.0</b>	76	1.58

The tenability criterion is not met for either path on levels 3 through 5 and failures are noted in red text. Varying the chair fire in CFAST by changing its maximum HRR and growth rate did not solve the tenability failure. The result of this model is that the furniture should not be allowed because it presents a smoke hazard to the entire atrium that cannot be mitigated without changing the space. However, this same fire is modeled in FDS for confirmation, but a different result was achieved, which indicates this fire scenario is not well modeled in a two-zone model like CFAST.



Smokeview 6.1.11 - Jul 16 2014

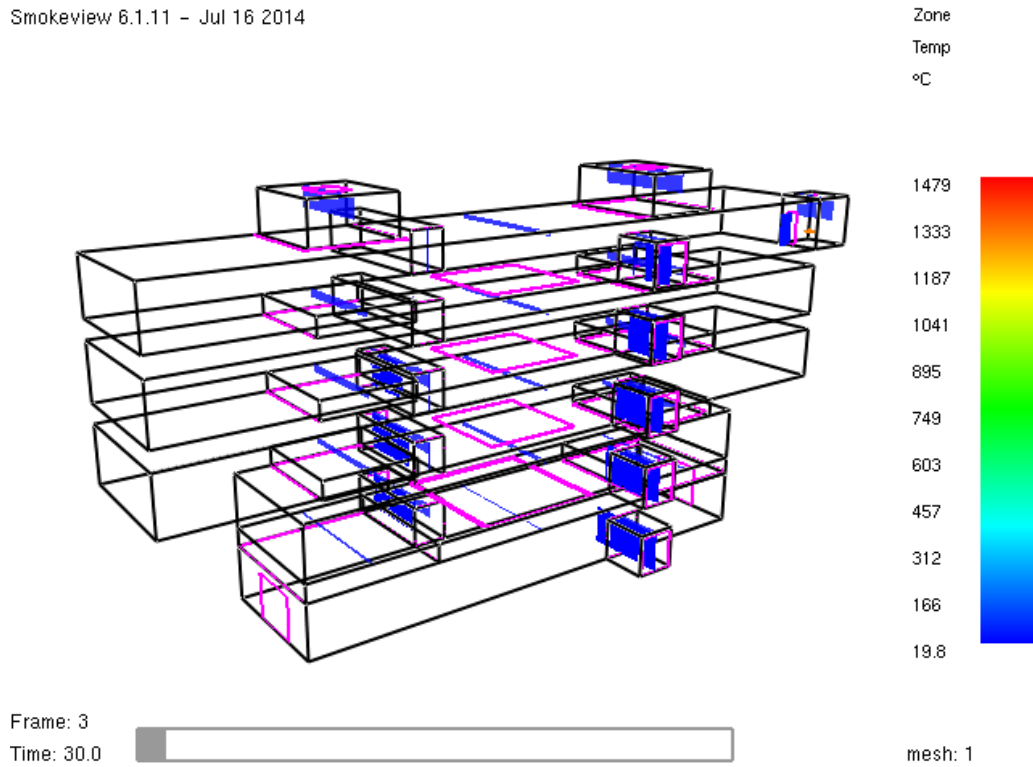


Figure k – CFAST Office Fire Smoke Layer Height at Detection

Smokeview 6.1.11 - Jul 16 2014

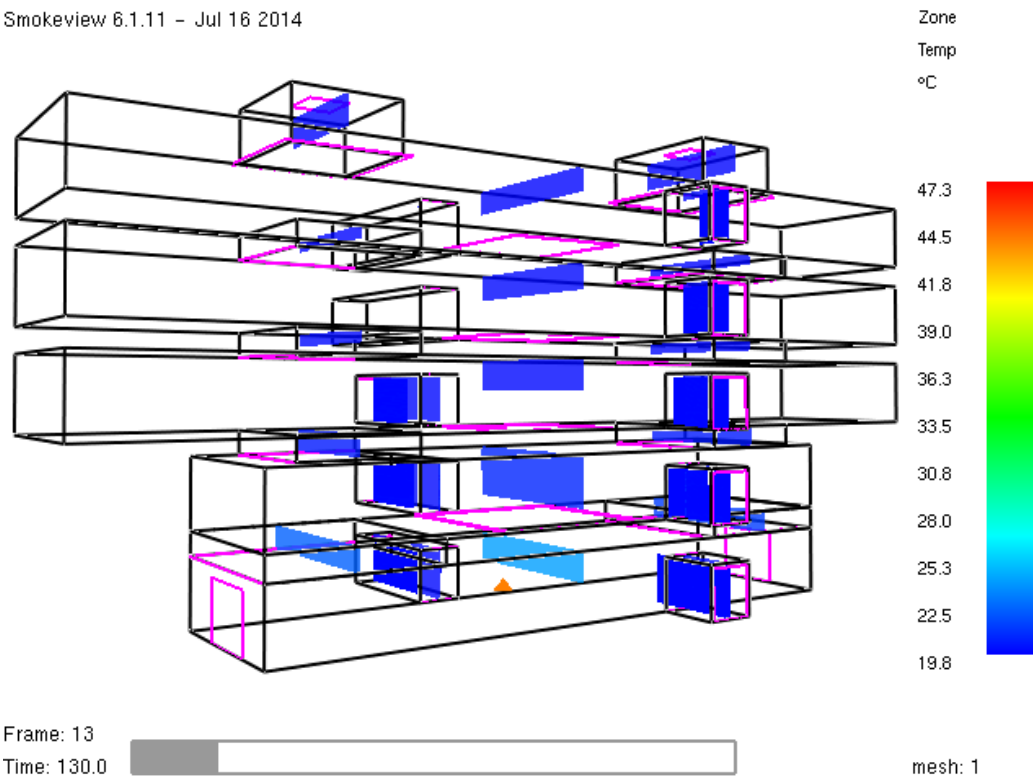


Figure l – CFAST Atrium Chair Fire Smoke Layer Height at Detection



## FDS

### Model Details

Unlike CFAST, FDS is not a two-zone model, it is a computational fluid dynamic model (CFD). In general, FDS should give a fairly realistic assessment of the conditions of a space during a fire, given the proper inputs. Due to the complexity of the atrium, a CFD model would be expected to give a better result than a two-zone model.

The atrium was modeled in FDS similarly to CFAST by using 25 rectangular meshes. Wall angles were not input to the model because angled walls are not expected to significantly affect the smoke layer height. A coarse mesh resolution of 0.3 m (about 1 foot) was chosen to balance computational time and accuracy for the large open space of the atrium; with this mesh resolution, there are about 260,000 cells in the model

Smoke detectors were placed at the location of the elevator on all levels and at the vents, to represent duct smoke detectors, on levels 2 and 3. Beam smoke detectors were placed at the locations indicated on the plans. Two sprinklers are placed equal distance from the fire source.

The atrium is naturally ventilated with interior doors to the hallways initially open and exterior doors on level 2 initially closed. When any detection device activates, the interior doors close and exterior doors open, the ducts to the atrium also close.

The same chair fire from the CFAST simulation is modeled in FDS as a t-squared ultrafast growth rate 700 kW maximum HRR. Figure m below shows the actual heat release rate curve FDS generated for this fire.

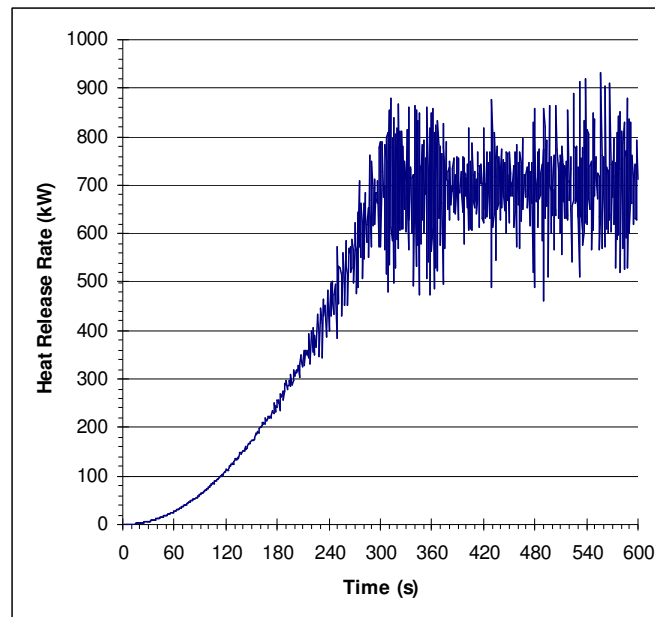


Figure m – FDS t-squared Ultrafast 700 kW HRR Curve



## Results

The fire was detected after 85 seconds by the smoke detector by the elevator on level 2. Figure n at the bottom of this page shows a Smokeview rendering at the time of detection. Table 8a below summarizes the results of the simulation for levels 2 and 3; levels 4 through 6 are not included because a smoke layer does not form on these levels.

Table 8a – Atrium Chair Fire Smoke Layer & Tenability

Level	Smoke Layer Height at Detection (ft)	Time at Tenability Failure (s)	ASET (s)	RSET (1) (s)	$\frac{ASET}{RSET}$ (1)	RSET (2) (s)	$\frac{ASET}{RSET}$ (2)
G2	10.5	n/a	-	52	-	52	-
3	n/a	293	208	121	2.74	76	2.74

ASET exceeds RSET for all levels so the tenability criterion is met for this chair fire simulation and the safety factor is greater than 1.5 for both paths for all levels. A smoke layer forms on level 2, but does not fail the tenability criterion for the duration of the simulation. A smoke layer forms on level 3 sometime after detection and the smoke layer on level 3 eventually descends below 6 feet from the floor. Figure o on the next page shows a Smokeview rendering at the time of tenability failure, note that multiple detection devices have activated prior to tenability failure.

Smokeview 6.1.11 - Jul 16 2014

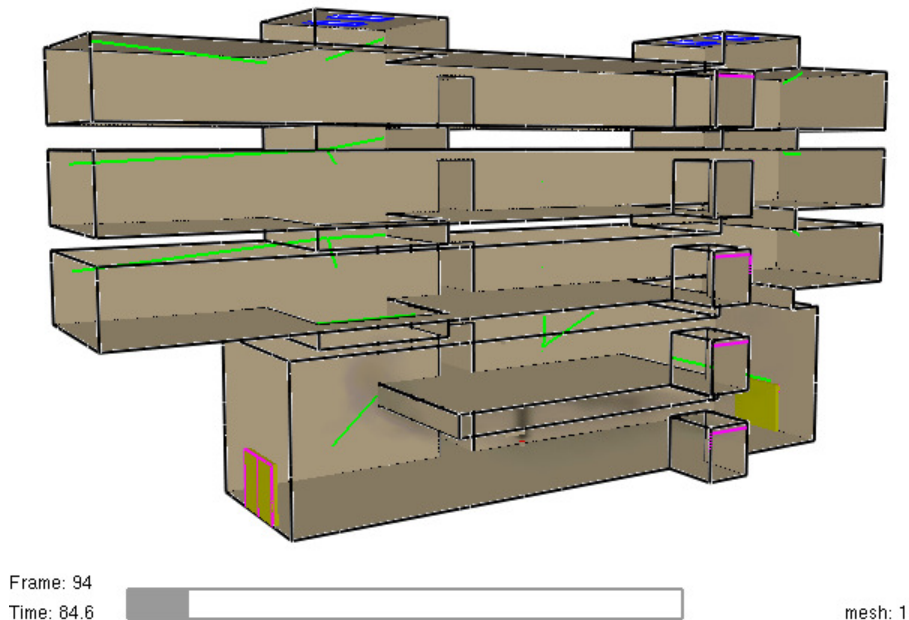
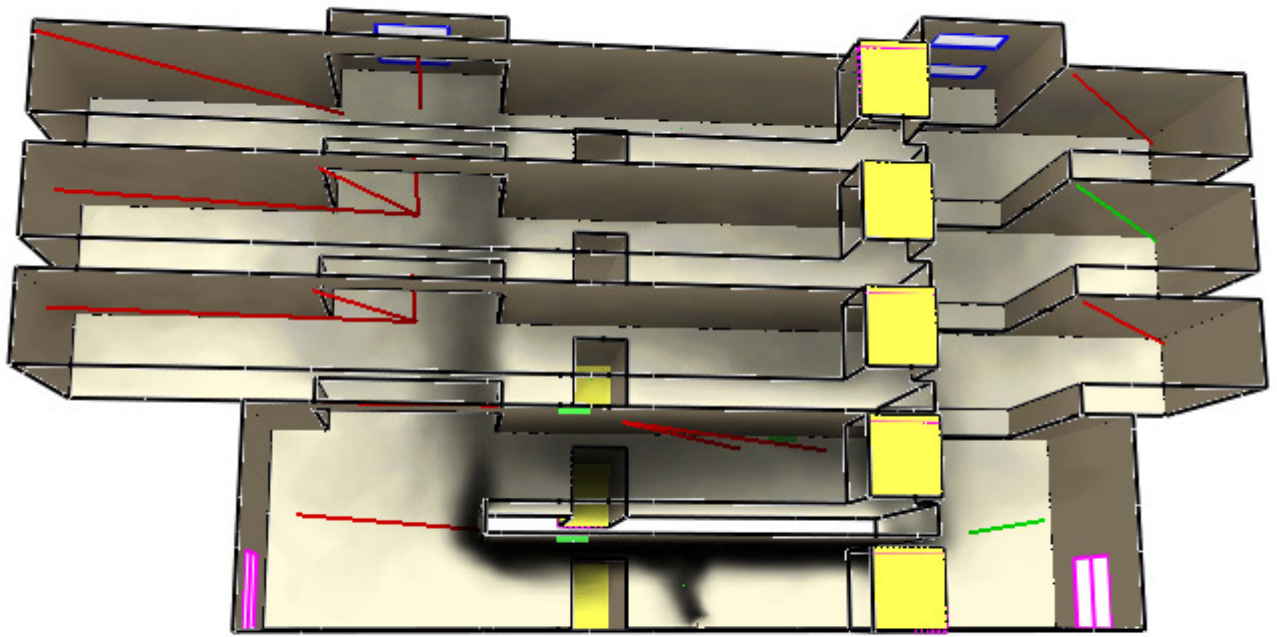


Figure n – FDS Atrium Chair Fire 3D Smoke at Detection



Smokeview 6.1.11 - Jul 16 2014



Frame: 338

Time: 292.8



mesh: 1

Figure o – FDS Atrium Chair Fire 3D Smoke at Tenability Failure



## **Conclusions and Recommendations**

The analysis of the Center for Science in this report shows that the building meets prescriptive code requirements and meets the performance based analysis of the atrium using CFAST and FDS for tenability based on smoke layer height in the atrium. The prescriptive requirements met are for structural fire protection, egress, the fire suppression system, and the fire alarm, detection, and communication systems. The performance based analysis is met for a typical fire scenario using the DETACT model and the atrium by using CFAST and FDS. The DETACT model shows that a typical occupancy fire will not reach flashover before the sprinkler system activates to control the fire. The fire models of the atrium in CFAST and FDS show that the tenability criterion is met, which is to keep the smoke layer height 6 feet above the floor long enough to allow occupants to safely egress, where safe egress is based on ASET and RSET.

It is the recommendation of this report that the fuel load in the atrium be kept to a minimum, allowing only for chairs and other furniture with no more than a 700 kW maximum HRR that would grow no faster than a t-squared medium fire, based on the results of the fire models in this report. This recommendation can be accomplished by using furniture that exhibits similar flammability characteristics to the design fire used in the fire models; this furniture should have minimal cushioning and use traditional materials in its construction, such as cotton instead of foam. If furniture with a higher maximum HRR or a faster growth rate is to be placed in the atrium, new fire models should be run to ensure that tenability is maintained long enough to allow occupants to safely egress.

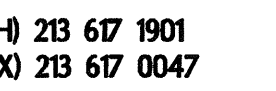


## **Appendix**

Selected portions of the building plans and other design plans are attached to the end of this report. The order of attached documents is as follows:

- Foundation and Framing Plans
- Typical Details (Structural)
- Life Safety Plans
- Hydraulic Calculations and Sprinkler Shop Drawings
- As-Built Fire Alarm Plans





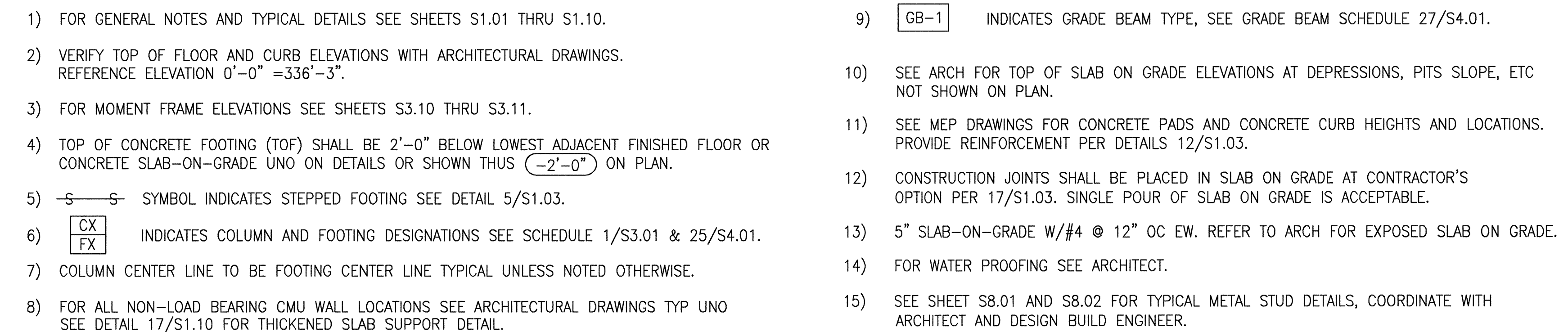
**NG DESIGN**  
Nelson & Associates, LLC  
Box 270254  
Denver, CO 80127



Title  
T LEVEL  
FOUNDATION PLAN -  
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2.01W



1 FOUNDATION PLAN - WEST  
S2.01W SCALE: 1/8" = 1'-0"



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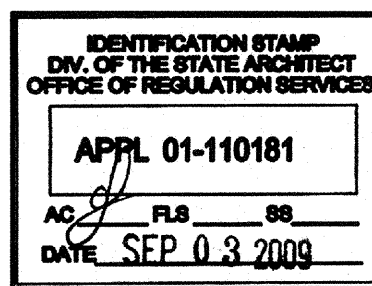
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CENTER FOR

AN LUIS OBISPO, CA

## Drawing Tide

## SECOND LEVEL FRAMING PLAN - EAST



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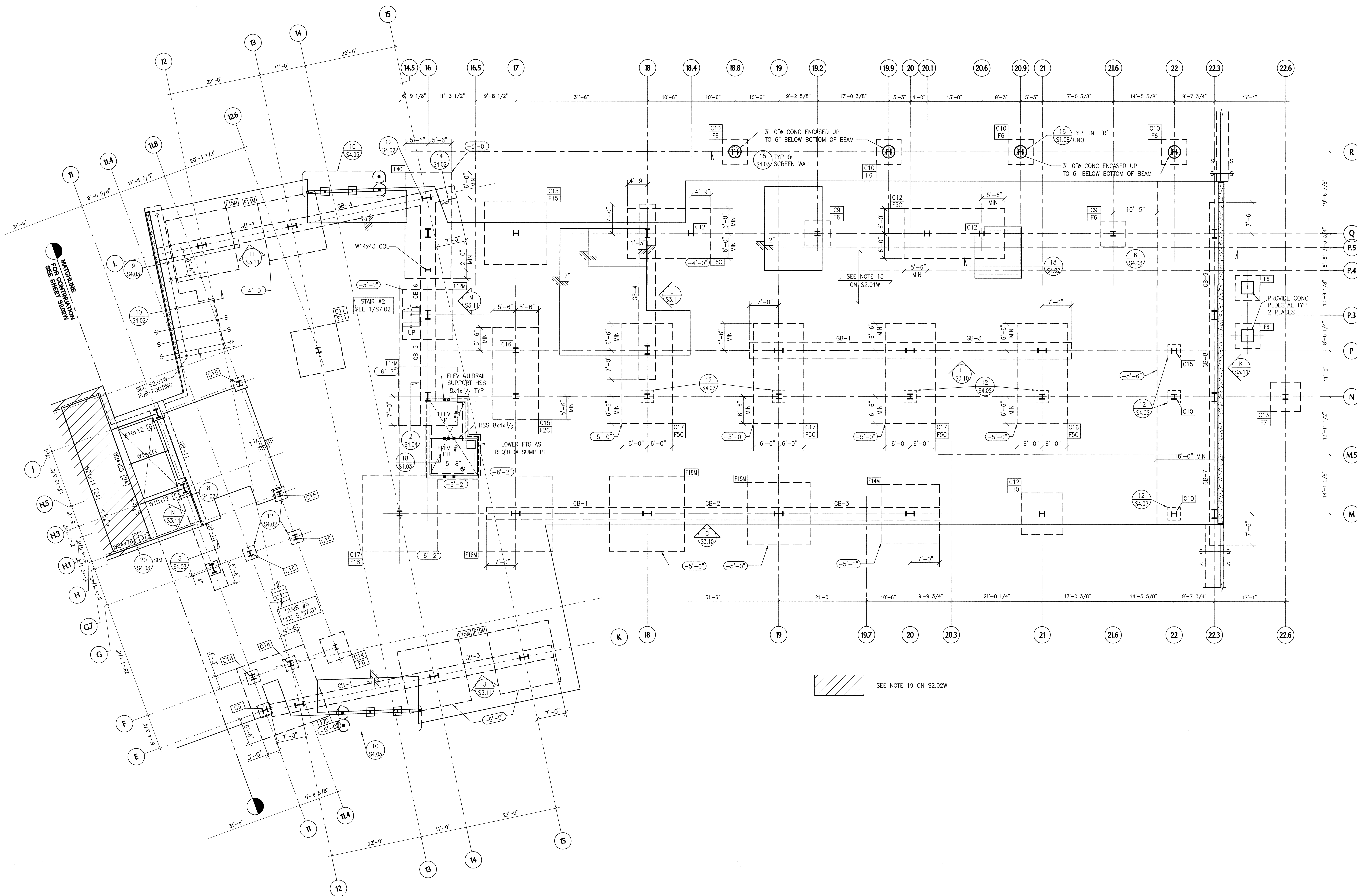
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Drawing N

## S2.02E



1 SECOND LEVEL FRAMING PLAN - EAST

S2.02E SCALE: 1/8" = 1'-0"

## NOTE

NOTE:  
1. SEE NOTES ON SHEET S2.01W.





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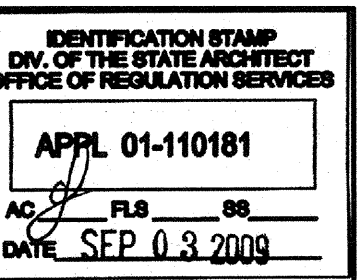
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10/23/09

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SCIENCE  
SAN LUIS OBISPO, CA

SECOND LEVEL  
FRAMING PLAN - WEST



Date: OCTOBER 23, 2009  
Job No: L40302.05  
Drawn By:  
Checked By:

Drawing No. \_\_\_\_\_

## S2.02W



1 SECOND LEVEL FRAMING PLAN - WEST  
S2.02W SCALE: 1/8" = 1'-0"





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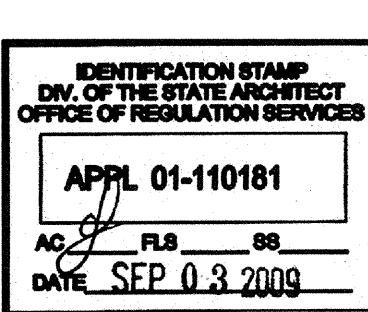
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**LIGHTING DESIGN**  
David Nelson & Associates, LLC  
P.O. Box 270254  
Littleton, CO 80127



Revisions  
BD DOCUMENTS 10/23/09

CENTER FOR SCIENCE  
SAN LUIS OBISPO, CA

Drawing Title  
THIRD LEVEL  
FRAMING PLAN - EAST

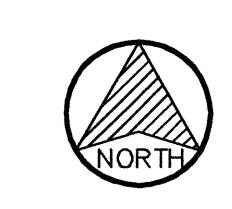


Date: OCTOBER 23, 2009  
Job No: L40302.05  
Drawn By:  
Checked By:  
Drawing No.

S2.03E

1 THIRD LEVEL FRAMING PLAN - EAST  
S2.03E SCALE: 1/8" = 1'-0"

NOTES:  
1. SEE NOTES ON SHEET S2.02W.





## Results

**STRUCTURAL ENGINEER**  
John A. Martin & Associates, Inc.  
100 South Grand Ave, 4th Flr  
Los Angeles, CA 90015 (J 11717)

## MECHANICAL ENGINEER

Ramsey Engineers  
 1 Linden Street  
 Oakland, CA 94607

## ELECTRICAL ENGINEER

Integrated Design Associates, Inc  
40 De La Cruz Boulevard, Suite 110  
Santa Clara, CA 95054

## CIVIL ENGINEER

Kannon Associates  
 50 Southwood Drive  
 San Luis Obispo, CA 93401

## LANDSCAPE ARCHITECT

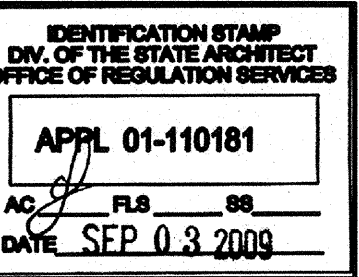
Catherine Spitz and Associates  
12 1/2 Glencoe Avenue  
Marina del Rey, CA 90292

## LABORATORY

Research Facilities Design  
65 Fifth Avenue, Suite 300  
San Diego, CA 92103-3107

## LIGHTING DESIGN

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Littleton, CO 80127



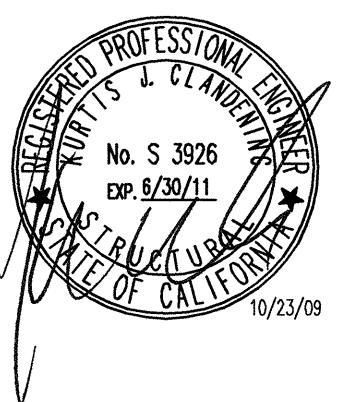
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DOCUMENTS 10/23/09

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SCIENCE  
SAN LUIS OBISPO, CA

## Drawing Title

### THIRD LEVEL FRAMING PLAN - WEST



Date: OCTOBER 23, 2009

Job No: L40302.05

Drawn By: \_\_\_\_\_

Checked By: \_\_\_\_\_

Drawing No.

S2.03W



1 THIRD LEVEL FRAMING PLAN - WEST

(S2.03W) SCALE: 1/8" = 1'-0"

NOTE:  
1. SEE NOTES ON SHEET S2.02W.



Consultants  
**STRUCTURAL ENGINEER**  
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Oakland, CA 94607

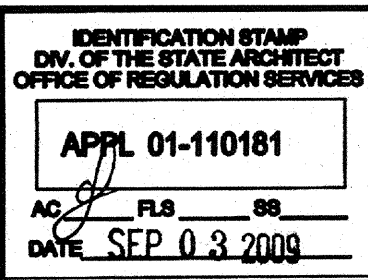
**ELECTRICAL ENGINEER**  
Integrated Design Associates, Inc.  
3140 De La Cruz Boulevard, Suite 110  
Santa Clara, CA 95054

**CIVIL ENGINEER**  
Cannon Associates  
1050 Southwood Drive  
San Luis Obispo, CA 93401

**LANDSCAPE ARCHITECT**  
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4212 1/2 Glencoe Avenue  
Marina del Rey, CA 90292

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**LIGHTING DESIGN**  
David Nelson & Associates, LLC  
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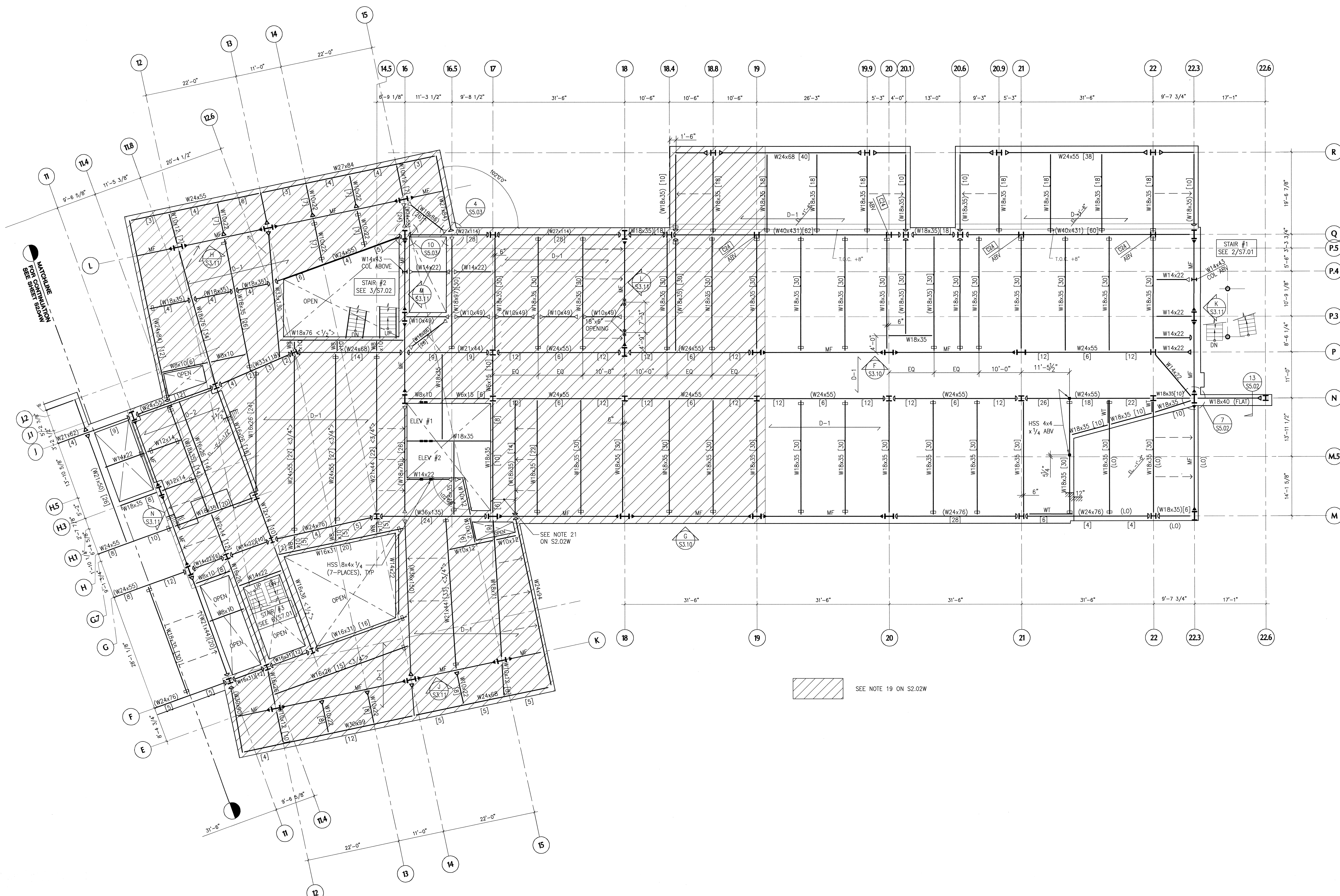
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FOURTH LEVEL  
FRAMING PLAN - EAST



Date: OCTOBER 23, 2009  
Job No: L40300205  
Drawn By:  
Checked By:

Drawing No.

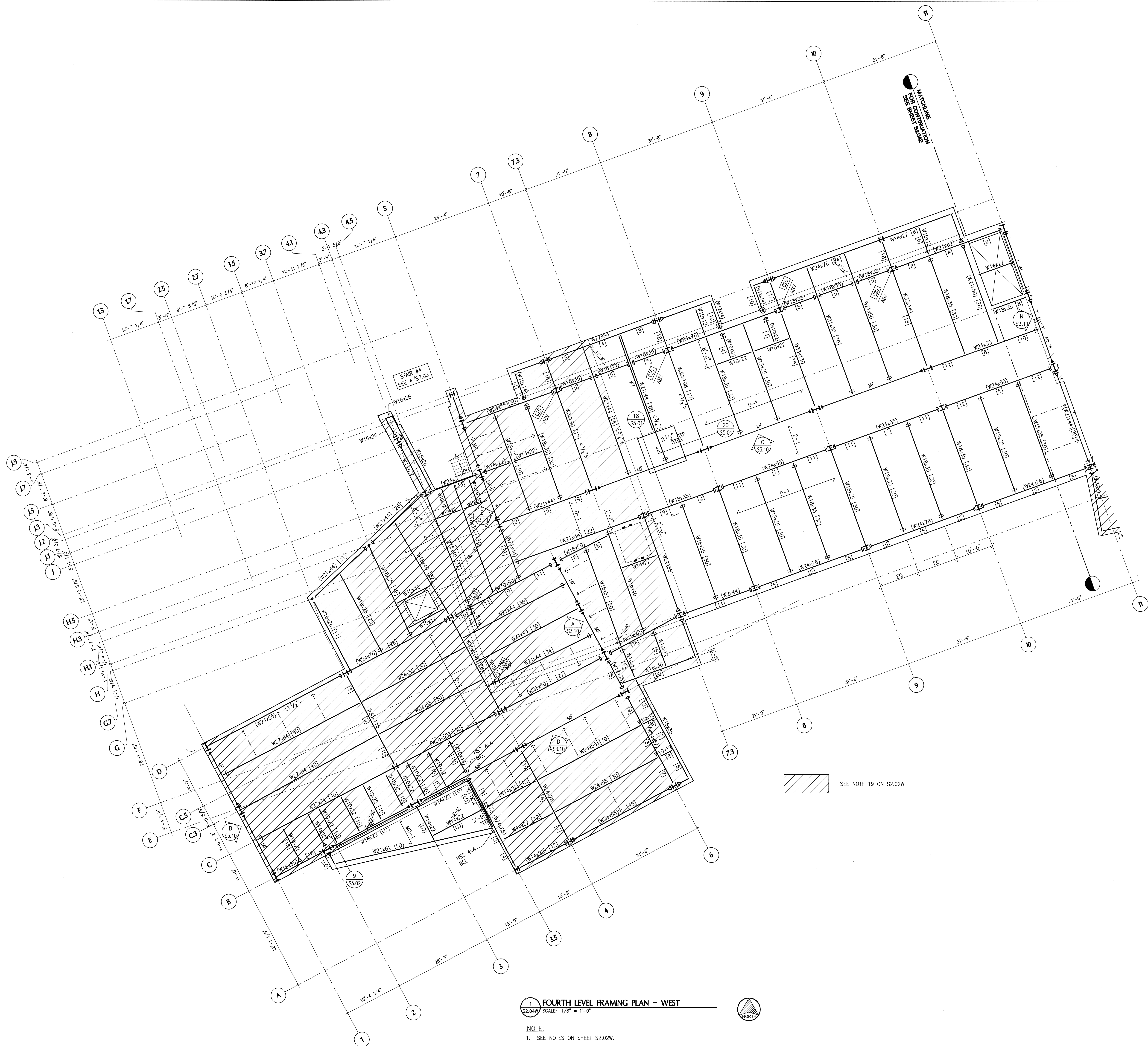
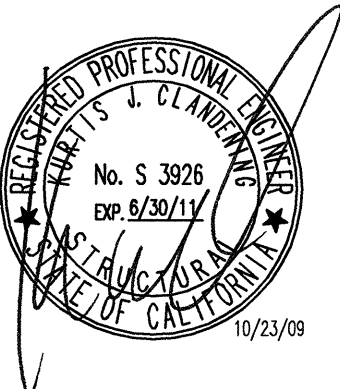
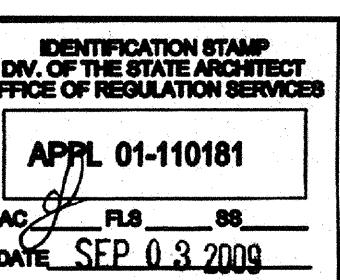
S2.04E



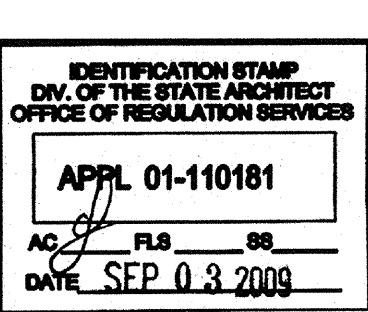
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S2.04E SCALE: 1/8" = 1'-0"

NOTE:  
1. SEE NOTES ON SHEET S2.02W.







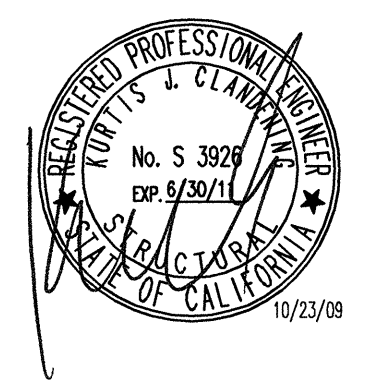


Revisions

BD DOCUMENTS	10/23/09
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CENTER FOR SCIENCE  
SAN LUIS OBISPO, CA

Drawing Title  
FIFTH LEVEL  
FRAMING PLAN - EAST



Date: OCTOBER 23, 2009  
Job No: L40302.05  
Drawn By:  
Checked By:  
Drawing No.

S2.05E

1 FIFTH LEVEL FRAMING PLAN - EAST  
S2.05E SCALE: 1/8" = 1'-0"

NOTE:  
1. SEE NOTES ON SHEET S2.02W.



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## Results

STRUCTURAL ENGINEER

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usey Engineers  
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land, CA 94607

ELECTRICAL ENGINEER

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Santa Clara, CA 95054

**L. ENGINEER**

non Associates  
0 Southwood Drive  
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LANDSCAPE ARCHITECT

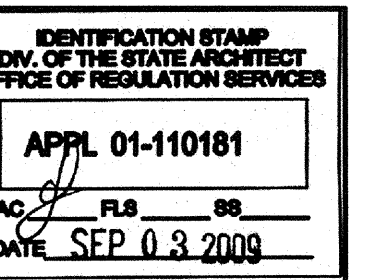
herine Spitz and Associates  
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## LABORATORY

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## TESTING DESIGN

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## Conclusions

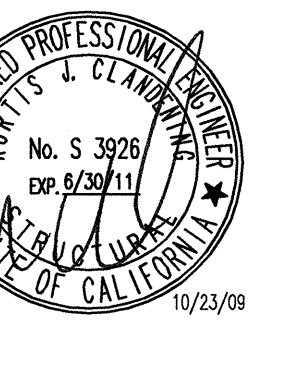
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### Working Title

### TH LEVEL

#### AMING PLAN – WEST



Date: OCTOBER 23, 2009

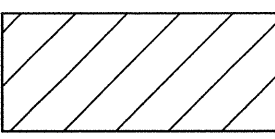
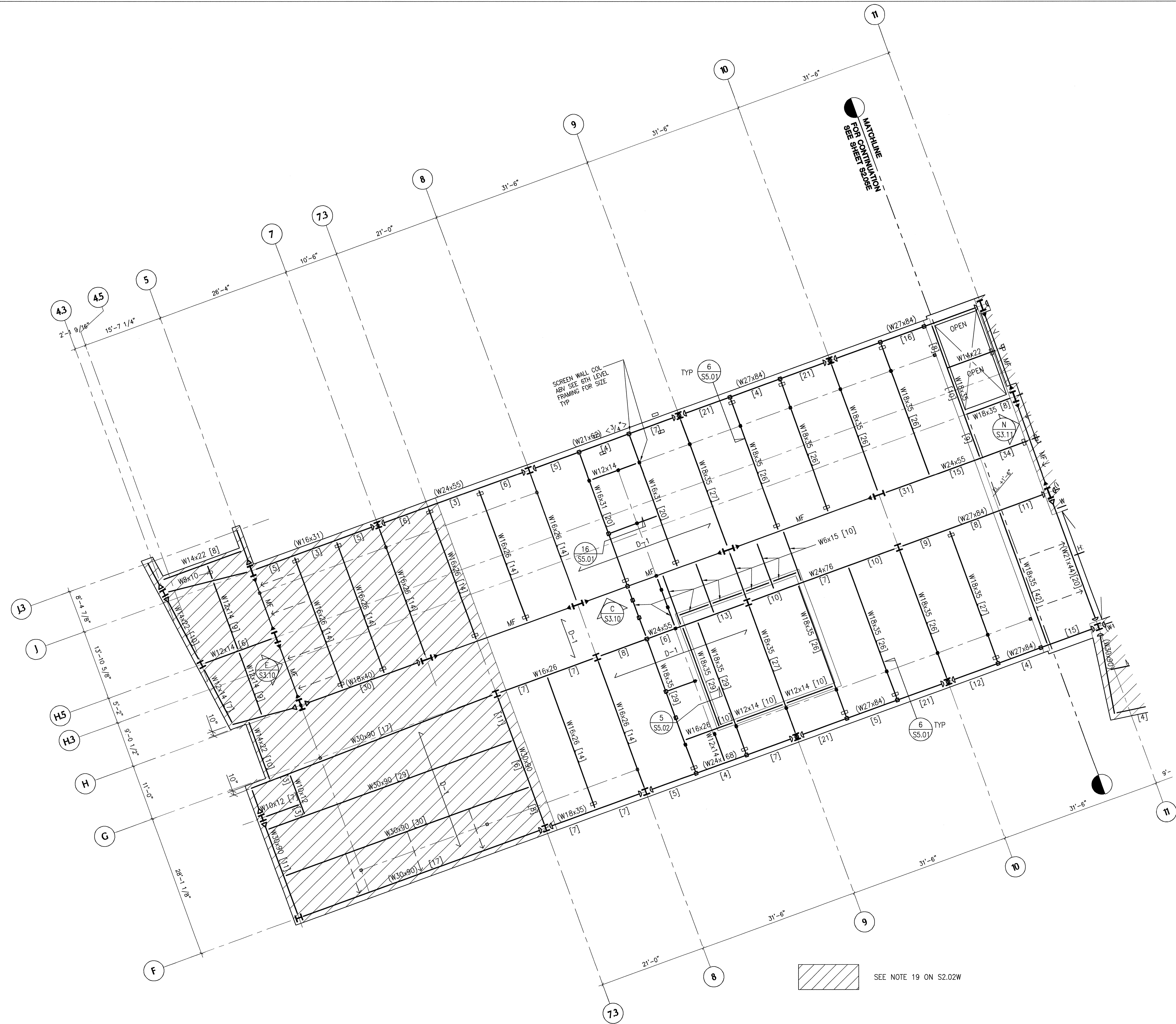
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Drawn By:

Checked By:

Drawing No.

S2.05W



SEE NOTE 19 ON S2.02W

1 FIFTH LEVEL FRAMING PLAN - WEST

S2.05W SCALE: 1/8" = 1'-0"

NOTE:

1. SEE NOTES ON SHEET S2.02W.





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### SIXTH LEVEL

#### FRAMING PLAN – EAST



S2.06E

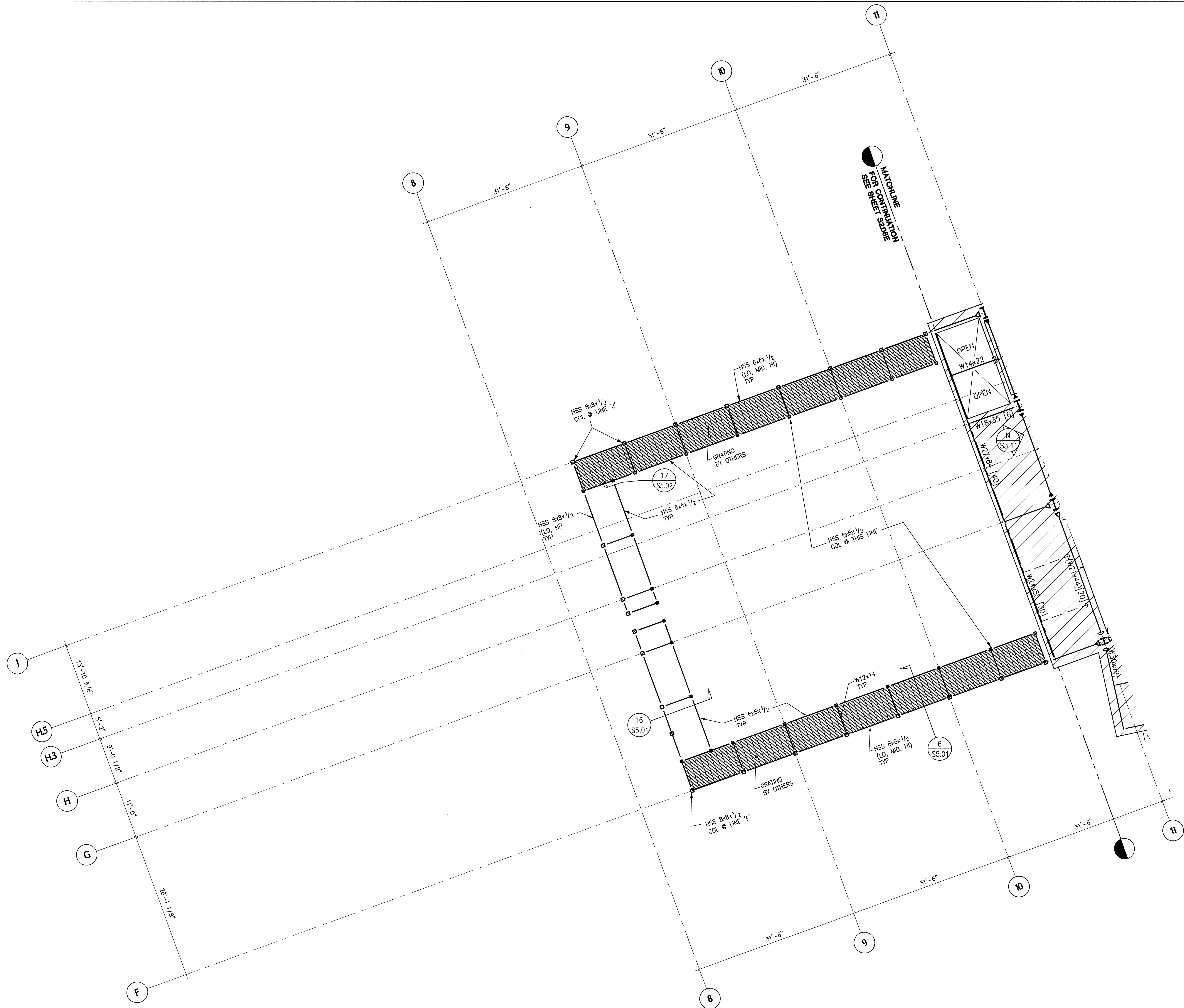


(S2.06E) SCALE: 1/8" = 1'-0"

1. SEE NOTES ON SHEET S2.02W.



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1 SIXTH LEVEL FRAMING PLAN - WEST

SCALE: 1/8" = 1'-0"

NOTE:

1. SEE NOTES ON SHEET S2.02W.



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LANDSCAPE ARCHITECT

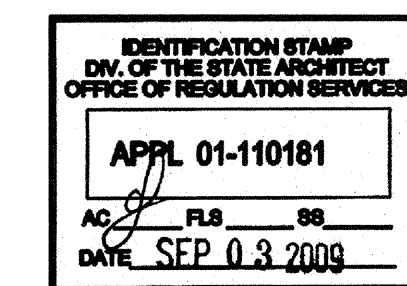
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SAN LUIS OBISPO, CA

Drawing Title

SIXTH LEVEL  
FRAMING PLAN - WEST



Date: OCTOBER 23, 2009

Job No: L40302.05

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Checked By:

Drawing No.

S2.06W



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Date: 10/27/2009  
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STEEL DECKING

1. THE STEEL DECKING SHALL BE OF TYPE AND GAUGE AS CALLED FOR ON DRAWINGS. DECKING AND ALL ACCESSORIES SHALL BE FORMED FROM STEEL SHEETS HAVING A MINIMUM YIELD STRENGTH OF 38,000 PSI AND CONFORMING TO A-653. THE STEEL SHALL BE ZINC-COATED CONFORMING TO A-653. CLASS C60. DECK UNITS SHALL BE CONTINUOUS OVER THREE OR MORE SPANS WHERE POSSIBLE.
2. MINIMUM BEARING OF DECKING ON SUPPORTS SHALL BE 2 INCHES. SHEETS SHALL BE ATTACHED TO ALL SUPPORTING STEEL MEMBERS BY WELDING AS INDICATED ON DRAWINGS AND IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS. UPON COMPLETION OF ERECTION, ALL WELDS IN EXPOSED DECK AREAS SHALL HAVE TOUCH-UP, 16-SLAC, CLEAN AND PRIME WITH A ZINC-RICH PRIMER. DECK WELDING SHALL BE AS NOTED ON PLANS. WHERE NO WELDING IS NOTED, THE SIDE LAP OF EACH PANEL SHALL BE FASTENED BY 1 INCH LONG FILLET WELDS OR APPROVED FUSION WELDS AT 24" ON CENTER MAXIMUM, OR BUTT PUNCHED AT 18 INCHES ON CENTER.
3. SEE DRAWINGS FOR DETAIL OF REINFORCING OF DECK OPENINGS. SEE ARCHITECTURAL, MECHANICAL, ELECTRICAL DRAWINGS, ETC., FOR SIZE AND LOCATION OF REQUIRED OPENINGS.
4. SHEAR CONNECTORS SHALL BE NELSON GRANULAR FLUX-FILLED HEADED ANCHOR STUDS OR AN APPROVED EQUAL, AND BE MADE FROM C-1015 COLD ROLLED STEEL, AND SHALL CONFORM TO A.S.T.M. SPECIFICATION A-108, GRADES 1015-1020 WITH A MINIMUM TENSILE STRENGTH OF 60,000 P.S.I. STUD WELDING INSPECTING AND TESTING SHALL CONFORM TO AWS D1.1. STUD WELDING INSPECTING AND TESTING SHALL CONFORM TO AWS D1.1.
5. DEFORMED BAR ANCHOR STUDS SHALL BE NELSON D2, GRANULAR FLUX-FILLED REBAR STUDS OR APPROVED EQUAL, AND SHALL BE MADE OF LOW CARBON COLD ROLLED STEEL, WITH A MINIMUM TENSILE STRENGTH OF 60,000 PSI. STUD WELDING INSPECTING AND TESTING SHALL CONFORM TO AWS D1.1.
6. HANGERS SUPPORTED BY METAL DECK WITH STRUCTURAL CONCRETE FILL SHALL BE INSTALLED USING ISO-APPROVED ANCHORAGE SYSTEMS. SUCH HANGERS SHALL BE USED TO SUPPORT DUCTWORK (54" X 16" MAX.), PIPING (4" ROUND MAX.), OR CEILING, HANGERS MUST BE AT LEAST TWO FLUTES APART ON SAME DECK SPAN. LARGER DUCTWORK AND PIPING SHALL BE SUPPORTED BY STRUCTURAL BEAMS OR COLUMNS. COORDINATE WITH TYPICAL DETAILS.

STRUCTURAL STEEL & MISCELLANEOUS METAL

1. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH THE AISC SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS (LATEST EDITION AND SUPPLEMENTS).
2. ALL STRUCTURAL STEEL SHALL CONFORM TO ASTM A572, GRADE 50 U.S.N. ALL ROLLED STEEL WF SHAPES TO BE ASTM A992 OR 50. STRUCTURAL STEEL, CHANNELS, AND ANGLES SHALL CONFORM TO ASTM A36 UNO.
3. PIPE COLUMNS - ASTM A53, GRADE "B".
4. STEEL TUBES - ASTM A500, GRADE "B" (FY = 46000 PSI).
5. BOLTS - ALL BOLTS SHALL BE A325SS BOLTS TYP. U.S.N.O.
6. ANCHOR STUDS SHALL BE NELSON GRANULAR FLUX-FILLED HEADED ANCHOR STUDS OR AN APPROVED EQUAL, AND BE MADE FROM C-1015 COLD ROLLED STEEL, AND SHALL CONFORM TO A.S.T.M. SPECIFICATION A-108, GRADES 1015-1020 WITH A MINIMUM TENSILE STRENGTH OF 60,000 P.S.I. STUD WELDING INSPECTING AND TESTING SHALL CONFORM TO A.S.T.M. D1.1-2004.
7. ANCHOR BOLTS - F1554 GRADE 55 S1
8. THE STRUCTURAL STEEL FABRICATOR SHALL FURNISH SHOP DRAWINGS FOR ARCHITECT'S & STRUCTURAL ENGINEER'S REVIEW BEFORE FABRICATION.
9. BOLT HOLES IN STEEL SHALL BE 1/8 INCH LARGER IN DIAMETER THAN NOMINAL SIZE OF BOLT USED, UNLESS OTHERWISE NOTED.
10. ALL WELDS SHALL BE PREQUALIFIED IN CONFORMITY WITH THE CODE FOR WELDING IN BUILDING CONSTRUCTION (AWS D1.1) OF THE AMERICAN WELDING SOCIETY. ELECTRODES TO BE E70 SERIES UNLESS NOTED OTHERWISE.
11. BUTT WELDS, COMPLETE JOINT PENETRATION OR PARTIAL JOINT PENETRATION ARE NOT INDICATED AS C.J.P.P. OR P.J.P. RESPECTIVELY.
12. WELDING OF SHEET METAL AND METAL STUDS SHALL BE IN ACCORDANCE WITH AWS D1.3-98.
13. WELD LENGTHS CALLED FOR ON PLANS ARE THE NET EFFECTIVE LENGTH REQUIRED. WELD SIZE SHALL BE AS MINIMUM UNLESS A LARGER SIZE IS NOTED.
14. WELDING TESTS AND INSPECTIONS - SEE SPECIFICATION.
15. CAMBER -  
A. PROVIDE UPWARD CAMBER TO ALL MEMBERS SHOWN TO HAVE CAMBER. AMOUNT MEASURED IN THE FIELD PRIOR TO ERECTION SHALL NOT DEVIATE BY MORE THAN ALLOWED BY THE AISC SPECIFICATIONS. DO NOT CAMBER MEMBERS BELOW ELEVATOR ENTRANCE DOORS.  
B. BEAMS DETAILED WITHOUT SPECIFIED CAMBER SHALL BE FABRICATED SO THAT AFTER ERECTION ANY MINOR CAMBER DUE TO ROLLING OR SHOP ASSEMBLY SHALL BE UPWARD. TOP OF ALL MEMBERS SHALL BE CLEARLY IDENTIFIED.
16. COMPOSITE STRUCTURAL STEEL BEAMS ARE DESIGNED IN ACCORDANCE WITH "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS" OF THE AISC, NOT TO REQUIRE SHORING.
17. ALL STRUCTURAL STEEL SURFACES TO BE WELDED OR HIGH-STRENGTH BOLTED, TO BE ENCASED IN CONCRETE, TO RECEIVE SPRAY-APPLIED FIREPROOFING, OR TO BE ENCLOSED BY FINISH MATERIALS SHALL BE LEFT UNPAINTED.
18. ALL STRUCTURAL STEEL AND MISCELLANEOUS METAL EXPOSED TO WEATHER IN FINAL STRUCTURE SHALL NOT BE HOT GALVANIZED AFTER FABRICATION.
19. THE CONTRACTOR SHALL REVIEW ALL WELDING DETAILS FOR ACCESSIBILITY. ANY WELD INDICATED AS A SHOP WELD MAY BE WELDED IN THE FIELD WITH APPROVED WELD PROCEDURES AND INSPECTION. ANY WELD INDICATED AS A FIELD WELD MAY BE SHOP WELDED WITH APPROVED WELD PROCEDURES AND INSPECTION.
20. ALL GROOVE WELDS INDICATED THIS  ARE C.J.P.P., UNLESS NOTED OTHERWISE.
21. PROVIDE A QUALITY ASSURANCE PLAN PER AISC 341 CHAPTER 18 REFER TO AISC 341 APPENDIX Q FOR QUALITY ASSURANCE PLAN REQUIREMENTS.

REINFORCING STEEL

1. ALL REINFORCING STEEL SHALL BE DETAILED AND PLACED IN CONFORMANCE WITH THE CBC 2007 BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE (ACI-318), AND THE MANUAL OF STANDARD PRACTICE FOR REINFORCED CONCRETE CONSTRUCTION BY THE C.E.S.I. AND THE W.C.R.S.I., OR AS MODIFIED BY THE CONSTRUCTION DOCUMENTS.
2. REINFORCING BARS - A-615 GRADE 60 OR A-706 GRADE 60 UNLESS NOTED OTHERWISE.
3. WELDING OF REINFORCING STEEL SHALL BE WITH LOW HYDROGEN ELECTRODES IN CONFORMANCE WITH RECOMMENDED PRACTICES FOR WELDING REINFORCING STEEL, ETC., AMERICAN WELDING SOCIETY, AWS-D1.4. ALL REINFORCING TO BE WELDED SHALL BE ASTM A-706, GRADE 60. WELDING OF REINFORCING STEEL SHALL BE WITH LOW HYDROGEN ELECTRODES IN CONFORMANCE WITH RECOMMENDED PRACTICES FOR WELDING REINFORCING STEEL, ETC., AMERICAN WELDING SOCIETY, AWS-D1.4-08. ALL WELDS SHALL DEVELOP THE FULL STRENGTH OF THE REBAR, UNO.
4. ALL REINFORCING BAR BENDS SHALL BE MADE COLD. REINFORCING SHALL NOT BEND MORE THAN TWICE AT THE SAME LOCATION.
5. WELDED WIRE FABRIC - A-185.
6. WINDOW LAP OF WELDED WIRE FABRIC SHALL BE 6 INCHES, OR ONE FULL MESH PLUS TWO INCHES, WHICHEVER IS GREATER.
7. REINFORCING SPLICES SHALL BE MADE AS INDICATED ON THE DRAWINGS.
8. DOWELS BETWEEN FOOTINGS AND WALLS OR COLUMNS SHALL BE THE SAME GRADE, SIZE AND SPACING AS THE VERTICAL REINFORCING, RESPECTIVELY, UNLESS NOTED OTHERWISE.
9. ALL BARS SHALL BE MARKED SO THEIR IDENTIFICATION CAN BE MADE WHEN THE FINAL IN-PLACE INSPECTION IS MADE.

FOUNDATION

1. FOUNDATION DESIGN BASED ON GEOTECHNICAL REPORT BY EARTH SYSTEMS PACIFIC DATED OCTOBER 27, 2008 & UPDATED DATE JUNE 26, 2007. COMPANY COPIES ARE AVAILABLE FOR REVIEW AT THE ARCHITECT'S OFFICE.
2. FOOTING DESIGN BASED ON ALLOWABLE SOIL PRESSURE OF 4,500 PSF WHERE BEARING A MINIMUM 1'-0" INTO SOUND ROCK.
3. CONTRACTOR TO PROVIDE FOR DE-WATERING OF EXCAVATIONS FROM EITHER SURFACE WATER, GROUND WATER OR SEEPAGE.
4. CONTRACTOR SHALL PROVIDE FOR DESIGN AND INSTALLATION OF ALL CRIBBING, SHEATING AND SHORING REQUIRED TO SAFELY RETAIN THE EARTH BANKS.
5. EXCAVATION AND COMPACTING IF REQUIRED, SHALL BE APPROVED BY THE GOVERNING AGENCY AND THE FOUNDATION ENGINEER PRIOR TO PLACING THE CONCRETE AND REINFORCING. FOUNDATION ENGINEER TO SUBMIT LETTER OF COMPLIANCE TO OWNER. COMPACT FILL IN LAYERS TO A MINIMUM OF 85% RELATIVE COMPACTION AT BUILDING FOOTPRINT PER GEOTECH REPORT.
6. ALL EXCAVATIONS SHALL BE PROPERLY BACKFILLED. DO NOT PLACE BACKFILL BEHIND WALLS BEFORE THE WALLS HAVE GAINED FULL DESIGN STRENGTH. CONTRACTOR SHALL BRACE OR PROTECT ALL BUILDING AND RETAINING WALLS FROM GRADE FROM LIVE LOADS UNTIL ATTACKING FLOORS ARE COMPLETELY IN PLACE AND HAVE ATTAINED FULL STRENGTH. CONTRACTOR SHALL PROVIDE FOR DESIGN, PERMITS AND INSTALLATION OF SUCH BRACING.
7. FOOTINGS SHALL BE PLACED AND ESTIMATED ACCORDING TO DEPTHS SHOWN ON DRAWINGS. SHOULD SOIL ENCOUNTERED AT THESE DEPTHS NOT BE APPROVED BY THE FOUNDATION ENGINEER, FOOTING ELEVATIONS WILL BE ALTERED AS REQUIRED.
8. FOOTING BACKFILL AND UTILITY TRENCH BACKFILL WITHIN BUILDING AREA SHALL BE MECHANICALLY COMPACTED IN LAYERS, IN ACCORDANCE WITH SOIL REPORT. FLOODING WILL NOT BE ALLOWED.
9. ALL ABANDONED FOOTINGS, UTILITIES, ETC., THAT INTERFERE WITH NEW CONSTRUCTION SHALL BE REMOVED.
10. ALL EARTHWORK SHALL BE DONE IN ACCORDANCE WITH GEOTECHNICAL REPORT RECOMMENDATIONS AND CHECKED & INSPECTED BY THE SOILS ENGINEER OR THEIR REPRESENTATIVE.
11. ALL SUB-SLAB ASSEMBLIES AND COMPOSITIONS SHALL BE PER GEOTECH RECOMMENDATIONS.

CONCRETE (CAST-IN-PLACE)

1. ALL PHASES OF WORK PERTAINING TO THE CONCRETE CONSTRUCTION SHALL CONFORM TO THE CBC 2007.
2. SCHEDULE OF STRUCTURAL CONCRETE 28-DAY STRENGTHS & TYPES:  
LOCATION IN STRUCTURE STRENGTH PSI TYPE  
FOUNDATIONS & BRACE BEAMS 4,000 HARDROCK  
COLUMNS AND WALLS 4,000 HARDROCK  
SLAB-ON-GRADE 3,000 HARDROCK  
PERIMETER BASEMENT WALLS 4,000 HARDROCK  
CONCRETE FILL OVER METAL DECK 4,000 LIGHT WEIGHT  
ALL OTHER CONCRETE 4,000 HARDROCK
3. PORTLAND CEMENT SHALL CONFORM TO ASTM C-150, TYPE II, LOW ALKALI.
4. AGGREGATE FOR HARDROCK CONCRETE - C-33. EXCEPTIONS MAY BE USED ONLY WITH PERMISSION OF THE STRUCTURAL ENGINEER. MAXIMUM AGGREGATE SIZE=1".
5. FORMS FOR CONCRETE SHALL BE LAID OUT AND CONSTRUCTED TO PROVIDE THE SPECIFIED CONCRETE SHOWN ON THE DRAWINGS.
6. THE CONTRACTOR SHALL MAINTAIN A LOG OF STRUCTURAL SLAB ELEVATIONS BASED ON THE ARCHITECTURAL DRAWINGS PLUS THE ADDITION OF ANY CAMBERS INDICATED ON THE CONSTRUCTION DOCUMENTS. THIS LOG SHALL INDICATE SCHED ELEVATIONS PRIOR TO THE CONCRETE POUR, AND TOP OF CONCRETE SLAB PRIOR TO REMOVAL OF FORMS.
7. THE CONCRETE SLAB THICKNESS SHALL BE MAINTAINED UNLESS OTHERWISE SHOWN.
8. DRY PACK OR NON SHORING GROUT UNDER BASEPLATES, SILL PLATES, ETC., SEE CONTRACT DOCUMENTS.
9. CONCRETE MIXING OPERATION, ETC., SHALL CONFORM TO C-94.
10. PLACEMENT OF CONCRETE SHALL CONFORM TO ACI 304 AND CONTRACT DOCUMENTS. ROUGHEN ALL CONCRETE SURFACES AGAINST WHICH CONCRETE IS TO BE PLACED TO 1/2" MIN. MAXIMUM.
11. IF COLUMNS AND WALLS ARE PLACED WITH FLOOR, TWO HOURS MUST ELAPSE BETWEEN END OF COLUMN OR WALL POUR AND BEGINNING OF FLOOR POUR.
12. CLEAN AND ROUGHEN THE SURFACE OF ALL HORIZONTAL CONSTRUCTION JOINTS BY REMOVING THE ENTIRE SURFACE AND EXPOSING CLEAN AGGREGATE SOLIDLY EMBEDDED IN MATRIX.
13. THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCEMENT PLACED IN CAST-IN-PLACE CONCRETE:  
MINIMUM COVER, INCHES  
A. CONCRETE CAST AGAINST AND PERMANENTLY EXPOSED TO EARTH..... 3  
B. FORMED CONCRETE EXPOSED TO EARTH OR WEATHER:  
#5 THROUGH #8 BARS..... 1 1/2  
#9 BAR, #10 OR D37 WIRE..... 2  
C. CONCRETE NOT EXPOSED TO WEATHER OR IN CONTACT WITH DRIVING SLABS, WALLS AND JOISTS:  
#14 AND #18 BARS..... 1 1/2  
#11 BAR AND SMALLER..... 1  
BEAMS, COLUMNS AND WALL JAMBS..... 1  
PRIMARY REINFORCEMENT, TIES, STIRRUPS, AND SPIRALS:  
#3 THROUGH #11..... 1 1/2  
#14 AND #18 BARS..... 2 1/2
14. ALL REINFORCING BARS, ANCHOR BOLTS AND OTHER CONCRETE INSERTS SHALL BE WELL SECURED IN POSITION PRIOR TO PLACING CONCRETE.
15. PROVIDE SLEEVES FOR PLUMBING AND ELECTRICAL OPENINGS IN CONCRETE BEFORE PLACING. DO NOT CUT ANY REINFORCING WHICH MAY COME IN CONTACT WITH CONCRETE IS NOT PERMITTED EXCEPT AS SHOWN. NOTIFY THE STRUCTURAL ENGINEER IN ADVANCE OF CONDITIONS NOT SHOWN ON THE DRAWINGS.
16. CONDUIT OR PIPE SIZE (O.D.) SHALL NOT EXCEED ONE THIRD OF SLAB THICKNESS AND SHALL BE PLACED BETWEEN THE TOP AND BOTTOM REINFORCING, UNLESS SPECIFICALLY DETAILED OTHERWISE. CONCENTRATIONS OF CONDUITS OR PIPES SHALL BE AVOIDED EXCEPT WHERE DETAILED OPENINGS ARE PROVIDED.
17. PROJECTING CORNERS OF BEAMS, WALLS, COLUMNS, ETC., SHALL BE FORMED WITH A 1/2 IN. CHAMFER, UNLESS OTHERWISE NOTED IN THE DOCUMENTS. PROVIDE 3/8" RADIUS BLUNSE CHAMFER AT ALL EXPOSED CORNERS AT BASEMENT.
18. CURING COMPOUNDS USED ON CONCRETE TO RECEIVE A FINISH SHALL BE APPROVED BY THE FINISH APPLICATOR BEFORE USE.
19. THE MAXIMUM SIZE OF A SINGLE POUR FOR ANY DAY FOR ELEVATED SLABS SHALL NOT EXCEED 20,000 SQUARE FEET, AND THE RATIO OF LENGTH TO WIDTH OF THE POUR SHALL NOT EXCEED 2 TO 1 WITHOUT THE APPROVAL OF THE ARCHITECT.

GENERAL

1. THE PROJECT SPECIFICATIONS FORM A PART OF THESE GENERAL NOTES.
2. DIMENSIONS SHALL TAKE PRECEDENCE OVER SCALED DRAWINGS.
3. ALL WORK SHALL CONFORM TO THE STANDARDS OF THE FOLLOWING CODE: CALIFORNIA BUILDING CODE, 2007 EDITION AS APPROVED BY THE STATE OF CALIFORNIA AND ANY OTHER REGULATING AGENCIES WHICH HAVE AUTHORITY OVER ANY PORTION OF THE WORK, INCLUDING THOSE CODES AND STANDARDS LISTED IN THE CONTRACT DOCUMENTS.
4. MANUFACTURED MATERIALS SHALL BE APPROVED BY THE CHECKING AGENCY PRIOR TO THEIR USE. ALL REQUIREMENTS OF THOSE APPROVALS SHALL BE FOLLOWED.
5. SEE ARCHITECTURAL DRAWINGS FOR THE FOLLOWING:  
A. SIZE AND LOCATION OF ALL DOOR AND WINDOW OPENINGS.  
B. SIZE AND LOCATION OF ALL NON-BEARING PARTITIONS.  
C. SIZE AND LOCATION OF ALL CONCRETE CURBS, FLOOR DRAINS, GROOVES, DEPRESSED AREAS, CHANGES IN LEVEL, CHAMBERS, CHAMBERS, INSULATION, FLOOR OR ROOF OPENINGS.  
D. EXTERIOR WALL SYSTEM.  
E. SIZE AND LOCATION OF ALL FLOOR OR ROOF OPENINGS.  
F. STAIR FRAMING AND DETAILS.  
G. DIMENSIONS NOT SHOWN ON STRUCTURAL DRAWINGS.
6. SEE MECHANICAL, PLUMBING AND ELECTRICAL DRAWINGS FOR THE FOLLOWING:  
A. PIPE RUNS, SLEEVES, HANGERS, TRENCHES, WALL, ROOF AND FLOOR OPENINGS, ETC. NOT SHOWN OR OUTLETS IN WALLS AND SLABS.  
B. ELECTRICAL CONDUITS, RUNS, BOXES, GUTTERS IN WALLS AND SLABS.  
C. ANCHORAGE AND BRACING FOR ELECTRICAL, MECHANICAL OR PLUMBING EQUIPMENT.  
D. ANCHOR BOLTS FOR MOTOR MOUNTS.  
E. SIZE, WEIGHT, AND LOCATION OF MACHINES AND EQUIPMENT BASES.
7. SPECIFICATIONS, CODES AND STANDARDS NOTED IN THE CONTRACT DOCUMENTS SHALL BE OF THE LATEST APPROVED ISSUE, INCLUDING SUPPLEMENTS, UNLESS OTHERWISE NOTED. MATERIAL SPECIFICATIONS ARE ASTM LATEST EDITION.
8. CONSTRUCTION MATERIALS SHALL BE SPREAD OUT IF PLACED ON FRAMED FLOORS OR ROOFS. LOAD SHALL NOT EXCEED THE DESIGN LIVE LOAD PER SQUARE FOOT. PROVIDE ADEQUATE SHORING AND/OR BRACING WHERE STRUCTURE HAS NOT ATTAINED DESIGN STRENGTH OR WHERE OVERLOAD IS ANTICIPATED.
9. THE CONTRACTOR SHALL VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION. THE ARCHITECT SHALL BE NOTIFIED OF ANY DISCREPANCIES OR INCONSISTENCIES.
10. NOTES AND DETAILS ON DRAWINGS SHALL TAKE PRECEDENCE OVER GENERAL NOTES AND TYPICAL DETAILS. WHERE NOTES AND DETAILS ON DRAWINGS AND THESE GENERAL NOTES AND TYPICAL DETAILS ARE IN CONFLICT WITH THE PROJECT SPECIFICATIONS, THE MOST STRINGENT SHALL APPLY. CONDITIONS NOT SPECIFICALLY SHOWN SHALL BE CONSTRUCTED AS SHOWN FOR SIMILAR WORK.
11. MECHANICAL AND ELECTRICAL LOADS MAY BE SUPPORTED FROM BEAMS. LIGHT MECHANICAL AND ELECTRICAL LOADS ANCHORED INTO METAL DECK ASSEMBLY MUST BE ANCHORED INTO STRUCTURAL CONCRETE ABOVE. SEE STEEL DECKING NOTES AND DETAILS IF NO CONCRETE EXISTS.
12. STAIR FRAMING AND DESIGN-BUILD ELEMENTS, WHEN NOT SPECIFICALLY DETAILED ON THE STRUCTURAL OR ARCHITECTURAL DRAWINGS, SHALL BE THE DESIGN RESPONSIBILITY OF THE CONTRACTOR AND MAY BE SUPPORTED BY THE PRIMARY STRUCTURE. CONTRACTOR SHALL PROVIDE AND INSTALL ALL ANCHILARY MEMBERS INCLUDING BUT NOT LIMITED TO BEAMS, COLUMNS, POSTS, FOOTINGS, STIFFENERS, GUSSETS, HITCHES, BRACES, ETC., AND THE ATTENDANT CONNECTIONS, AS REQUIRED BY THE STRUCTURAL ENGINEER OF RECORD, TO SUPPORT LOADS IMPOSED BY THE STAIR FRAMING AND DESIGN-BUILD ELEMENTS ON THE PRIMARY STRUCTURE. DESIGN & DETAILING OF THESE ELEMENTS SHALL BE DEVELOPED AND STAMPED BY A LICENSED ENGINEER IN THE STATE OF CALIFORNIA. CONTRACTOR SHALL SUBMIT THE DESIGN TO THE STRUCTURAL ENGINEER OF RECORD FOR REVIEW AND APPROVAL PRIOR TO START FABRICATION. DESIGN-BUILD ELEMENTS & THEIR SUPPORT SHALL BE DESIGNED TO AVOID IMPROVED TORSIONAL AND HORIZONTAL LOADS INTO THE PRIMARY STRUCTURE. SPECIAL STAIR FRAMING SHOWN ON THE STRUCTURAL DRAWINGS SHALL BE STRICTLY ADHERED TO BY THE CONTRACTOR.
13. THE CONTRACT DOCUMENTS REPRESENT THE FINISHED STRUCTURE. THEY DO NOT INDICATE THE METHOD OF CONSTRUCTION. THE CONTRACTOR SHALL PROVIDE ALL MEASURES NECESSARY TO PROTECT THE STRUCTURE DURING CONSTRUCTION. SUCH MEASURES SHALL INCLUDE, BUT NOT BE LIMITED TO, BRACING, SHORING FOR LOADS DUE TO CONSTRUCTION EQUIPMENT, ETC., OBSERVATION VISITS TO THE SITE BY THE STRUCTURAL ENGINEER SHALL NOT INCLUDE INSPECTION OF THE ABOVE ITEMS.
14. OPENINGS, POCKETS, ETC. SHALL NOT BE PLACED IN STRUCTURAL MEMBERS UNLESS SPECIFICALLY DETAILED ON THE STRUCTURAL DRAWINGS. NOTIFY THE STRUCTURAL ENGINEER WHEN DRAWINGS BY OTHERS SHOW OPENINGS, POCKETS, ETC., LARGER THAN 6 INCHES NOT SHOWN ON THE STRUCTURAL DRAWINGS, BUT WHICH ARE LOCATED IN STRUCTURAL MEMBERS.
15. THE CONTRACTOR SHALL INVESTIGATE SITE FOR FILLED EXCAVATIONS OR BURIED STRUCTURES SUCH AS CESSPOOLS, CISTERNS, FOUNDATIONS, ETC. IF ANY SUCH STRUCTURES ARE FOUND, ARCHITECT SHALL BE NOTIFIED IMMEDIATELY.
16. DESIGN LIVE LOADS:  
AREA DESIGN LIVE LOAD REMARKS  
EXTERIOR AT GRADE (PUBLIC PLAZA) 150 PSF UNREDOUCED  
TYPICAL OFFICE AND CLASSROOMS 100 PSF (80+20) REDUCIBLE  
STAIRS/CORRIDORS/PUBLIC AREAS 150 PSF UNREDOUCED  
(BASEMENT AND LEVEL 1)  
STAIRS/CORRIDORS/PUBLIC AREAS 100 PSF REDUCED  
(LEVELS 2 AND 3)  
AUDITORIUM AND LIBRARY 150 PSF UNREDOUCED  
MECHANICAL PENHOUSE 150 PSF UNREDOUCED  
MECHANICAL ROOMS 50 PSF UNREDOUCED  
LIGHT STORAGE 40 PSF UNREDOUCED  
ROOF 50 PSF REDUCIBLE
17. OCCUPANT DESIGN LATERAL LOAD CRITERIA  
CATEGORY CATEGORY = III  
WIND: ZONE = 85 MPH  
EXPOSURE = B  
1W = 1.15  
INTERNAL PRESSURE=0.18 FOR ENCLOSED STRUCTURE  
COMPONENTS & CLADDING WIND PRESSURE= 35 PSF

SEISMIC:

- SITE SOIL PROFILE TYPE = B  
1 = 1.25 S<sub>w</sub> = 0.84  
S<sub>0</sub> = 1.28 S<sub>01</sub> = 0.32  
S<sub>1</sub> = 0.48 OCC CAT=III  
SDC = D  
R = 8 SMF (ABOVE LEVEL 2)  
R = 5 SPECIAL CONCRETE SHEAR WALL (LEVEL 2 AND BELOW)  
C<sub>s</sub> = 0.038  
SEISMIC DESIGN BASE SHEAR= 0.038 BLDG DEAD LOAD  
ANALYSIS PROCEDURE USED= MODAL RESPONSE SPECTRUM ANALYSIS.  
(ASCE7-05 SECTION 12.8)  
V=7301.5 KIPS

DEFERRED APPROVAL

1. THE CONTRACTOR AT HIS EXPENSE, SHALL PROVIDE DESIGN AND DETAILS OF FRAMING ANCHORAGE PREPARED BY CALIFORNIA REGISTERED CIVIL ENGINEER FOR BUILDING DEPARTMENT. ARCHITECT AND STRUCTURAL ENGINEER'S APPROVAL FOR THE FOLLOWING:  
"EXTERIOR METAL STUDS"  
"ROOF STACKS"  
THE DESIGN SHALL CONFORM TO THE 2007 CALIFORNIA BUILDING CODE. SEE SPECIFICATION, ARCHITECTURAL, MECHANICAL AND ELECTRICAL DRAWINGS FOR ADDITIONAL ITEMS NOT COVERED IN THE ABOVE LIST. ANY REQUIRED MODIFICATION TO BUILDING STRUCTURE SHALL BE PAID BY THE CONTRACTOR.



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Revisions  
8D DOCUMENTS 10/29/09

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GENERAL NOTES



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1. AN INDEPENDENT TESTING AGENCY AND SPECIAL INSPECTORS SHALL BE RETAINED BY THE OWNER TO PERFORM THE TESTS AND INSPECTION AS REQUIRED BY SECTION 1704 OF THE CALIFORNIA BUILDING CODE. THE CONTRACTOR SHALL PROVIDE ACCESS TO THE SPECIAL INSPECTOR TO THE SITE OR FABRICATION SHOPS AND SHALL FURNISH SAMPLES OF MATERIALS FOR TESTING AS REQUESTED BY THE TESTING AGENCY AND THE GOVERNING CODE. CONTRACTOR TO PROVIDE TESTS PER CBC SECTION 1708.

- [illegible]

STRUCTURAL STEEL						
X	REVIEW MILL CERTIFICATE, TEST REPORTS AND MATERIAL IDENTIFICATION DELIVERED TO THE SITE					
C	REVIEW WELDING PROCEDURE SPECIFICATION & WELDER CERTIFICATION					
P	INSTALLATION OF NON-SLIP CRITICAL HIGH-STRENGTH BOLTS & WASHERS (PROVIDE CONTINUOUS INSPECTION IF INSTALLATION IS PERFORMED WITH CALIBRATED WRENCH)					
P	INSTALLATION OF SLIP CRITICAL-HIGH-STRENGTH BOLTS & WASHERS					
P	FIELD SECTION INSPECTION		P	SHOP	P	FIELD
X	FABRICATION INSPECTION		C	SHOP	C	FIELD
X	WELDING INSPECTION		X	SHOP	X	FIELD
X	NON-DESTRUCTIVE WELD TEST		X	SHOP	X	FIELD
X	BOLTING INSPECTION		X	SHOP	X	FIELD
P	COMPOSITE STEEL INSPECTION & TESTING					
P	INSTALLATION OF ANCHOR BOLTS BEFORE & DURING CONCRETE POUR					
METAL DECK						
X	REVIEW MILL CERTIFICATES & TEST REPORTS					
P	PLACEMENT INSPECTION					
P	WELDING & FASTENING INSPECTION					
REINFORCING STEEL						
X	REVIEW MILL CERTIFICATES & TEST REPORTS					
X	SAMPLE & TEST [X] REINFORCING BARS [X] WELDED WIRE FABRIC					
P	PLACEMENT INSPECTION					
C	WELDING INSPECTION					
P	TEST REINFORCING FOR WELDABILITY OTHER THAN ASTM A706					
CONCRETE, SHOTCRETE, CMU, GROUT & MORTAR						
CONCRETE	CMU	GROUT	MORTAR			
X	X	X	X	MIX DESIGN REVIEW		
X	X	X	X	VERIFICATION OF CORRECT MIX DESIGN USED DURING POUR		
X	C	X		PREPARATION OF SAMPLES FOR TESTING PURPOSES		
X				BATCH PLANT INSPECTIONS		
C	C	X		CAST, PICK-UP AND COMPRESSION TEST SAMPLES		
X				SLUMP, ENTRAINED AIR, & TEMPERATURE TEST		
X				SHRINKAGE TEST		
C	C	C	P	PLACEMENT INSPECTION		
P	P			CURING TEMPERATURE AND TECHNIQUES		
P				FORMWORK INSPECTION		
MISCELLANEOUS						
C	MECHANICAL ANCHORS					
C	ADHESIVE OR GROUTED ANCHORS AND DOWELS					
C	BOLTS CAST IN CONCRETE OR MASONRY					
C	COLD FORM METAL FRAMING INSTALLATION AND WELDING					
NOTES:						
C	INDICATES CONTINUOUS INSPECTION					
P	INDICATES PERIODIC INSPECTION					
X	INDICATES REQUIRED INSPECTION					

1. CODE LEVEL DESIGN SEISMIC LOAD DEFLECTIONS.

2. TYPICAL MAXIMUM VERTICAL DEFLECTIONS OF PERIMETER BEAMS ARE  $\Delta a = 1"$   $\Delta b = \frac{1}{2}"$  UNO IN ITEM 3.

### 3. GRAVITY DEFLECTION AT CURTAIN WALL.

(-) INDICATES DOWNWARD DEFLECTION  
(+) INDICATES UPWARD DEFLECTION  
 $\Delta_{DL}$  DEFLECTION DUE TO SUPERIMPOSED DEAD LOAD ONLY, NEGLECTING THE EFFECTS OF WEIGHT OF DECK AND FRAMING MEMBERS.  
 $\Delta_{LL}$  DEFLECTION DUE TO LIVE LOAD ONLY.  
 $\Delta_{TL}$  DEFLECTION DUE TO LIVE LOAD, SUPERIMPOSED DEAD LOAD, AND SELF WEIGHT OF THE DECK AND FRAMING MEMBERS.

1. ADHESIVE EXISTING CONCRETE SHALL BE EPOXY GROUTED WITH HILTI HIT RESO INJECTION COWLING ANCHOR ICC ES REPORT NO. ESR1682 OR APPROVED EQUAL.
2. THE HOLE DIAMETER IN EXISTING CONCRETE SHALL BE DRILLED WITH A BIT COMPLYING WITH ANSI STANDARD B212.15-1994 TO THE SPECIFIED DIAMETER AND DEPTH LISTED IN THE ICC ES REPORT AND MANUFACTURER RECOMMENDATIONS.
3. THE HOLE MUST BE CLEANED USING COMPRESSED AIR AND A NYLON BRUSH.
4. THE CONTRACTOR SHALL FOLLOW ALL RECOMMENDATIONS BY MANUFACTURER DURING EPOXY GROUTING.
5. THE FOLLOWING MINIMUM EMBEDMENT OF GRADE 60 REINFORCING INTO HARD ROCK CONCRETE OR SOLID GROUTED MASONRY SHALL BE AS FOLLOWS, UNLESS NOTED OTHERWISE:

REFER TO ICC ES REPORT FOR EMBED DEPTHS AT SPACING LESS THAN NOTED.

1. CONCRETE BLOCK SHALL BE HOLLOW LOAD-BEARING CONCRETE MASONRY UNITS CONFORMING TO C90 GRADE N, MEDIUM WEIGHT. USE OPEN END UNITS FOR ALL EXTERIOR WALLS, AND BOND BEAM UNITS AT HORIZONTAL REINFORCING.

3. MORTAR SHALL BE AS SPECIFIED FOR CONCRETE.
4. MORTAR MIX SHALL CONFORM TO REQUIREMENTS FOR TYPE S AND PROJECT SPECIFICATIONS. MORTAR SHALL ATTAIN A COMPRESSIVE STRENGTH OF 1900 PSI AT 28 DAYS. ADMIXTURE SHALL BE SIKKA RED LABEL.
5. GROUT SHALL CONFORM TO REQUIREMENTS FOR COARSE GROUT. GROUT SHALL ATTAIN A COMPRESSIVE STRENGTH OF 2,000 PSI AT 28 DAYS. ADMIXTURE SHALL BE SIKKA GROUT A10.
6. ADMIXTURES SHALL BE ADDED TO MORTAR OR GROUT RESPECTIVELY PER MANUFACTURER'S RECOMMENDATIONS.
7. PROVIDE A MINIMUM OF ONE BAR DIAMETER (1/2 INCH MINIMUM) GROUT BETWEEN WALL REINFORCING AND MASONRY UNITS.
8. LOW-IFL BSTRUCTION: MAXIMUM GROUT POUR HEIGHT IS 5 FEET.
9. HIGH-IFL GROUTED CONSTRUCTION MAY BE USED IN CONFORMANCE WITH CHAPTER 24 OF THE GOVERNING CODE.
10. ALL CELLS IN CONCRETE BLOCKS SHALL BE FILLED SOLID WITH GROUT, UNLESS NOTED OTHERWISE.
11. CELLS SHALL BE IN VERTICAL ALIGNMENT. DOMELS IN FOOTINGS SHALL BE SET TO ALIGN WITH CORES CONTAINING REINFORCING STEEL.
12. REFER TO ARCHITECTURAL DRAWING FOR SURFACE AND HEIGHT OF UNITS LAYING PATTERN AND JOINT TYPE.
13. ASSUMED ULTIMATE COMPRESSIVE STRENGTH OF COMPLETED MASONRY WALL IS 1500 PSI U.O.

ANCHOR BOLT	ANB	ANCHOR BOLT	ANB
ARISE	ARI	ARISE AND BELLOW	ARI
ADL	ADL	ADDITIONAL	ADL
ADJ	ADJ	ADJUST	ADJ
ALT	ALT	ALTERNATE	ALT
ANCH	ANCH	ANCHOR	ANCH
ARCH	ARCH	ARCHITECTURAL	ARCH
AS	AS	ASBESTOS	AS
AT	AT	ATMOSPHERE	AT
AV	AV	AVAILABILITY	AV
AW	AW	AWAY	AW
AX	AX	AXIS	AX
AY	AY	AY	AY
BA	BA	BALANCE	BA
BAC	BAC	BALANCE	BAC
BACK	BACK	BACK	BACK
BE	BE	BEARING	BE
BEH	BEH	BEARING	BEH
BEI	BEI	BEARING	BEI
BEL	BEL	BELT	BEL
BEW	BEW	BELT	BEW
BIB	BIB	BIB	BIB
BIG	BIG	BIG	BIG
BIS	BIS	BIS	BIS
BOT	BOT	BOTTOM	BOT
BOU	BOU	BOU	BOU
BOV	BOV	BOV	BOV
BR	BR	BRACE	BR
BRB	BRB	BRACE	BRB
BRK	BRK	BRK	BRK
BRL	BRL	BRL	BRL
BS	BS	BS	BS
BTH	BTH	BTH	BTH
BTO	BTO	BTO	BTO
BTT	BTT	BTT	BTT
BUS	BUS	BUS	BUS
BUW	BUW	BUW	BUW
CA	CA	CA	CA
CAB	CAB	CAB	CAB
CAC	CAC	CAC	CAC
CAD	CAD	CAD	CAD
CAF	CAF	CAF	CAF
CAG	CAG	CAG	CAG
CAH	CAH	CAH	CAH
CAI	CAI	CAI	CAI
CAJ	CAJ	CAJ	CAJ
CAK	CAK	CAK	CAK
CAL	CAL	CAL	CAL
CAM	CAM	CAM	CAM
CAN	CAN	CAN	CAN
CAO	CAO	CAO	CAO
CAP	CAP	CAP	CAP
CAR	CAR	CAR	CAR
CAS	CAS	CAS	CAS
CAT	CAT	CAT	CAT
CAU	CAU	CAU	CAU
CAV	CAV	CAV	CAV
CAX	CAX	CAX	CAX
CAY	CAY	CAY	CAY
CAZ	CAZ	CAZ	CAZ
CB	CB	CB	CB
CBG	CBG	CBG	CBG
CBH	CBH	CBH	CBH
CBK	CBK	CBK	CBK
CBL	CBL	CBL	CBL
CBM	CBM	CBM	CBM
CBN	CBN	CBN	CBN
CBP	CBP	CBP	CBP
CBQ	CBQ	CBQ	CBQ
CBR	CBR	CBR	CBR
CBS	CBS	CBS	CBS
CBT	CBT	CBT	CBT
CBU	CBU	CBU	CBU
CBV	CBV	CBV	CBV
CBW	CBW	CBW	CBW
CBX	CBX	CBX	CBX
CBY	CBY	CBY	CBY
CBZ	CBZ	CBZ	CBZ
CC	CC	CC	CC
CCA	CCA	CCA	CCA
CCB	CCB	CCB	CCB
CCC	CCC	CCC	CCC
CCD	CCD	CCD	CCD
CCF	CCF	CCF	CCF
CCG	CCG	CCG	CCG
CCH	CCH	CCH	CCH
CCI	CCI	CCI	CCI
CCJ	CCJ	CCJ	CCJ
CCK	CCK	CCK	CCK
CCL	CCL	CCL	CCL
CCM	CCM	CCM	CCM
CCN	CCN	CCN	CCN
CCO	CCO	CCO	CCO
CCP	CCP	CCP	CCP
CCQ	CCQ	CCQ	CCQ
CCR	CCR	CCR	CCR
CCS	CCS	CCS	CCS
CCU	CCU	CCU	CCU
CCV	CCV	CCV	CCV
CCW	CCW	CCW	CCW
CCX	CCX	CCX	CCX
CCY	CCY	CCY	CCY
CCZ	CCZ	CCZ	CCZ
CD	CD	CD	CD
CDA	CDA	CDA	CDA
CDB	CDB	CDB	CDB
CDC	CDC	CDC	CDC
CDD	CDD	CDD	CDD
CDE	CDE	CDE	CDE
CDF	CDF	CDF	CDF
CDG	CDG	CDG	CDG
CDH	CDH	CDH	CDH
CDI	CDI	CDI	CDI
CDJ	CDJ	CDJ	CDJ
CDK	CDK	CDK	CDK
CCL	CCL	CCL	CCL
CCM	CCM	CCM	CCM
CCN	CCN	CCN	CCN
CCO	CCO	CCO	CCO
CCP	CCP	CCP	CCP
CCQ	CCQ	CCQ	CCQ
CCR	CCR	CCR	CCR
CCS	CCS	CCS	CCS
CCU	CCU	CCU	CCU
CCV	CCV	CCV	CCV
CCW	CCW	CCW	CCW
CCX	CCX	CCX	CCX
CCY	CCY	CCY	CCY
CCZ	CCZ	CCZ	CCZ
CE	CE	CE	CE
CEA	CEA	CEA	CEA
CEB	CEB	CEB	CEB
CEC	CEC	CEC	CEC
CED	CED	CED	CED
CEE	CEE</		



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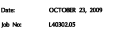


ID DOCUMENTS 10/23/09

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Drawing Title

## GENERAL NOTES

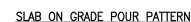
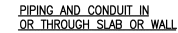
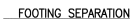
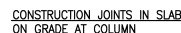
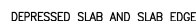
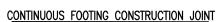


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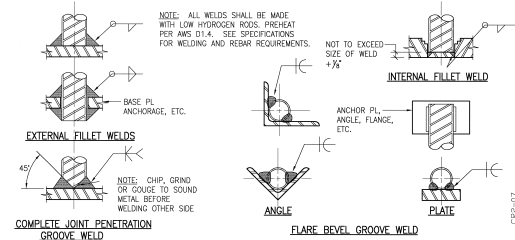
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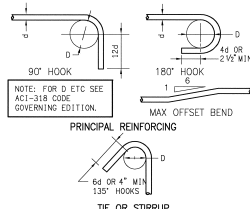






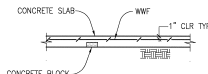


REINFORCING BAR WELDS - BAR TO PLATE OR STEEL SHAPE



NOTES: 1. ALL BENDS SHALL BE MADE COLD  
2. #14 & #18 BARS SHALL BE BEND-TESTED AND APPROVED PRIOR TO BENDING

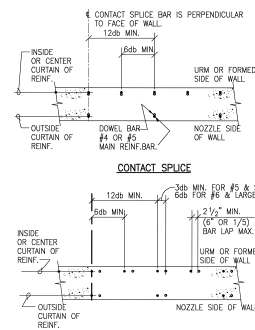
BAR BENDS



TYPICAL SLAB ON GRADE

### SHOTCRETE

- SHOTCRETE MAY BE USED IN LIEU OF SINGLE SIDED CAST-IN-PLACE CONCRETE AT BASEMENT WALLS.
- SHOTCRETE SHALL CONFORM TO ALL REQUIREMENTS OF ACI SECTION 1913, EXCEPT AS MODIFIED BY THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.
- DEFINITIONS:  
SHOTCRETE IS MORTAR OR CONCRETE PNEUMATICALLY PROJECTED AT A HIGH VELOCITY ONTO A SURFACE.  
NET MIX SHOTCRETE IS SHOTCRETE IN WHICH ALL OF THE INGREDIENTS INCLUDING WATER ARE MIXED BEFORE INTRODUCTION INTO THE PLACING EQUIPMENT.  
DRY MIXED SHOTCRETE DESIGNATES A MIXTURE OF PORTLAND CEMENT AND SAND - MIXED DRY, PASSED THROUGH A CEMENT GUN AND CONVEYED BY AIR THROUGH A FLEXIBLE HOSE. HYDRATED AT A NOZZLE ON THE END OF SUCH FLEXIBLE HOSE, AND DEPOSITED BY AIR PRESSURE IN ITS PLACE OF FINAL REPOSE.
- MATERIALS:  
CEMENT: ASTM C150 TYPE V, LOW ALKALI, NO FLY ASH.  
AGGREGATE: ACI 506. GRADATION NO. 1 OR NO. 2, C33.  
WATER: POTABLE, FRESH.
- SHOTCRETE CONTRACTOR MUST SHOW A MINIMUM OF 5 YEARS EXPERIENCE ON BUILDING PROJECTS AND MUST BE APPROVED BY THE ARCHITECT.
- EXISTING CONCRETE THAT IS USED AS A FORM FOR NEW CONCRETE SHALL BE CLEANER OF ALL EXISTING PLASTER OR ANY OTHER FINISH MATERIALS, SANDBLASTED OR WATERBLASTED, AND SATURATED PRIOR TO PLACING CONCRETE. THE EXISTING CONCRETE SHALL BE WETTED DAILY UNTIL THE SURFACE WILL NOT ABSORB MOISTURE. PLACEMENT OF NEW CONCRETE AGAINST THE WETTED SURFACE OF THE CONCRETE SHALL NOT BE DELAYED MORE THAN 3 DAYS AFTER THE LAST APPLICATION OF WATER TO THE SURFACE OF THE EXISTING CONCRETE.
- "ROUGHEN" WHERE INDICATED, MEANS ROUGHENING TO FULL AMPLITUDE OF 1/4".



NOTE:  
1. HORIZ. REIN. REQUIREMENTS ARE SIMILAR.  
2. 6B IS BAR DIAMETER.  
3. CONTACT SPLICE MAY BE USED FOR #4 & #5 REIN.  
4. BARS LARGER THAN #5 MUST USE NON-CONTACT LAP SPLICE.

PLAN - SHOTCRETE WALL REINFORCING DETAIL

TENSION DEVELOPMENT LENGTH SCHEDULE ( $l_{dE}$ )

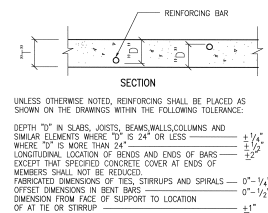
BAR SIZE	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS
#3	22	17	19	15	17	13	15	12	14	12
#4	29	22	25	19	22	17	20	16	19	15
#5	36	28	31	24	28	22	25	20	24	18
#6	43	33	37	29	33	26	31	24	28	22
#7	53	48	54	42	49	37	44	34	41	32
#8	72	55	62	48	55	43	51	39	47	36
#9	81	62	70	54	63	48	57	44	53	41
#10	91	70	79	61	70	54	64	49	58	46
#11	101	78	87	67	78	60	71	55	66	51
#14	121	93	105	81	94	72	86	66	79	61
#18	161	124	139	107	125	96	114	88	106	81

BAR SPLICE LENGTH SCHEDULE

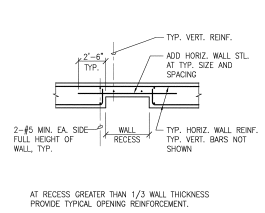
BAR SIZE	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS	TOP OTHER BARS	OTHER TOP OTHER BARS
#3	28	22	24	19	22	17	20	16	18	17
#4	37	29	32	25	29	22	26	20	25	19
#5	47	36	40	31	36	28	33	25	31	24
#6	56	43	48	37	43	33	40	31	37	28
#7	67	51	58	44	51	39	47	36	44	33
#8	83	62	72	55	62	48	57	44	53	41
#9	105	81	91	70	81	63	74	57	69	53
#10	118	91	102	79	91	70	83	64	77	59
#11	131	101	113	87	101	79	93	73	86	66

- NOTES:  
1. LAP SPLICES ARE SHOWN ON DWGS. WHERE NO LAP LENGTH IS SHOWN, USE THIS SCHEDULE.  
2. BAR SPLICE SCHEDULE BASED ON CASE #1; LAP CLASS B  
3. C-C BARS MUST BE 3.0x MIN BY CODE = CASE 1  
4. BAR COVER ON BMS & COLS 1 1/2" + 1/2" = 2" >  $d_b$  = CASE 1 REQUIRED LAP LENGTH.

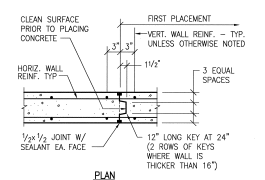
REGULAR WEIGHT CONCRETE REINFORCING DEVELOPMENT LENGTH & SPLICE LENGTH SCHEDULE



TOLERANCES FOR PLACING AND FABRICATION OF REINFORCING BARS

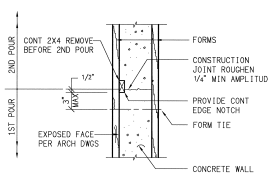


TYPICAL WALL RECESS



NOTE:  
1. PROVIDE CONSTRUCTION JOINT AT 60'-0" MAX  
2. LOCATION AND DETAIL OF JOINTS SHALL BE APPROVED BY ARCHITECT PRIOR TO CONSTRUCTING FORMS OR PLACING CONCRETE

WALL VERTICAL CONSTRUCTION JOINTS



NOTE: PROVIDE CONT 2X4 ON BOTH FACES WHEN BOTH FACES ARE EXPOSED - REMOVE 2X4 AND TIGHTEN FORM TIE BEFORE PLACING 2ND POUR

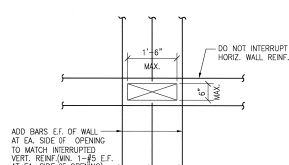
WALL HORIZONTAL CONSTRUCTION JOINTS

CONCRETE WALL REINFORCING SCHEDULE

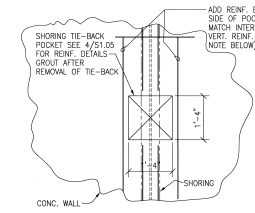
WALL THICKNESS	BAR SIZE & SPACING EACH MAT - $f_y = 60$ KSI	REMARKS
4"	#4 @ 12" VERT	SINGLE MAT
4 1/2" TO 6"	#4 @ 12" VERT	SINGLE MAT
6 1/2" TO 8"	#4 @ 12" VERT	SINGLE MAT
8 1/2" TO 10"	#4 @ 12" VERT	DOUBLE MAT
10 1/2" TO 12"	#4 @ 12" VERT	DOUBLE MAT
12 1/2" TO 14"	#4 @ 12" VERT	DOUBLE MAT
14 1/2" TO 16"	#4 @ 12" VERT	DOUBLE MAT
16 1/2" TO 20"	#4 @ 12" VERT	DOUBLE MAT

NOTES:  
1. THE ABOVE SHALL BE MINIMUM REINFORCING FOR ALL WALLS, SLAB OF PITS AND TRENCHES  
2. SINGLE MAT REINFORCING SHALL BE IN THE CENTER OF WALL UNLESS OTHERWISE DETAILED

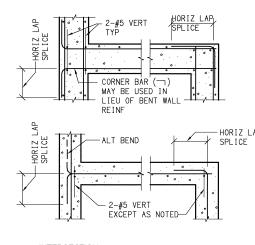
CONCRETE WALL MINIMUM REINFORCING SCHEDULE



TYPICAL WALL/SLAB SMALL OPENING DETAIL



SHORING TIEBACK-POCKET DETAIL



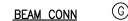
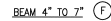
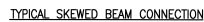
REINFORCING AT WALL INTERSECTIONS



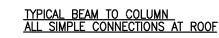


NOTES:

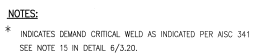
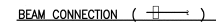
- ## SIMPLE BEAM CONNECTION DETAILS



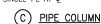
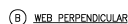
TYPICAL HOLE THRU BEAM WEB DETAIL



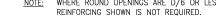
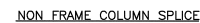
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20



18

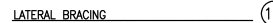
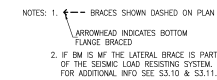
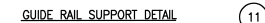
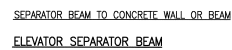
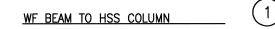
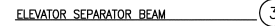


16

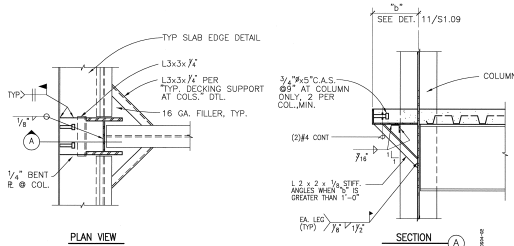






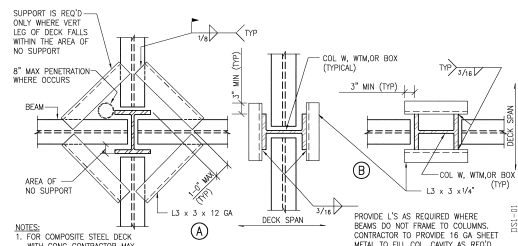






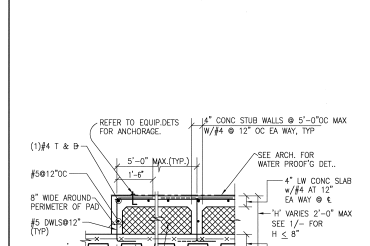
- NOTES:
- 1) SAW AT EXTERIOR CORNER CONDITIONS, AND AT OPPOSITE COL. ORIENTATION.
  - 2) SEE 18/55.02 FOR ALTERNATE DETAIL AT MOMENT FRAMES.

TYPICAL BENT PLATE FORM ANGLE SUPPORTS AT COLUMNS



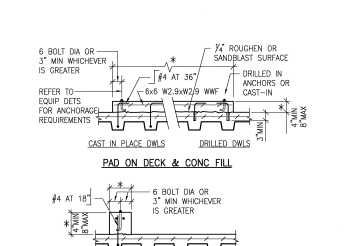
- NOTES:
1. FOR COMPOSITE STEEL DECK WITH CONC CONTRACTOR MAY DELETE ANGLES SHOWN AS REQ'D DURING CONC PLACEMENT.
  2. SEE 18/55.02 FOR ALTERNATE DETAIL AT MOMENT FRAMES.

METAL DECK SUPPORT AT COLUMN



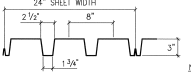
- NOTES:
- 1) SAW AT EXTERIOR CORNER CONDITIONS, AND AT OPPOSITE COL. ORIENTATION.
  - 2) SEE 18/55.02 FOR ALTERNATE DETAIL AT MOMENT FRAMES.

TYP. CONCRETE BUILT-UP SECTION



- NOTES:
- 1) SAW AT EXTERIOR CORNER CONDITIONS, AND AT OPPOSITE COL. ORIENTATION.
  - 2) SEE 18/55.02 FOR ALTERNATE DETAIL AT MOMENT FRAMES.

SUPPORT AT CONCRETE FILL DECK



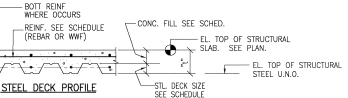
- NOTES:
1. DECK LAYOUT SHALL PROVIDE ALL DECK SHEETS OF SUFFICIENT LENGTH TO EXTEND CONTINUOUSLY OVER AT LEAST 3 SPANS.
  2. ENDS OF ADJOINING DECK SHEETS SHALL BE CENTERED OVER SUPPORTS & ABUTTED OR ACCEPTABLY LAPPED 2". ABUTTED SHEETS REQUIRE 2 TYPICAL WELDS AT EACH WELD LOCATION.
  3. PUDDLE WELDS INDICATED AS 1/2" SHALL MEET THE WELD REQUIREMENTS FOR A FULL EFFECTIVE 1/2" DIAMETER FUSION AREA AT THE FACE OF THE SUPPORT MEMBER, & THE BURNED OUT PORTION OF THE DECK SHEET SHALL BE FILLED WITH METAL WELD ROD MATERIAL TO THE THICKNESS OF THE SHEET WITHOUT POROSITY AT THE EDGE OF THE WELD TO THE SHEET.
  4. DO NOT SUSPEND CEILING, LIGHT FIXTURES & CONDUITS, DUCTS, PIPING, OR OTHER UTILITIES & UTILITY COMPONENTS FROM DECK.
  5. SEE SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS.

3" DECK - SECTION

DECK TYPE	DECK SIZE	CONC. FILL	1"	STEEL DECK PROPERTIES	DECK REINFORCING	MAX. UNSHORED LENGTH (SEE NOTE 1)
						DECK SPAN
MD-1	3"-16GA (N24)	-	3"	S <sub>y</sub> = 0.850 IN <sup>3</sup> S <sub>w</sub> = 1.005 IN <sup>3</sup> I = 1.647 IN <sup>4</sup>	-	8'-0" 10'-0" 11'-0"

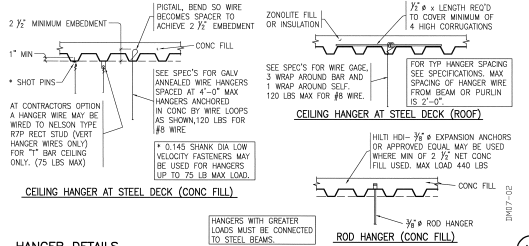
METAL ROOF DECKING SCHEDULE

DECK TYPE	DECK SIZE	CONC. FILL	1"	STEEL DECK PROPERTIES	DECK REINFORCING	MAX. UNSHORED LENGTH (SEE NOTE 1)
						DECK SPAN
D-1	3"-20GA (N42)	3/4" LW	6 1/4"	S <sub>y</sub> = 0.534 IN <sup>3</sup> S <sub>w</sub> = 0.564 IN <sup>3</sup> I = 0.896 IN <sup>4</sup>	6x6-W2.0xW2.0 WWF	1-SPAN 8'-0" 2-SPAN 10'-0" 3-SPAN 11'-0"
D-2	3"-20GA (N42)	2 1/4" LW	4 1/2"	S <sub>y</sub> = 0.361 IN <sup>3</sup> S <sub>w</sub> = 0.37 IN <sup>3</sup> I = 0.423 IN <sup>4</sup>	6x6-W2.0xW2.0 WWF	1-SPAN 7'-0" 2-SPAN 8'-0" 3-SPAN 9'-0"

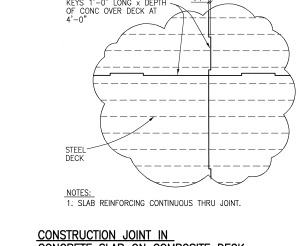


- NOTES:
1. STEEL DECK SHALL BE SHORED @ MIDSPAN WHERE SPAN EXCEEDS MAX UNSHORED LENGTH.
  2. FOR TYPICAL STEEL DECK DETAILS, SEE SHEET 500.09 & 500.10.
  3. FOR TYPICAL WELDED SHEAR STUD LAYOUT, SEE DETAIL 1/500.10.
  4. SEE 11/- & 12/- FOR DECK WELDING.
  5. ALL DECKS BY WERCO OR APPROVED EQUAL.
  6. DECK D-2 IS NOT 2-HOUR RATED.

COMPOSITE STEEL DECK SCHEDULE



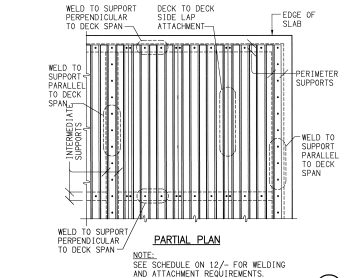
HANGER DETAILS



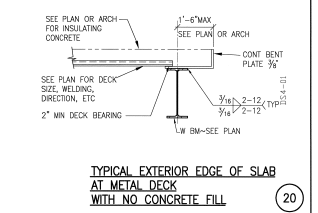
CONSTRUCTION JOINT IN CONCRETE SLAB ON COMPOSITE DECK

LOCATION	W3	3" N-24
PERIMETER FRAMING PARALLEL TO DECK SPAN	3/4" # PUDDLE WELDS #12" O.C.	3/4" # PUDDLE WELDS #12" O.C.
PERIMETER FRAMING PERPENDICULAR TO DECK SPAN	(4)-3/4" # PUDDLE WELDS PER PANEL	(4)-3/4" # PUDDLE WELDS PER PANEL
SUPPORT FRAMING PARALLEL TO DECK SPAN	3/4" # PUDDLE WELDS #12" O.C.	3/4" # PUDDLE WELDS #12" O.C.
SUPPORT FRAMING PERPENDICULAR TO DECK SPAN	(4)-3/4" # PUDDLE WELDS PER PANEL	(4)-3/4" # PUDDLE WELDS PER PANEL
SEAM ATTACHMENT	BUTTON PUNCH #3" @ 12" O.C.	1 1/2" LONG TSW #12" O.C.

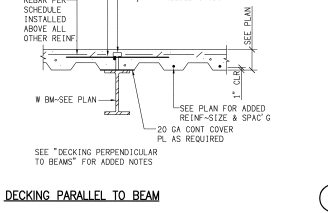
TYP. METAL DECK ATTACHMENT SCHEDULE



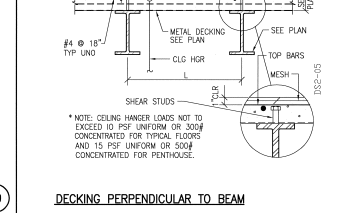
TYPICAL METAL DECK ATTACHMENT PATTERN



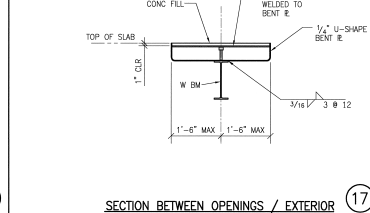
TYPICAL EXTERIOR EDGE OF SLAB AT METAL DECK WITH NO CONCRETE FILL



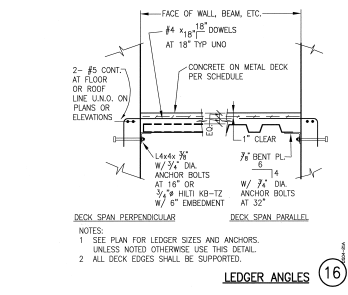
DECKING PARALLEL TO BEAM



DECKING PERPENDICULAR TO BEAM



SECTION BETWEEN OPENINGS / EXTERIOR



LEDGER ANGLES

**ZGF**  
ARCHITECTS LLP

Architects / Planners / Interior Design  
Partner: Susan M. Lippert, Strategic Design Group  
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**CIVIL ENGINEER**  
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**LANDSCAPE ARCHITECT**  
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Marina del Rey, CA 90292  
**LABORATORY**  
Research Facilities Design  
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San Diego, CA 92103-3837  
**LIGHTING DESIGN**  
David Nelson & Associates, LLC  
P.O. Box 270254  
Littleton, CO 80127

**REVISIONS**

NO.	DESCRIPTION	DATE
1	ISSUED FOR PERMIT	10/23/09

**CENTER FOR SCIENCE**  
SAN LUIS OBISPO, CA

**DATE:** OCTOBER 21, 2009  
**JOB NO.:** L409205  
**DESIGNER:**  
**CHECKED BY:**  
**DRAWING NO.:**

**S108**





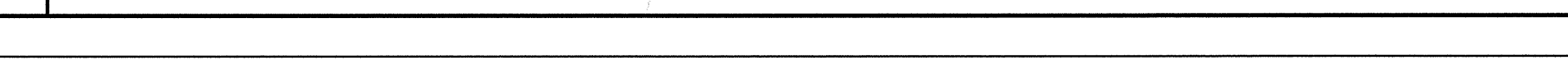




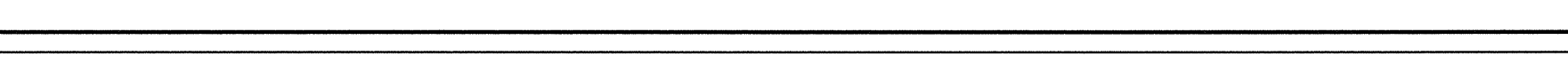












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1212 S. Flower Street  
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**MECHANICAL ENGINEER**  
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Oakland, CA 94607

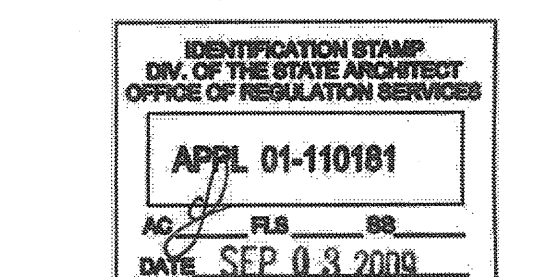
**ELECTRICAL ENGINEER**  
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Santa Clara, CA 95054

**CIVIL ENGINEER**  
Cannon Associates  
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**LANDSCAPE ARCHITECT**  
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**LABORATORY**  
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San Diego, CA 92103-3107

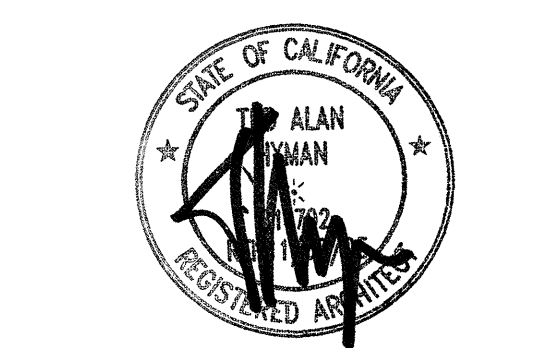
**LIGHTING DESIGN**  
David Nelson & Associates, LLC  
P.O. Box 270254  
Littleton, CO 80127



Revisions  
BD DOCUMENTS 10/23/09

**CENTER FOR SCIENCE**  
SAN LUIS OBISPO, CA

Drawing Title  
**LIFE SAFETY PLAN - FIFTH FLOOR**



Date: OCTOBER 23, 2009  
Job No: L4030205  
Drawn By: TR/CS  
Checked By:  
Drawing No.

A0.15

**SYMBOLS LEGEND**

--- ATRIUM SEPARATION/CONTROL AREA SEPARATION 1 HR. FIRE RATED WALL ASSEMBLY, CBC 404.5 EXCEPTION 3

..... 1 HR. FIRE RATED SEPARATION

--- EXIT ENCLOSURE & SHAFT ENCLOSURES 2 HR. FIRE RATED WALL ASSEMBLY, CBC 707.4 AND 1020.1

--- CONTROL AREA SEPARATION 2 HR. FIRE RATED WALL ASSEMBLY, CBC 414.2.4

◀X DIRECTION OF EGRESS AND NUMBER OF OCCUPANTS USING EGRESS

EXIT SIGN, SINGLE FACE

EXIT SIGN, DOUBLE FACE

POINT OF TWO EXIT OPTIONS

NAME ROOM NAME

AREA ROOM AREA

OC OCCUPANCY LOAD

OC OCCUPANCY LOAD FACTOR

OC OCCUPANCY GROUP

NAME EXIT COMPONENT

OC OCCUPANCY LOAD

OC OCCUPANCY GROUP

OC OCCUPANT TAG

OC EXIT COMPONENT TAG

**MEANS OF EGRESS SYSTEM**

TRAVEL DISTANCE FROM MOST REMOTE POINT TO EXIT MAX. DISTANCE 300'

EXIT ACCESS

INTERVENING SPACE

EXIT DOOR

EXIT STAIR

EXIT STAIR

EXIT DISCHARGE

XX" CPTD=COMMON PATH OF TRAVEL DISTANCE

XX" TD=TRAVEL DISTANCE

EXIT

DISTANCE TO EXIT

PATH OF TRAVEL

MOST REMOTE POINT

**CODE ANALYSIS**

**OCCUPANCY CLASSIFICATIONS**

A-3 SEMINAR ROOM W/OCCUPANT LOAD > 50 CBC 303.1

B MAIN OCCUPANCY CBC 304.1

H-3 HAZARDOUS CBC 307.1

S STORAGE ROOMS CBC 311.1

S-1 MECHANICAL ROOMS CBC 311.2

S-2 ELECTRICAL ROOMS CBC 311.3

**OCCUPANCIES**

**INDICATED ON PLANS.**

**FLOOR AREA CALCULATIONS**

	CALIFORNIA BUILDING CODE	CALIFORNIA PLUMBING CODE
EXTERIOR WALLS	EXCLUDED	EXCLUDED
MECH/OP. EGMT.	EXCLUDED	EXCLUDED
STAIRS	EXCLUDED	EXCLUDED
ELEVATORS	EXCLUDED	EXCLUDED
SHAFTS	EXCLUDED	EXCLUDED
STORAGE	EXCLUDED	EXCLUDED
CLOSETS	EXCLUDED	EXCLUDED
TERRACES	EXCLUDED	EXCLUDED
ATRIUM	EXCLUDED	EXCLUDED
CORRIDORS	EXCLUDED	EXCLUDED
RESTROOMS	EXCLUDED	EXCLUDED
TOTAL AREA	208,608 SF	124,993 SF

AREAS:  
FLOOR AREA OCCUPANCY (CBC SECTION 1002.1)  
LEVEL 1 23,146 SF  
LEVEL 2 43,458 SF  
LEVEL 3 43,209 SF  
LEVEL 4 33,307 SF  
LEVEL 5 25,294 SF  
LEVEL 6 19,958 SF  
ROOF 20,236 SF  
TOTAL 208,608 SF

FLOOR AREA FIXTURE COUNT (CPC)  
LEVEL 1 10,162 SF  
LEVEL 2 31,624 SF  
LEVEL 3 30,086 SF  
LEVEL 4 24,280 SF  
LEVEL 5 14,836 SF  
LEVEL 6 14,005 SF  
ROOF 0 SF  
TOTAL 124,993 SF

FLOOR AREA BY OCCUPANCY (CBC)  
B 108,281 SF  
A-3 12,748 SF  
H-3 985 SF  
S 1,405 SF  
S-1 6,456 SF  
S-2 1,284 SF  
TOTAL 131,159 SF

HIGH-RISE BUILDINGS (NON HIGH-RISE) (CBC 403)

ACTUAL BUILDING HEIGHT (NON-HIGHRISE): 108'-0" 6 STORIES AND PENTHOUSE  
DEFINED BUILDING HEIGHT (NON-HIGHRISE): 64'-0" TO TOP OF HIGHEST OCCUPIED FLOOR/LEVEL ABOVE BUILDING ACCESS.  
(CBC 403.1 EXCEPTION [SFM] 403.1.2)

ALLOWABLE AREA AND HEIGHT (CBC 503/504)

ALLOWABLE HEIGHT AND BUILDING AREAS FOR NON-SEPARATED OCCUPANCIES: (CBC TABLE 503) WITH AUTOMATIC SPRINKLER SYSTEM INCREASE (CBC SECTION 504.2 AND 506.3)

	GROUP B	GROUP S-1
ALLOWABLE MAXIMUM HGT (FT)	160'	180'
ALLOWABLE MAXIMUM STORIES	11	12
ALLOWABLE MAX. AREA/STORY	96,000 (48,000X2)	96,000 (48,000X2)

ACTUAL HEIGHT AND BUILDING AREAS PER CBC TABLE 503:  
CENTER FOR SCIENCE  
ACTUAL MAXIMUM HGT (FT) 108'-0"  
ACTUAL MAXIMUM STORIES 5  
ACTUAL MAX. AREA/STORY 43,458

TOTAL ALLOWABLE BUILDING AREA: 96,000 SF X 6 FLOORS = 576,000 SF  
TOTAL ACTUAL FLOOR AREA = 208,608 SF

ALLOWABLE HEIGHT AND BUILDING AREAS FOR SEPARATED OCCUPANCIES: (CBC SECTION 508.3.3)

FLOOR, HEIGHT AND BUILDING AREAS FOR SEPARATED OCCUPANCIES: (SEE SECTION 508.3.3)					
AREA:	GROUP A-3 (ACTUAL MAX. AREA/ ALLOWABLE MAX. AREA)	GROUP H-3	GROUP S-2	GROUP B	= X < 1
LEVEL 1	10,162/96,000 + 0/96,000	0/96,000	986/96,000	335/UL	= .005 < 1
LEVEL 2	0/96,000	0/96,000	0/96,000	30,020/UL	= .010 < 1
LEVEL 3	943/96,000 + 0/96,000	0/96,000	0/96,000	28,418/UL	= .010 < 1
LEVEL 4	712/96,000 + 0/96,000	0/96,000	0/96,000	22,976/UL	= .007 < 1
LEVEL 5	739/96,000 + 0/96,000	0/96,000	0/96,000	13,435/UL	= .008 < 1
LEVEL 6	192/96,000 + 0/96,000	0/96,000	288/96,000	13,097/UL	= .005 < 1
TOTAL	12,748/96,000 + 985/96,000	0/96,000	1,284/96,000	108,281/UL	= .155 < 2

HEIGHT:

	GROUP A-3	GROUP H-3	GROUP S-2
ALLOWABLE MAXIMUM HGT (FT)	160'	180'	180'
ALLOWABLE MAXIMUM STORIES	12	7	12

CONTROL AREAS (CBC TABLE 414.2.2)

CHEMICAL QUANTITIES, TYPE AND QUANTITY OF CHEMICALS AT OCCUPANCY SHALL NOT EXCEED (CBC TABLE 414.2.5(1))

PLUMBING CALCULATION (CPC TABLE 4-1)

CALCULATIONS BASED ON 2007 CALIFORNIA PLUMBING CODE.

TYPE OF BUILDING OR OCCUPANCY: OFFICE OR PUBLIC BUILDINGS

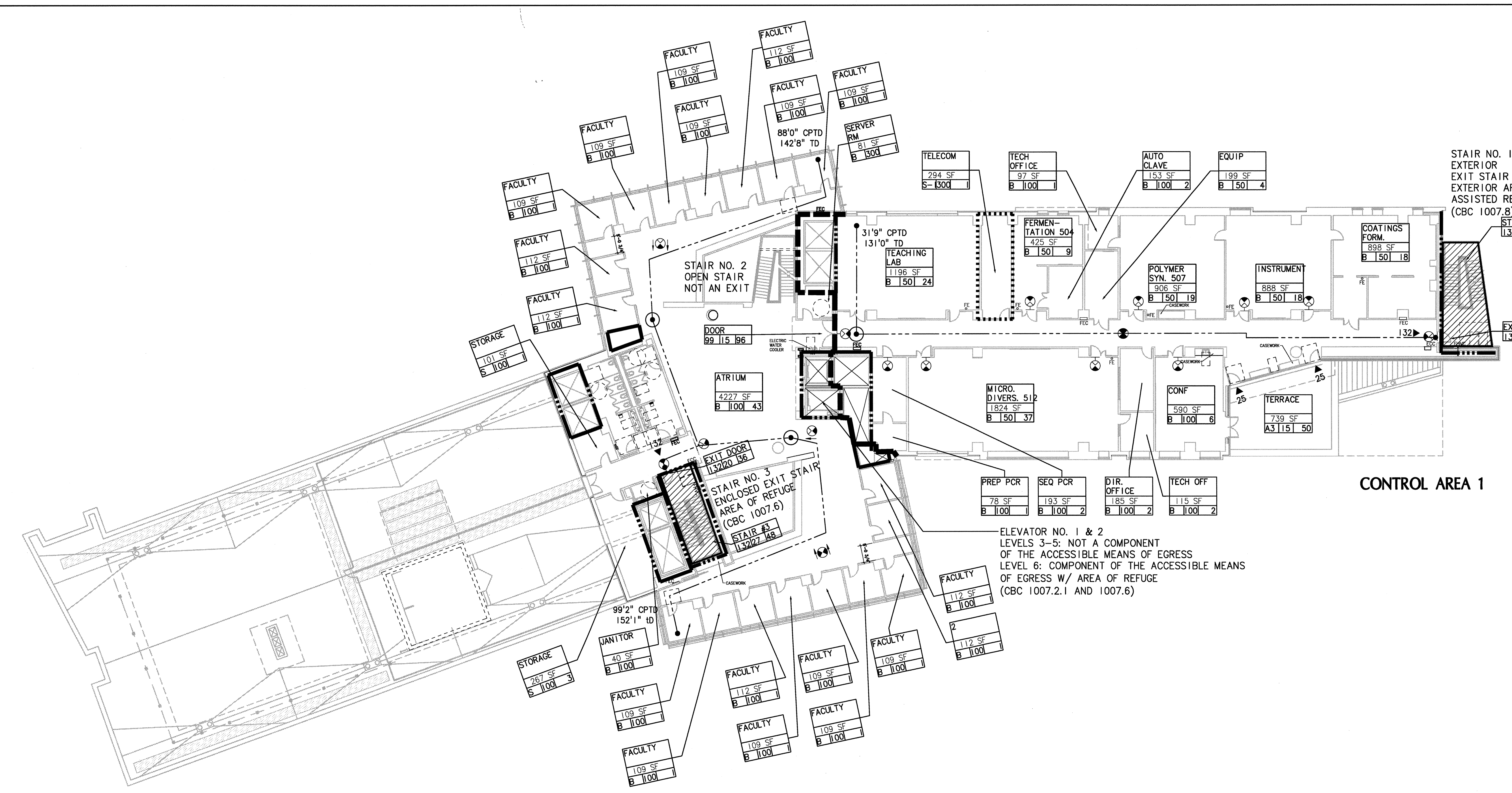
OCCUPANCY LOAD FACTOR: GROUP A-PRINCIPLE ASSEMBLY AREA (NO FIXED SEATING): 30

GROUP A-FIXED SEATING: 1/2 NUMBER OF SEATING

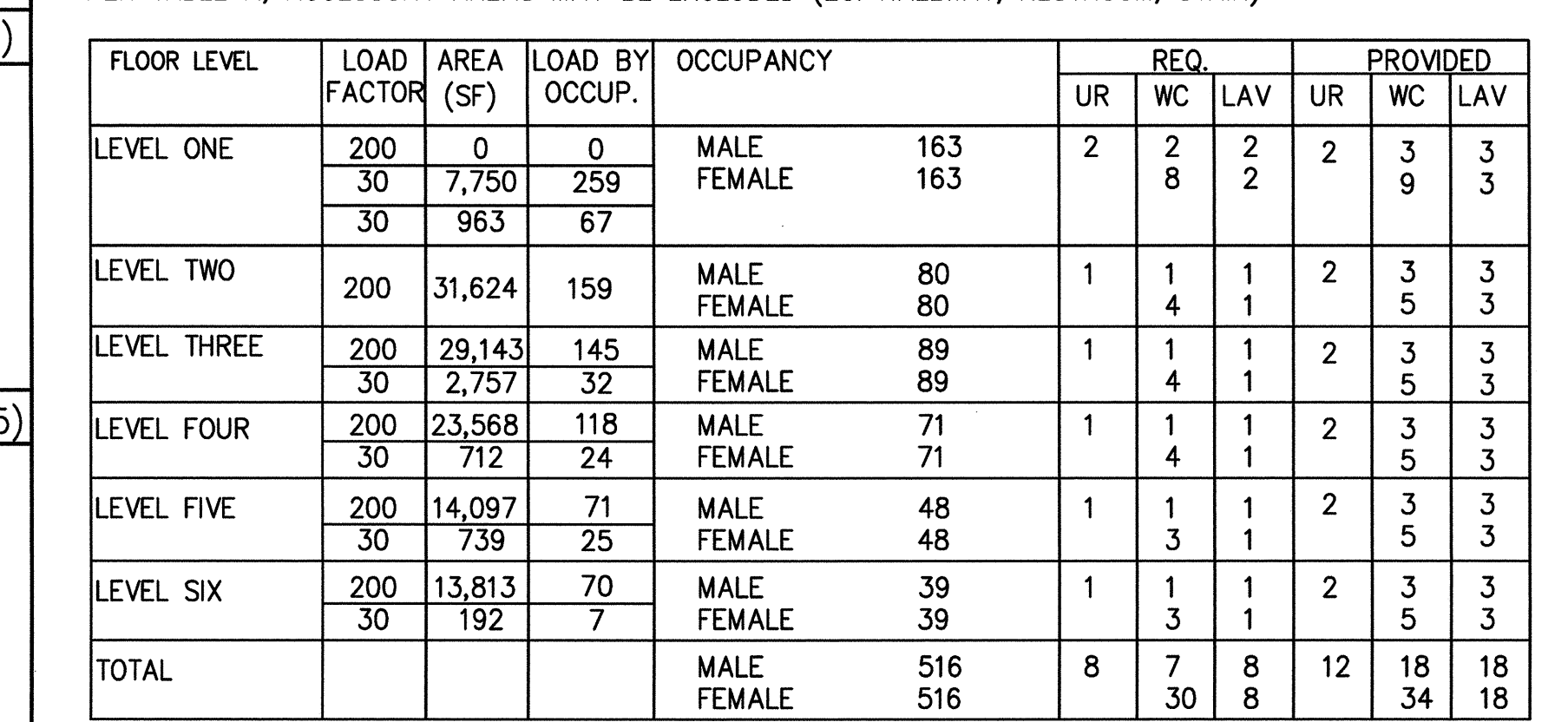
GROUP B-OFFICE OR PUBLIC BUILDINGS: 200

PER TABLE A, ACCESSORY AREAS MAY BE EXCLUDED (EG. HALLWAY, RESTROOM, STAIR)

FLOOR LEVEL	LOAD FACTOR	AREA (SF)	LOAD BY OCC.	OCCUPANCY	UR	REQ. WC	LAV	UR	PROVIDED. WC	LAV
LEVEL ONE	200	0	0	MALE 163	2	2	2	2	3	3
	30	7,750	259	FEMALE 163	8	8	8	8	9	9
	30	963	67							
LEVEL TWO	200	31,624	159	MALE 80	1	1	1	2	3	3
	30	29,143	145	FEMALE 80	4	4	4	5	3	3
LEVEL THREE	200	29,143	145	MALE 89	1	1	1	2	3	3
	30	2,757	32	FEMALE 89	4	4	4	5	3	3
LEVEL FOUR	200	23,568	118	MALE 71	1	1	1	2	3	3
	30	712	24	FEMALE 71	4	4	4	5	3	3
LEVEL FIVE	200	14,097	71	MALE 48	1	1	1	2	3	3
	30	739	25	FEMALE 48	4	4	4	5	3	3
LEVEL SIX	200	13,813	70	MALE 39	1	1	1	2	3	3
	30	192	7	FEMALE 39	3	3	3	5	3	3
TOTAL				MALE 516	8	7	8	12	18	18
				FEMALE 516	30	8	12	34	18	18







A0.16



[illegible]

BY  
**AERO** AUTOMATIC  
SPRINKLER CO.

SECTION 210000— COMMON WORK RESULTS FOR FIRE SUPPRESSION	PART 1 GENERAL 1.3 SHOP DRAWINGS	SECTION 211000— FIRE SUPPRESSION STANDPIPES	PART 1 GENERAL 1.3 SHOP DRAWINGS	SECTION 212000— FIRE SUPPRESSION SPRINKLER SYSTEMS	PART 1 GENERAL 1.3 SHOP DRAWINGS	SECTION 213000— FIRE PUMP	PART 1 GENERAL 1.3 SHOP DRAWINGS
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[illegible]

PROJECT DIRECTORY		PROJECT DATA	
OWNER	CALIFORNIA STATE POLYTECHNIC UNIVERSITY FACILITIES PLANNING & CAPITAL PROJECTS BULWING 75 SAN LEITE OROSP, CA 90427 TEL: (805) 756-2561 FAX: (805) 756-7596	NEW BUILDING DATA NUMBER OF STORIES: PROJECT NUMBER: TYPE CONSTRUCTION: BUILDING OCCUPANCY:	SK (B) STORIES L40920 18: FIRE-RESISTIVE GROUP 1 BUSINESS OCCUPANCY CONTAINING THE FOLLOWING USES:
ARCHITECT	ZIMMER GAMBEL FRASCA ARCHITECTS, LLP 1515 SOUTH FLORIN AVE. SUITE 700 LOS ANGELES, CA 90071 TEL: (310) 437-1861 FAX: (310) 437-0047	USE LOBBIES OFFICES RECEPTION LESS THAN 50 OCCUPANTS LABORATORIES ELECTRONIC DATA TELECOMMUNICATIONS STORAGE STORAGE FIRE PROTECTION: FLOOR AREA:	A-3 B B B B B-1 B-1 B-2 B-2 FULLY FIRE RATED FLOOR AREA
STRUCTURAL ENGINEER	JOHN A. MARTIN & ASSOCIATES 950 S. GRAND AVENUE LOS ANGELES, CA 90015 TEL: (310) 463-6400 FAX: (310) 463-3084	ELEVATOR ELEVATOR ELEVATOR ELEVATOR ELEVATOR ELEVATOR TOTAL:	50.0 21.160 O.S.F. 42.000 O.S.F. 43.200 O.S.F. 33.000 O.S.F. 25.000 O.S.F. 19.800 O.S.F.
MECHANICAL PLUMBING ENGINEER	RUSKEY ENGINEERS 94 LINCOLN VENTURE DRIVE OAKLAND, CA 94607 TEL: (916) 865-2070 FAX: (916) 865-2030	BUILDING CODES: 2007 CBCE: CALIFORNIA BUILDING CODE 2007 CFC: CALIFORNIA FIRE CODE 2007 CFC: CALIFORNIA FIRE CODE 2007 CFC: CALIFORNIA FIRE CODE 2009 NFPA 1: NATIONAL ELECTRICAL CODE 2009 NFPA 10: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 11: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 12: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 13: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 14: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 15: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 16: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 17: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 18: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 19: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 20: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 21: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 22: NATIONAL FIRE PROTECTION ASSOCIATION 2009 NFPA 23: NATIONAL 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## SCOPE OF WORK / HAZARD ANALYSIS

PROVIDE A COMPLETE WET PIPE FIRE SPRINKLER SYSTEM FOR A NEW 6-STORY CLASSROOM/LABORATORY BUILDING WITH FIRE PUMP & CLASS 1 STANDPIPE SYSTEM. ALL SPRINKLER TIE BACK RESPONSES SHALL BE TO CLASS 1 STANDPIPE SYSTEM. SPRINKLERS IN FINISHED CEILING TO BE RECESSED CHROME PENDENT SPRINKLERS. SPRINKLERS IN UNFINISHED AREAS TO BE TYPE 85 CHROME PENDENT SPRINKLERS. PIPING TO BE BLACK STEEL SCHEDULE 10 AND SCHEDULE 40.

**DESIGN CATEGORY:** CLASSIFICATION

CO.	RISQUANCE	HAZARD	MAX. SPACING	DESIGN	NOTE
1	LABORER'S/LECTURE	LDH, HAZARD	225	100/1500	100/0
2	LABORATORY	LDH, HAZARD	150	100/1500	100/0
3	LABORATORIES	LDH, HAZARD	150	150/1500	100/150
4	STORAGE/MECH/ELECT	LDH, QH, DB, 1	150	150/1500	100/150

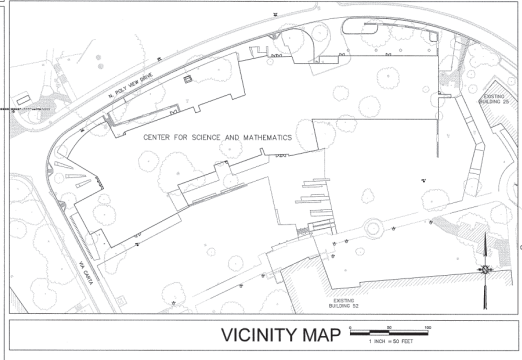
**FLOW TEST INFORMATION:** 150 GPM TO PERCENT

STATISTICAL	50 psi	STATISTICAL	54 psi	TEST DATE: 8-19-2011	9:12 AM
FLOW: 114 gpm		FLOW: 114 gpm		ORIPRICE SIZE: 2 1/2"	
				ORIPRICE DATE: 0.80	

**FLOW TEST PERFORMED BY FLUID RESOURCE MANAGEMENT**  
**NOTE: FLOWING HYDRANT #14 WITH STATIC & RESIDUAL PRESSURE FROM HYDRANT #61**

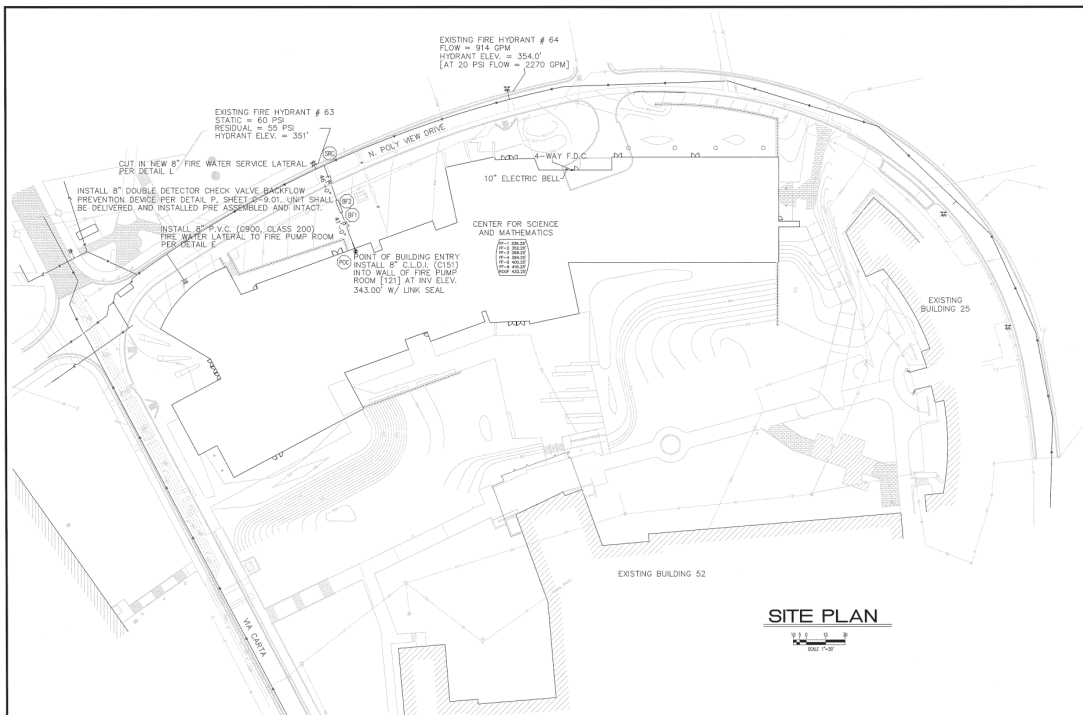
### GENERAL SYSTEM NOTES:

- ALL SYSTEM PIPING SHALL BE HYDROSTATICALLY TESTED AT 200 PSI OR AT 50 PSI ABOVE THE OPERATIONAL STATIC PRESSURE OF THE SYSTEM, WHICHEVER IS GREATER FOR TWO HOURS.
- EACH VALVE SHALL HAVE A PERMANENTLY AFFIXED SIGN INDICATING ITS FUNCTION. ALL SPRINKLER SYSTEM CONTROL VALVE HANDLES TO BE LOCKED IN "W" OR "X" POSITION.
- 2" CHROME OF SPARE SPRINKLERS OF EACH STYLE AND TEMPORARY BRASS PLUGS SHALL BE KEPT IN THE WAREHOUSE. SHALL BE LOCATED NEAR THE RISER WHERE THE TEMPERATURE TO WHICH THEY WILL BE EXPOSED IS 100°F OR GREATER.
- SPRINKLERS SHALL BE QUICK RESPONSE
- SPRINKLERS SHALL BE CHROME RECESSED CHROME PENDENT TYPE 85 OR SHALL BE IN ALUMINUM AND PARALLEL TO THE CEILING. SPRINKLERS SHALL BE LOCATED IN UNFINISHED AREAS TO BE TYCOO MODEL TY-RB QUICK RESPONSE BRASS UPRUSH
- MAIN PIPING FOR THIS SYSTEM SHALL BE SCHEDULE 10 PIPE WITH CHROME FINISH. BRASS BRANCHES SHALL BE SCHEDULE 40 PIPE. BRANCH LINE CONNECTIONS TO THE MAIN SHALL BE PRE-DRILLED AND WELDED. BRANCHES SHALL BE 1/2" TO 2" BLACK STEEL BMT SCHEDULE 40 WITH 1/2" CAST BRONZE BRASS BRANCHES. BRANCHES SHALL BE 1/4" AND LARGER BRANCH LINE A MAIN PIPING TO BE SCHEDULE 10 PIPE. GROUNDED CHROME BRASS GROUND/FIT
- ALL MATERIALS USED IN THE INSTALLATION OF THESE SYSTEMS SHALL BE NEW AND BE OF CURRENT TYPE AND
- ALL MATERIALS SHALL UNDERGO INSPECTION AND (NFA FACTORY MUTUAL) ALL MATERIALS SHALL BE TESTED BY THE MANUFACTURER. ALL MATERIALS SHALL BE 20% ABOVE AS PER THE AUTHORITY. HAVE JURISDICTION
- ALL PIPING SHALL BE SUPPORTED WITH HANGERS IN ACCORDANCE WITH NFPA 13, 2007
- SPACING AND DETAILS OF THE SUPPORT AND BRACING OF FIRE SPRINKLER PIPING SHALL BE IN ACCORDANCE WITH NFPA 13, 2007
- PAINTING OF THE SYSTEM PIPING AND COMPONENTS IS NOT PART OF THE CONTRACT. THE CONTRACTOR SHALL BE PERFORMED BY OTHERS
- UNDERGROUND PIPING IS NOT PART OF THE CONTRACT. THE CONTRACTOR SHALL CONTRACT TO START AT FLANGE (BY OTHERS) AT ABOVE FINISHED FLOOR
- WIRING OF WATERFLOW SWITCH & CONTROL, VALVE TAMPER SWITCHES BY OTHERS. THE ALARM DEVICES TO BE PROVIDED, INSTALLED AND TESTED BY OTHERS

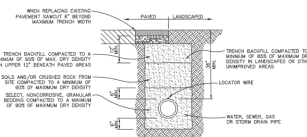
[illegible]

A photograph of a document cover. At the top is a circular seal with the text "OFFICE OF THE ATTORNEY GENERAL" around the perimeter and "STATE OF CALIFORNIA" in the center. Below the seal is a rectangular stamp that reads "RECEIVED" in large letters, with "JUL 10 1963" and "FBI - LOS ANGELES" in smaller text. To the right of the seal is a vertical stamp that reads "CAL POLY CENTER FOR SCIENCE". Below the seal is a rectangular stamp that reads "GILBANE CONSTRUCTION COMPANY, INC." in large letters, with "SAN FRANCISCO, CALIF." and "SAN PABLO, CALIF." in smaller text. At the bottom left is a rectangular stamp that reads "APPRO. 01-10181". At the bottom right is a rectangular stamp that reads "COVER SHEET".





FLOW TEST SUMMARY	
STATIC PSI	60
RESIDUAL PSI	35
PIPE DIA.	8"
LENGTH OF DISCHARGE	172'
FLOW GPM	2270
DATE	8-18-2017
LOCATION	N. POLY VIEW DRIVE
BY WHO	FLUE RESOURCE MANAGEMENT, INC.
ADJUSTED FLOW	
STATIC PSI	60
RESIDUAL PSI	35
GPM	2270
STATIC & RESIDUAL TAKEN FROM HYD. # 63	
FLOW TAKEN FROM HYD. # 64	

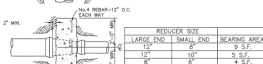
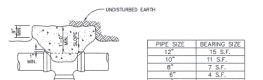


#### NOTES:

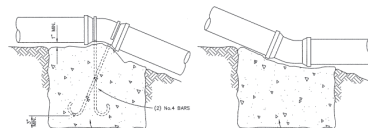
- ALL MATERIAL USED AS TRENCH BEDDING SHALL BE FREE OF STONES, TRUNK, LOGS, PAWNTS AND OTHER MATERIALS, AND SHALL BE CLEANED OF ANY ROCKS AND DEBRIS. MATERIAL LAYER SHALL BE 4 INCHES.
- WHEN BEDDING MATERIAL, INCLUDING BEDDING, THE BEDDING SHALL BE PLACED IN A 10\"/>

PIPE IN TRENCH DETAIL  
N.T.S.

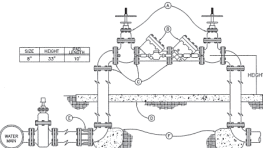
NOTE: UTILITY PLAN PREVIOUSLY APPROVED BY THE OFFICE OF STATE FIRE MARSHAL (FIRE and PANIC ONLY) ON NOV. 10, 2009. THESE DETAILS ARE ALL FROM THAT CIVIL PACKAGE.



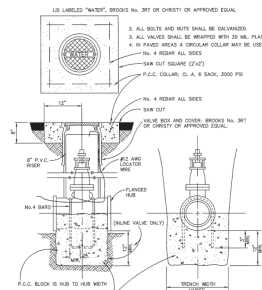
PIPE DIA.	THRUST BLOCK SIZE	BEARING AREA
12"	15 S.F.	
10"	11 S.F.	
8"	7 S.F.	
6"	4 S.F.	



PIPE DIA.	THRUST BLOCK SIZE	BEARING AREA
12"	15 S.F.	
10"	11 S.F.	
8"	7 S.F.	
6"	4 S.F.	



PIPE DIA.	THRUST BLOCK SIZE	BEARING AREA
12"	15 S.F.	
10"	11 S.F.	
8"	7 S.F.	
6"	4 S.F.	



GATE VALVE BOX & ANCHOR  
N.T.S.



NO.	DESCRIPTION	DATE	BY	CHECKED	APPROVED
1	REVISION				
2	REVISION				
3	REVISION				
4	REVISION				
5	REVISION				
6	REVISION				
7	REVISION				
8	REVISION				
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100	REVISION				









## Approved Fire Pumps

1151 N. Pomona Rd., Ste. B Corona, Ca 92882  
Dana Mueller  
Phone 951-738-9100  
Fax 951-7389191

Project : Cal Poly Center for Science

Quote Ref. : UK-999999-1

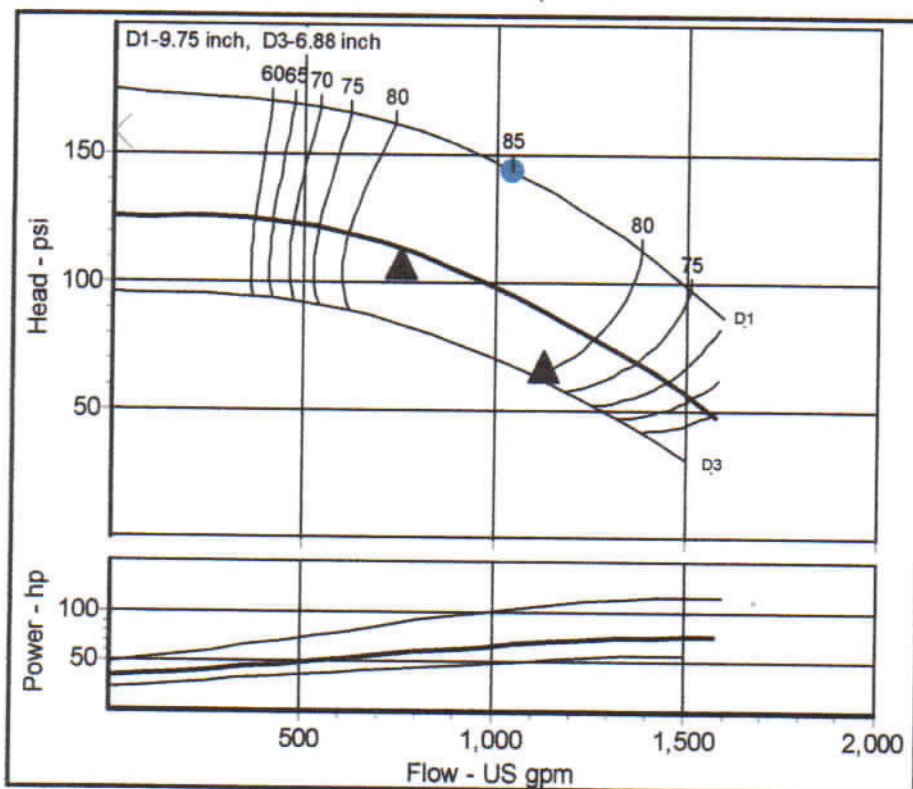
Page No : 1

Date :

Monday, February 28, 2011

Type: PG - In-Line Close Coupled Fire  
Pump Model: 6PVF10  
Pump Op. Speed: 3550 RPM, 60 Hz Electric  
Impeller Dia.: 8.24 inch  
Curve No.: 3116186  
Market: FM/UL/ULC Listed Fire Pump

Item : 1  
Impeller No.: 2699332  
Liquid: Water  
Temperature: 59 °F  
Viscosity: 1.14 cSt  
Sp. Gravity: 1.00  
Your Ref. :



Rated Flow	750 US gpm
Rated Head	113 psi
Imp. Dia.	8.24 inch
Rated Power Required	58.1 hp
Rated Efficiency	85.3 %

<b>NFPA Limits:</b>	
140% Head at shutoff	158.2 psi
65% Head at 150% flow	73.4 psi
Flow at 150%	1125 US gpm
Head at 150%	89 psi
Power Req. at 150%	69.3 hp
Efficiency at 150%	84.5 %
Peak Power	75.4 hp
Closed Valve Pressure	125.2 psi
Approval	UL

### Comments

Performance curve represents typical performance. NPSH data is

Flow (US gpm)	Head (psi)	Pump Efficiency (%)	Power Required (hp)	NPSH Required (ft)
0.0	125.2	0.0	34.7	
197.6	125.2	36.6	39.5	
395.1	124.2	62.8	45.7	
592.7	119.6	78.8	52.6	
790.2	110.9	86.2	59.5	
987.8	98.9	87.0	65.7	
1185.3	84.4	82.8	70.7	
1382.9	67.9	74.2	74.0	
1580.4	48.2	59.1	75.4	







[illegible]



**CAL POLY CENTER FOR SCIENCE**  
 5455 Hill Street, CA  
 91607-1003

**GILBANE CONSTRUCTION**  
 10000 Wilshire Blvd., Suite 100  
 Beverly Hills, CA 90210  
 310-276-1000

**2000 South Central Ave**  
 Phoenix, Arizona 85004  
 602-998-8888  
 AZ-CB-24079  
 06-01-0003

**933.550.7650**  
 Fax 602.998.8884  
 1000 Wilshire  
 Suite 100  
 Beverly Hills, CA 90210

**AUTOMATIC SPRINKLER CO.**

**SPRINKLER HEAD LEGEND**

SIZE	MODEL	TEMP	TYPE	TEST
1/2"	TR-100	132.5 F	DR	UL
3/4"	TR-150	155 F	DR	UL
1"	TR-200	175 F	DR	UL
1 1/2"	TR-250	200 F	DR	UL
2"	TR-300	250 F	DR	UL
2 1/2"	TR-350	325 F	DR	UL
3"	TR-400	375 F	DR	UL
4"	TR-500	425 F	DR	UL
5"	TR-600	525 F	DR	UL
6"	TR-700	625 F	DR	UL
8"	TR-800	725 F	DR	UL
10"	TR-900	825 F	DR	UL
12"	TR-1000	925 F	DR	UL
14"	TR-1100	1025 F	DR	UL
16"	TR-1200	1125 F	DR	UL
18"	TR-1300	1225 F	DR	UL
20"	TR-1400	1325 F	DR	UL
22"	TR-1500	1425 F	DR	UL
24"	TR-1600	1525 F	DR	UL
26"	TR-1700	1625 F	DR	UL
28"	TR-1800	1725 F	DR	UL
30"	TR-1900	1825 F	DR	UL
32"	TR-2000	1925 F	DR	UL
34"	TR-2100	2025 F	DR	UL
36"	TR-2200	2125 F	DR	UL
38"	TR-2300	2225 F	DR	UL
40"	TR-2400	2325 F	DR	UL
42"	TR-2500	2425 F	DR	UL
44"	TR-2600	2525 F	DR	UL
46"	TR-2700	2625 F	DR	UL
48"	TR-2800	2725 F	DR	UL
50"	TR-2900	2825 F	DR	UL
52"	TR-3000	2925 F	DR	UL
54"	TR-3100	3025 F	DR	UL
56"	TR-3200	3125 F	DR	UL
58"	TR-3300	3225 F	DR	UL
60"	TR-3400	3325 F	DR	UL
62"	TR-3500	3425 F	DR	UL
64"	TR-3600	3525 F	DR	UL
66"	TR-3700	3625 F	DR	UL
68"	TR-3800	3725 F	DR	UL
70"	TR-3900	3825 F	DR	UL
72"	TR-4000	3925 F	DR	UL
74"	TR-4100	4025 F	DR	UL
76"	TR-4200	4125 F	DR	UL
78"	TR-4300	4225 F	DR	UL
80"	TR-4400	4325 F	DR	UL
82"	TR-4500	4425 F	DR	UL
84"	TR-4600	4525 F	DR	UL
86"	TR-4700	4625 F	DR	UL
88"	TR-4800	4725 F	DR	UL
90"	TR-4900	4825 F	DR	UL
92"	TR-5000	4925 F	DR	UL
94"	TR-5100	5025 F	DR	UL
96"	TR-5200	5125 F	DR	UL
98"	TR-5300	5225 F	DR	UL
100"	TR-5400	5325 F	DR	UL
102"	TR-5500	5425 F	DR	UL
104"	TR-5600	5525 F	DR	UL
106"	TR-5700	5625 F	DR	UL
108"	TR-5800	5725 F	DR	UL
110"	TR-5900	5825 F	DR	UL
112"	TR-6000	5925 F	DR	UL
114"	TR-6100	6025 F	DR	UL
116"	TR-6200	6125 F	DR	UL
118"	TR-6300	6225 F	DR	UL
120"	TR-6400	6325 F	DR	UL
122"	TR-6500	6425 F	DR	UL
124"	TR-6600	6525 F	DR	UL
126				

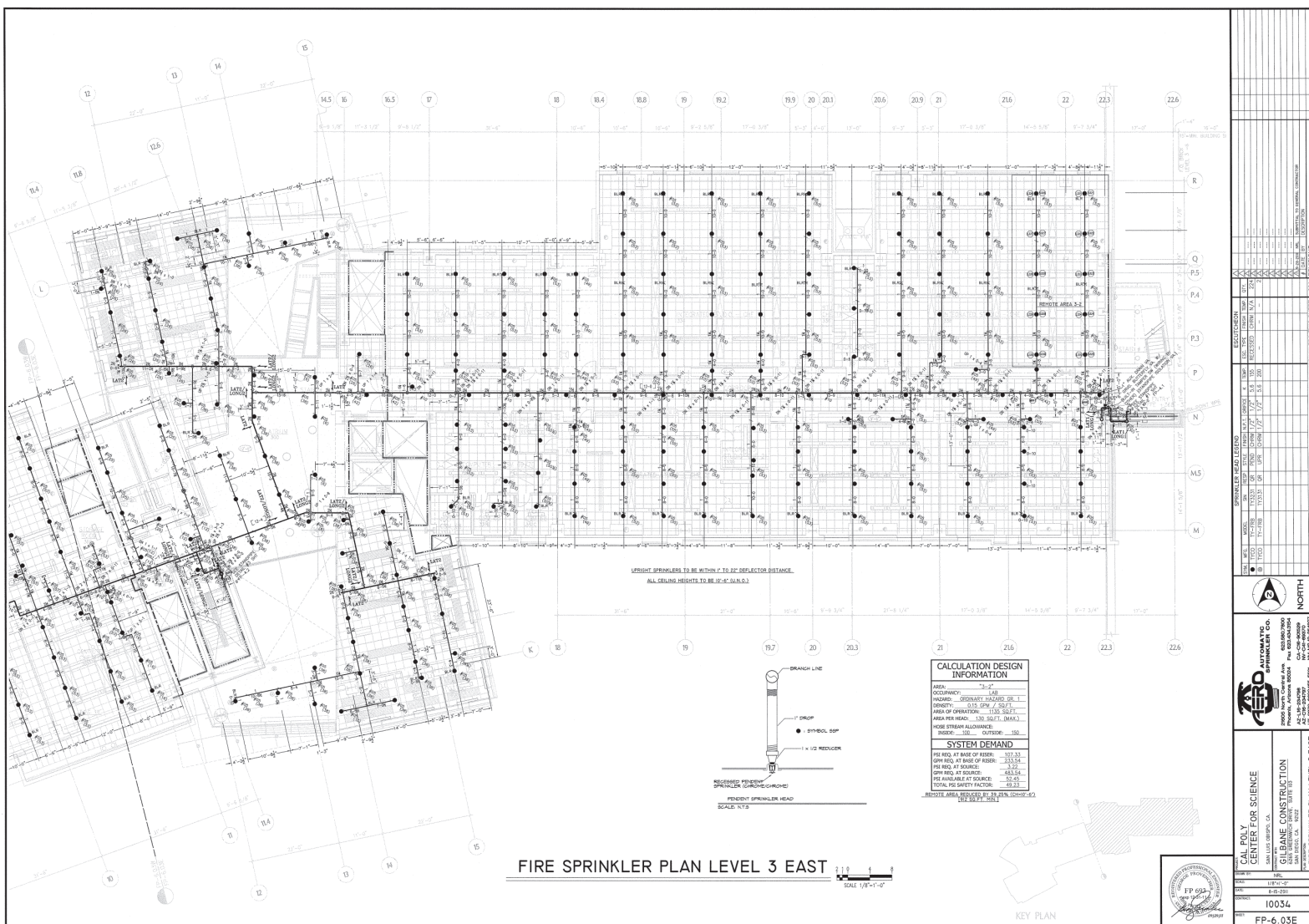




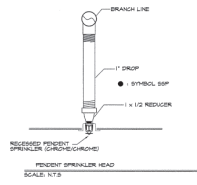












UPRIST SPRINKLERS TO BE WITHIN 4' TO 24' DEFLECTOR DISTANCE.  
ALL CEILING HEIGHTS TO BE 10'-0\"/>

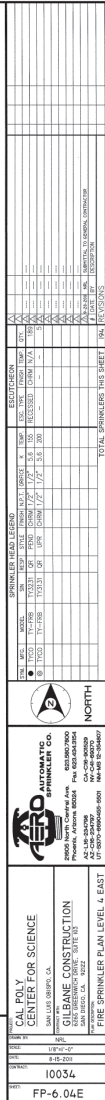
**FIRE SPRINKLER PLAN LEVEL 4 WEST**

KEY PLAN

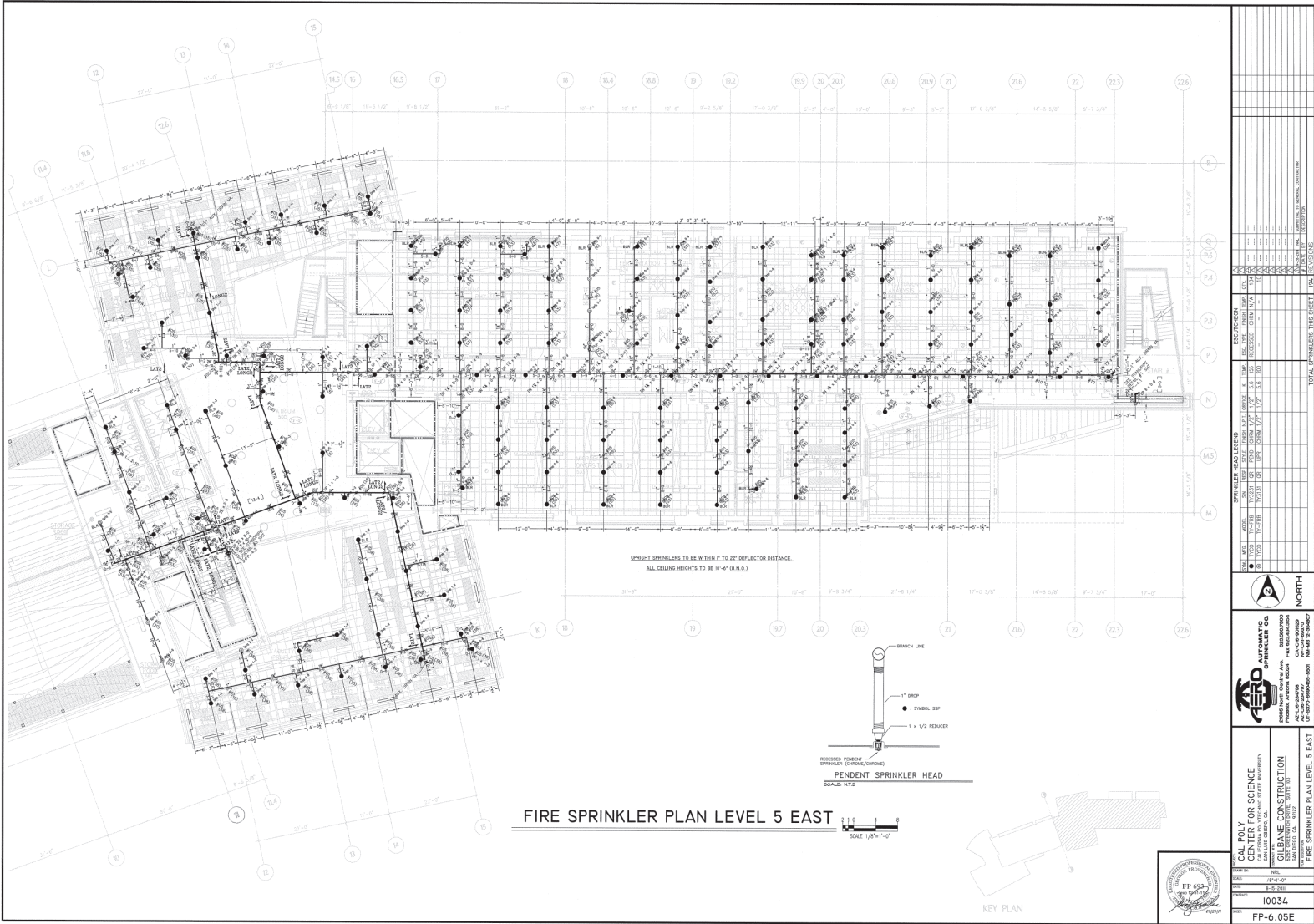


<b>CAL POLY CENTER FOR SCIENCE</b> 10000 Van Nuys Blvd., Suite 100 Van Nuys, CA 91411 (818) 709-1000	
<b>GILBANE CONSTRUCTION</b> 10000 Van Nuys Blvd., Suite 100 Van Nuys, CA 91411 (818) 709-1000	
<b>FP-6, 04W</b> FIRE SPRINKLER PLAN LEVEL 4 WEST	
SHEET NO. 10034	TOTAL SPRINKLERS THIS SHEET 18









NO.	REVISION	DATE	BY	CHKD.	DESCRIPTION
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**CAL POLY CENTER FOR SCIENCE**  
1000 S. STATE ST., SUITE 100  
SAN LUIS OBISPO, CA 94905  
TEL: 805/893-1000  
WWW.CALPOLY.EDU

**GILBANE CONSTRUCTION**  
20000 N. Central Ave.  
SAN ANTONIO, TX 78248  
TEL: 214/343-1000  
WWW.GILBANE.COM

**FIRE SPRINKLER PLAN LEVEL 5 EAST**

PROJECT: 10034

DATE: 8-10-2011

SCALE: 1/8" = 1'-0"

FP 6034

10034

FP-6, 05E



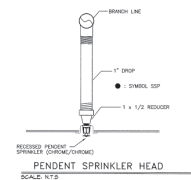
CALCULATION DESIGN INFORMATION	
AREA:	76,477
OCCUPANCY:	OFFICE / RETAIL
HAZARD:	LIGHT HAZARD
DENSITY:	0.15 GPM / SQ.FT.
AREA OF OPERATION:	3,500 SQ.FT.
AREA PER HEAD:	210 SQ.FT. (MAX.)
HOSE STREAM ALLOWANCE:	
INDOOR:	150
OUTDOOR:	150
SYSTEM DEMAND	
PSI REQ. AT BASE OF RISER:	118.88
SPR REQ. AT BASE OF RISER:	247.7
PSI REQ. AT SOURCE:	25.75
SPR REQ. AT SOURCE:	247.7
PSI AVAILABLE AT SOURCE:	53.80
TOTAL PSI SAFETY FACTOR:	13.53

CALCULATION DESIGN INFORMATION	
AREA:	76,477
OCCUPANCY:	LAB
HAZARD:	STRENGTH HAZARD (SLS)
DENSITY:	0.15 GPM / SQ.FT.
AREA OF OPERATION:	3,500 SQ.FT.
AREA PER HEAD:	210 SQ.FT. (MAX.)
HOSE STREAM ALLOWANCE:	
INDOOR:	150
OUTDOOR:	150
SYSTEM DEMAND	
PSI REQ. AT BASE OF RISER:	109.4
SPR REQ. AT BASE OF RISER:	237.4
PSI REQ. AT SOURCE:	25.75
SPR REQ. AT SOURCE:	237.4
PSI AVAILABLE AT SOURCE:	53.80
TOTAL PSI SAFETY FACTOR:	10.4

CALCULATION DESIGN INFORMATION	
AREA:	76,477
OCCUPANCY:	LAB
HAZARD:	STRENGTH HAZARD (SLS)
DENSITY:	0.15 GPM / SQ.FT.
AREA OF OPERATION:	3,500 SQ.FT.
AREA PER HEAD:	210 SQ.FT. (MAX.)
HOSE STREAM ALLOWANCE:	
INDOOR:	150
OUTDOOR:	150
SYSTEM DEMAND	
PSI REQ. AT BASE OF RISER:	109.4
SPR REQ. AT BASE OF RISER:	237.4
PSI REQ. AT SOURCE:	25.75
SPR REQ. AT SOURCE:	237.4
PSI AVAILABLE AT SOURCE:	53.80
TOTAL PSI SAFETY FACTOR:	10.4

CALCULATION DESIGN INFORMATION	
AREA:	76,477
OCCUPANCY:	OFFICE
HAZARD:	LIGHT HAZARD
DENSITY:	0.15 GPM / SQ.FT.
AREA OF OPERATION:	3,500 SQ.FT.
AREA PER HEAD:	210 SQ.FT. (MAX.)
HOSE STREAM ALLOWANCE:	
INDOOR:	150
OUTDOOR:	150
SYSTEM DEMAND	
PSI REQ. AT BASE OF RISER:	118.88
SPR REQ. AT BASE OF RISER:	247.7
PSI REQ. AT SOURCE:	25.75
SPR REQ. AT SOURCE:	247.7
PSI AVAILABLE AT SOURCE:	53.80
TOTAL PSI SAFETY FACTOR:	13.53

SPRINKLER HEADS TO BE WITHIN 4'-0" REFLECTOR DISTANCE.  
ALL CEILING HEIGHTS TO BE 8'-0" (MIN.)



## FIRE SPRINKLER PLAN LEVEL 6 EAST

SCALE: 1/8"=1'-0"

KEY PLAN



CAL POLY  
CENTER FOR SCIENCE  
STATE UNIVERSITY  
SAN LUIS OBISPO, CA 93406  
PROJECT NO. 10034  
DATE: 08/20/2019  
BY: J. GILBERT  
CHECKED: J. GILBERT  
APPROVED: J. GILBERT  
FIRE SPRINKLER PLAN LEVEL 6 EAST  
FP-6.06E

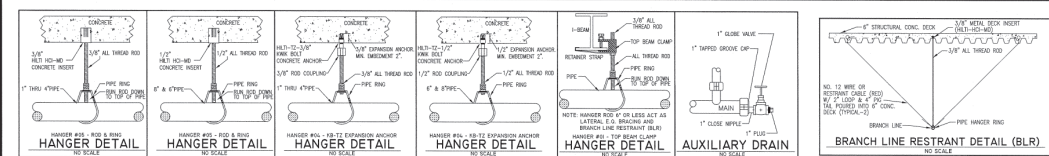


SPRINKLER PLAN LEGEND	
SPRINKLER HEAD	SYMBOL
BRANCH LINE	SYMBOL
1" DROP	SYMBOL
1 1/2" REDUCER	SYMBOL
PENDANT SPRINKLER HEAD	SYMBOL

SPRINKLER PLAN LEGEND	
SPRINKLER HEAD	SYMBOL
BRANCH LINE	SYMBOL
1" DROP	SYMBOL
1 1/2" REDUCER	SYMBOL
PENDANT SPRINKLER HEAD	SYMBOL

SPRINKLER PLAN LEGEND	
SPRINKLER HEAD	SYMBOL
BRANCH LINE	SYMBOL
1" DROP	SYMBOL
1 1/2" REDUCER	SYMBOL
PENDANT SPRINKLER HEAD	SYMBOL





Tol-Brace Seismic Calculations		
Project Address: Cal Poly Center for Science California Polytechnic State University San Luis Obispo, CA 360 P 1000A Calculations based on 2007 NFPA Paragraphs		
Tolco Component Fig. Number		
Maximum Spacing	45' (21.31 ft)	Adjusted Load
Maximum Brace Length	7' (3.31 ft)	Fig. 900 Universal Detail
Bracing Material	Fig. 900 Universal Detail	1500 lbs (680 kg)
Angle from Vertical	30°	
Least Rod of Operation	5/8" (1.27 in)	
L/R Value	200	
Max Horizontal Load	1500 lbs (680 kg)	
Force Factor (C)	0.65	
Fastener Information		
Fastener Orientation	90°/180°	
Type	16/32/12	
Diameter	1/2"	
Length	3.31"	
Maximum Load	1500 lbs (680 kg)	
Load Information		
Size and Type of Pipe	Total Length	Total Calculated Load
1" NPS 40 Steel Pipe (10.24 m)	1500 ft (457 m)	1500 lbs (680 kg)
Percentage added for Pile-ups and Splices	15%	1500 lbs (680 kg)
Total Adjusted Load of all pipe within Zone of Influence	1500 lbs (680 kg)	

Tol-Brace Seismic Calculations		
Project Address: Cal Poly Center for Science California Polytechnic State University San Luis Obispo, CA 360 P 1000A Calculations based on 2007 NFPA Paragraphs		
Tolco Component Fig. Number		
Maximum Spacing	45' (21.31 ft)	Adjusted Load
Maximum Brace Length	7' (3.31 ft)	Fig. 900 Universal Detail
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Max Horizontal Load	1500 lbs (680 kg)	
Force Factor (C)	0.65	
Fastener Information		
Fastener Orientation	90°/180°	
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Length	3.31"	
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Percentage added for Pile-ups and Splices	15%	1500 lbs (680 kg)
Total Adjusted Load of all pipe within Zone of Influence	1500 lbs (680 kg)	

SPRINKLER PIPE HANGER SPACING		
N.F.P.A. 13, 2007 EDITION		
TABLE 9.2.2.1 MAXIMUM DISTANCE BETWEEN HANGERS (FT-IN.)		
MINIMUM PIPE SIZE	3/4"	1"
STEEL PIPE	12'-0"	15'-0"
THICKWALL	12'-0"	15'-0"
COPPER TUBE	12'-0"	15'-0"
FIGURE A-9.2.3.4 DISTANCE FROM SPRINKLER TO HANGER		
CPVC	3'-6"	6'-0"
STEEL	3'-6"	6'-0"
THICKWALL	3'-6"	6'-0"
COPPER TUBE	3'-6"	6'-0"

SWAY BRACING		
Project Address: Cal Poly Center for Science California Polytechnic State University San Luis Obispo, CA 360 P 1000A Calculations based on 2007 NFPA Paragraphs		
Tolco Component Fig. Number		
Maximum Spacing	45' (21.31 ft)	Adjusted Load
Maximum Brace Length	7' (3.31 ft)	Fig. 900 Universal Detail
Bracing Material	Fig. 900 Universal Detail	1500 lbs (680 kg)
Angle from Vertical	30°	
Least Rod of Operation	5/8" (1.27 in)	
L/R Value	200	
Max Horizontal Load	1500 lbs (680 kg)	
Force Factor (C)	0.65	
Fastener Information		
Fastener Orientation	90°/180°	
Type	16/32/12	
Diameter	1/2"	
Length	3.31"	
Maximum Load	1500 lbs (680 kg)	
Load Information		
Size and Type of Pipe	Total Length	Total Calculated Load
1" NPS 40 Steel Pipe (10.24 m)	1500 ft (457 m)	1500 lbs (680 kg)
Percentage added for Pile-ups and Splices	15%	1500 lbs (680 kg)
Total Adjusted Load of all pipe within Zone of Influence	1500 lbs (680 kg)	

SEISMIC CRITERIA		
SEISMIC DESIGN CATEGORY	D	
SEISMIC IMP. FACTOR	1.0	
SITE SOIL PROFILE TYPE	SDS	
SPECTRAL RESPONSE ACCELERATIONS	0.15	
SEISMIC COEFFICIENT	0.15	
*S & S1 VALUES TAKEN FROM STRUCTURAL DRAWING		
*S1 - S1 - DATED 10-20-2005		
*VALUE INTERPOLATED FROM TABLE 3.3.5.2.2 OF N.F.P.A.		

WEIGHT OF WATER FILLED PIPE [ LB./FT. ]		
WEATHER OR GROUNDED PIPE	SCHEDULE 40	SCHEDULE 80
12"	13.4	13.4
14"	15.4	15.4
16"	17.4	17.4
18"	19.4	19.4
20"	21.4	21.4
22"	23.4	23.4
24"	25.4	25.4
26"	27.4	27.4
28"	29.4	29.4
30"	31.4	31.4
32"	33.4	33.4
34"	35.4	35.4
36"	37.4	37.4
38"	39.4	39.4
40"	41.4	41.4
42"	43.4	43.4
44"	45.4	45.4
46"	47.4	47.4
48"	49.4	49.4
50"	51.4	51.4
52"	53.4	53.4
54"	55.4	55.4
56"	57.4	57.4
58"	59.4	59.4
60"	61.4	61.4
62"	63.4	63.4
64"	65.4	65.4
66"	67.4	67.4
68"	69.4	69.4
70"	71.4	71.4
72"	73.4	73.4
74"	75.4	75.4
76"	77.4	77.4
78"	79.4	79.4
80"	81.4	81.4
82"	83.4	83.4
84"	85.4	85.4
86"	87.4	87.4
88"	89.4	89.4
90"	91.4	91.4
92"	93.4	93.4
94"	95.4	95.4
96"	97.4	97.4
98"	99.4	99.4
100"	101.4	101.4

Tol-Brace Seismic Calculations		
Project Address: Cal Poly Center for Science California Polytechnic State University San Luis Obispo, CA 360 P 1000A Calculations based on 2007 NFPA Paragraphs		
Tolco Component Fig. Number		
Maximum Spacing	45' (21.31 ft)	Adjusted Load
Maximum Brace Length	7' (3.31 ft)	Fig. 900 Universal Detail
Bracing Material	Fig. 900 Universal Detail	1500 lbs (680 kg)
Angle from Vertical	30°	
Least Rod of Operation	5/8" (1.27 in)	
L/R Value	200	
Max Horizontal Load	1500 lbs (680 kg)	
Force Factor (C)	0.65	
Fastener Information		
Fastener Orientation	90°/180°	
Type	16/32/12	
Diameter	1/2"	
Length	3.31"	
Maximum Load	1500 lbs (680 kg)	
Load Information		
Size and Type of Pipe	Total Length	Total Calculated Load
1" NPS 40 Steel Pipe (10.24 m)	1500 ft (457 m)	1500 lbs (680 kg)
Percentage added for Pile-ups and Splices	15%	1500 lbs (680 kg)
Total Adjusted Load of all pipe within Zone of Influence	1500 lbs (680 kg)	

Tol-Brace Seismic Calculations		
Project Address: Cal Poly Center for Science California Polytechnic State University San Luis Obispo, CA 360 P 1000A Calculations based on 2007 NFPA Paragraphs		
Tolco Component Fig. Number		
Maximum Spacing	45' (21.31 ft)	Adjusted Load
Maximum Brace Length	7' (3.31 ft)	Fig. 900 Universal Detail
Bracing Material	Fig. 900 Universal Detail	1500 lbs (680 kg)
Angle from Vertical	30°	
Least Rod of Operation	5/8" (1.27 in)	
L/R Value	200	
Max Horizontal Load	1500 lbs (680 kg)	
Force Factor (C)	0.65	
Fastener Information		
Fastener Orientation	90°/180°	
Type	16/32/12	
Diameter	1/2"	
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Tol-Brace Seismic Calculations		
Project Address: Cal Poly Center for Science California Polytechnic State University San Luis Obispo, CA 360 P 1000A Calculations based on 2007 NFPA Paragraphs		
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Force Factor (C)	0.65	
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Load Information		
Size and Type of Pipe	Total Length	Total Calculated Load
1" NPS 40 Steel Pipe (10.24 m)	1500 ft (457 m)	1500 lbs (680 kg)
Percentage added for Pile-ups and Splices	15%	1500 lbs (680 kg)
Total Adjusted Load of all pipe within Zone of Influence	1500 lbs (680 kg)	





FIELD ADJUSTABLE PRESSURE REDUCING

## Field Adjustable Pressure Reducing (URFA)

Elkhart's URFA valve is a true pressure reducing valve, operated automatically by inner hydraulic controls. While the valves are preset at the factory, they are field adjustable — allowing you to tailor the pressure to your needs. They feature manual valve open and close, as well as pressure adjustment — all of which require extremely low torque to change due to the patent pending design. Inlet pressure up to 400 psi (27.58 bar) is controlled under all flow and no-flow conditions.

Valve size and weight permit installation in significantly tighter areas and smaller hose cabinets (those used for 1½" or 2½" valves) — allowing savings of both space and money. The URFA also functions as a floor control valve in automatic sprinkler systems as well as a standpipe valve or hose valve for Class I and Class III systems.





INLET SIZE	OUTLET SIZES	TYPE	CERT.	DIMENSIONS (INCHES)										FINISH			Wt. (Lbs.)	MODEL	FIGURE
2½" F	2½"	Angled	Straight	UL Listed	Closed		Open		C	D	E	F	Integral Superv. Switch	Brass		Chrome			
NPT*	F (NPT)* M (NHT)				A	B	A	B						Cast	Pol	Pol			
•	•	•	•	•	13⅞	11⅞	14¼	12¼	2⅞	3¼	5	4¼	o	s	o	o	18½	URFA-20-2.5	1
•	•	•	•	•	13⅞	11⅞	14¼	12¼	2⅞	3⅞	5	4¼	o	s	o	o	18½	URFA-25-2.5	2
•	•	•	•	•	14½	11⅞ <sub>32</sub>	15⅞	12¼	3½	4	5	4¼	o	s	o	o	26½	URFA-20S-2.5	3

KEY s = standard o = option

\* Grooved connection available for inlet or outlet use — add 1.44" per connection.

Figure 1

URFA-20-2.5

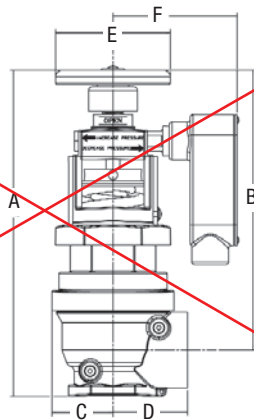


Fig. 1

Figure 2

URFA-25-2.5

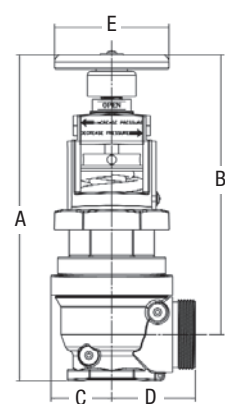


Fig. 2

Figure 3

URFA-20S-2.5

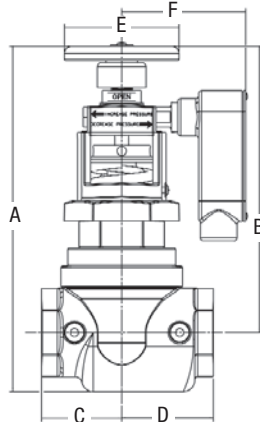


Fig. 3

### PRODUCT HIGHLIGHTS

URFA features include:

- Manual open-close requires less than 15 lbs. of torque
- Pressure rated up to 400 psi (27.58 bar)
- Flow rated up to 500 gpm (1893 lpm)
- Open-Close indication from 2 view directions
- Color-coded pressure reduction label
- Tapped for pressure gauge on both inlet and outlet side of valve
- Tamper-resistant protection
- UL Listed as a check valve for use in dual riser systems
- Optional integral supervisory switch (alarm) mounts directly to valve with no bracket required
- Optional integral supervisory switch (alarm) is available either "OPEN TO SIGNAL" or "CLOSE TO SIGNAL"
  - With the valve in the open position, to close an electrical circuit and send the signal is defined as "OPEN TO SIGNAL"
  - With the valve in the closed position, to close an electrical circuit and send a signal is defined as "CLOSE TO SIGNAL"

### ADDITIONAL INFORMATION

Includes adjustment rod.

### THREADS

- Valve inlet information is NPT unless otherwise specified. Special threads available through adapter use.
- See index T-12 for alternative outlet thread options.





# **Elkhart Brass**

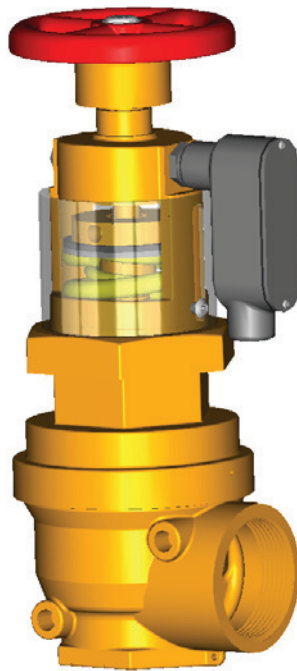
**Fire Fighting Equipment**

URFA –20S-2.5”

URFA-20-2.5”

URFA-25-2.5”

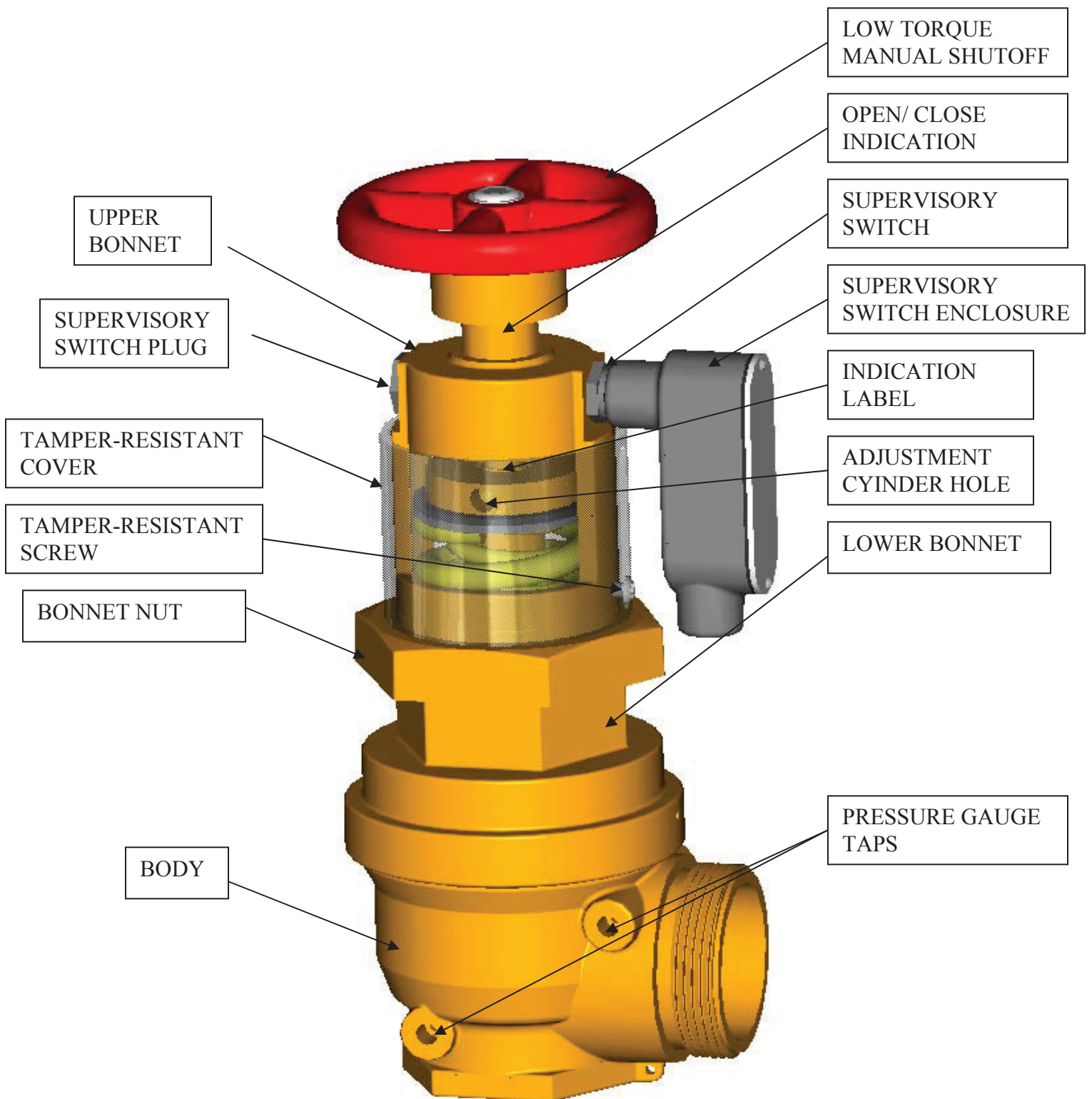
## **INSTALLATION AND OPERATING INSTRUCTIONS FOR FIELD ADJUSTABLE PRESSURE REDUCING/ CONTROLLING VALVES**



(URFA-20-2.5 MODEL SHOWN)



## URFA VALVE MAJOR COMPONENTS





## **SPECIFICATIONS**

- Pressure rated up to 400 psi.
- Flow rated up to 500 GPM
- Open-Close indication from 2 view directions
- Pressure reduction can be field adjusted
- Pressure reduction adjustment can be easily determined by indication label
- Pressure reduction adjustment has tamper resistant feature
- Low-torque manual close handwheel
- Built-in automatic check valve
- Regulates pressure under both flow and no-flow conditions
- Tapped for pressure gauge on both inlet and outlet side of valve
- Optional integral supervisory switch (For Indoor Use Only)

## **INLET – OUTLET CONNECTIONS**

VALVE MODEL	INLET THREAD	OUTLET THREAD
<del>URFA-20-2.5</del>	<del>2-1/2" FEMALE NPT</del>	<del>2-1/2" FEMALE NPT</del>
URFA-20S-2.5	2-1/2" FEMALE NPT	2-1/2" FEMALE NPT
URFA-25-2.5	2-1/2" FEMALE NPT	2-1/2" MALE HOSE

## **APPLICATION**

### **A. AUTOMATIC SPRINKLER SYSTEMS**

The models URFA-20S-2.5 and URFA-20-2.5 valves are most commonly used in automatic sprinkler systems as floor control valves in high-rise buildings where supply riser pressures exceed 175 psi. The URFA valves are Listed by Underwriters Laboratories as “Special System Water Control Valves – Pressure Reducing and Pressure Control Type (VLMT)”, and also meet the listing requirements for indicating valves. Installation requirements for pressure reducing valves in automatic sprinkler systems are given in Section 4-6.1.2 of NFPA 13, Standard for the installation of Sprinkler Systems, 1999 Edition. When designing URFA pressure reducing valves into a sprinkler system a maximum flow rate of 400 GPM should be observed.

URFA Pressure Reducing Valves are also listed as checking devices, which eliminates the need for a separate check valve. When sprinklers on a given floor are fed from dual risers, the URFA valve acts as a check valve to prevent loss of sprinkler water supply in the event of one riser sustaining damage.

Requirements for Alarm Attachments are given in Section 5-15.1.6 of NFPA 13, Standard for the installation of Sprinkler Systems, 1999 Edition. An integral, listed supervisory alarm switch is available on URFA pressure reducing valves as option number “01” when ordering.



## **B. STANDPIPE SYSTEM**

The models URFA-25-2.5 and URFA-20-2.5 valves are most commonly used in standpipe systems. The URFA-25-2.5 valves have a male hose thread outlet for connecting to fire suppression hose. When hose racks are used, the URFA-20-2.5 can be utilized along with a special hose nipple for support of the rack. The URFA valves are Listed by Underwriters Laboratories as Standpipe Equipment Pressure Reducing Devices (VUTX). Requirements for installation of pressure reducing valves in standpipe systems are given in Section 5-8 of NFPA-14, Standard for the Installation of Standpipe Hose Systems, 1993 Edition.

## **INSTALLATION REQUIREMENTS**

### **A. AUTOMATIC SPRINKLER SYSTEM**

1. To permit easy replacement or repair of valve, pipe unions or rubber gasket mechanical couplings should be installed immediately upstream or downstream of each URFA valve.
2. A relief valve of not less than ½ inch size is to be installed on the downstream side of each URFA valve
3. Pressure gauges are to be installed on the inlet and outlet side of each pressure-reducing valve
4. Valve adjustment setting should be selected to provide an outlet pressure not exceeding 165 psi at the maximum inlet pressure
5. Upon system completion, each Valve must be tested under both flow and no-flow conditions to verify that static residual outlet pressures and flow rates satisfy system design requirements. See Section 8-2.5 NFPA 13 for more information on mandatory flow and no-flow test requirements.

### **B. STANDPIPE SYSTEM**

1. The URFA-25-2.5 can be used for both Class I and Class III service.
2. NFPA 14 requires that hose valve outlet pressures for Class I and Class III service be no greater than 175 psi. and no less than 100 psi. When permitted by the authority having jurisdiction, pressures less than 100 psi may be allowed, but in no cases shall the valve discharge pressure be less than 65 psi
3. Upon system completion, each valve must be tested under both flow and no-flow conditions to verify that static and residual outlet pressures and flow rates satisfy system design requirements. See Section 8-5.5 of NFPA 14 for more information on required flow and no-flow testing.

## **CONSTRUCTION & OPERATING PRINCIPLE**

The URFA is a field adjustable pressure-reducing valve, which utilizes a hydraulic piston and cylinder assembly within the valve lower bonnet to allow the valve to self-throttle in response



to the pressure on the downstream side of the valve. Because the piston, main stem and valve seat float freely from the manual valve stem and handwheel assembly, the valve is able to self-close under static conditions and maintains a reduced pressure both under no-flow and flowing conditions. Valve discharge pressure is transmitted to the top side of the piston through pressure passages in the main stem. The presence of the piston results in a net area differential, which produces a hydraulic balancing force in the closed direction. The magnitude of this balancing force is in direct proportion to the hydraulic area of the piston.

The Field Adjustable feature of the valve is controlled by a spring within the valve upper bonnet. The spring adds an opening force to the main stem so that pressure reduction may be changed as the spring force is changed. This feature allows for the valve to satisfy all expected inlet/outlet pressure ratios. The Field Adjustable feature allows for one type of valve to be specified for all locations in a structure. Once installed the valves can be adjusted to the correct pressure reduction ratio based on their locations.

The URFA valves feature a patent pending manual close design that allows for extremely low torque of the handwheel while manually opening and closing the valve. The unique design allows for the independent operation of the valve stem from the manual close push-rod; this allows for the operator to bypass the large torque required to overcome the stiffness of the adjustment spring.

## **INSTALLATION OF VALVE**

- The valve should first be plumbed into the system
- The upper bonnet may be rotated for optimized access to adjustment window
  - Loosen Bonnet Nut
  - Rotate Upper Bonnet to desired location of adjustment window
  - Apply service removable thread lock to the Bonnet Nut threads
  - Tighten the Bonnet Nut firmly
- See wire diagram for proper installation of supervisory switch
- The system should be slowly filled with water and purged of air
- The system should then be flushed to remove any debris

## **VALVE SETTING SELECTION**

The URFA valves have settings of A, B, C, D, and E. Each valve setting corresponds to a pressure reduction graph located at the end of this manual. The valve setting is determined by where the top of the adjustment cylinder lines up on the Adjustment Identification Label located on the main stem (refer to Figure 1). To determine the correct setting for each URFA valve in the system design please use the following step.

1. Determine the standpipe or sprinkler riser residual pressure for each valve location. This is the inlet pressure at each valve under design flow conditions. In order to accurately determine these pressures, complete water supply data will be required, including results of municipal supply, flow test, and the pump performance curve. The URFA inlet pressure will be equal to the sum of the pump discharge pressure and the



municipal supply pressure at the design flow rate, less piping friction loss and elevation loss.

2. Turn to the appropriate valve performance chart. The valve model and flow range for each graph is indicated in the title at the top of the graph. Be sure to use the correct graph for the designed flow rate through the valve.
3. Locate the valve inlet residual pressure on the vertical axis of the chart and draw a line from the pressure horizontally across the chart.
4. Locate the desired valve outlet residual pressure on the chart horizontal axis and draw a vertical line from this pressure across the chart
5. From the intersection of the inlet and outlet pressure lines constructed in (3) and (4) above, move horizontally to the nearest valve performance curve (actually straight diagonal lines). This will be the appropriate valve setting for the chosen location.
6. Determine the valve static inlet pressure. This will be the sum of the municipal supply static pressure plus the pump churn pressure, less the elevation loss.
7. To determine the valve static outlet pressure, refer to the appropriate static chart. Locate the valve static inlet pressure on the vertical axis of the chart. Follow across to the appropriate valve curve and drop down to the horizontal axis to read valve outlet static pressure.
8. If static outlet pressure is found to exceed the maximum outlet pressure allowed by NFPA 13 or NPFA 14, it will be necessary to re-select a valve setting to the left of the originally chosen type.

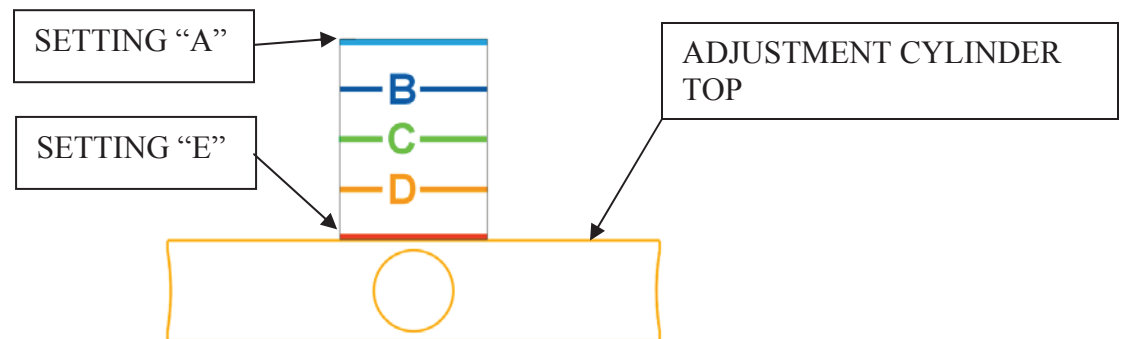


Figure - 1

## **SETTING PRESSURE REDUCTION**

1. Remove the tamper-resistant screw from the clear cover by means of tamper-resistant Allen wrench provided with valve.
2. Insert adjustment tool provided with valve through the slot in the clear cover into the hole in the adjustment cylinder.
3. Rotate adjustment cylinder until the top of the adjustment cylinder is aligned with desired mark on the Indication Label (refer to Figure 1).
4. Once rotation limit is reached during adjustment remove the adjustment tool from the adjustment cylinder hole and re-insert the adjustment tool into the next available hole.



5. Once the proper adjustment is obtained verify the outlet pressure is correct with pressure gauges both upstream and downstream of the valve during both flow and no-flow pressure testing; make adjustments as needed. See Section 8-2.5 of NFPA 13 for more details on required flow and no-flow testing.
6. Once the valve is properly adjusted replace the tamper-resistant screw that was removed in step 2.
7. A tamper-resistant allen wrench and adjustment tool should be stored in a special location for Fire Department use.

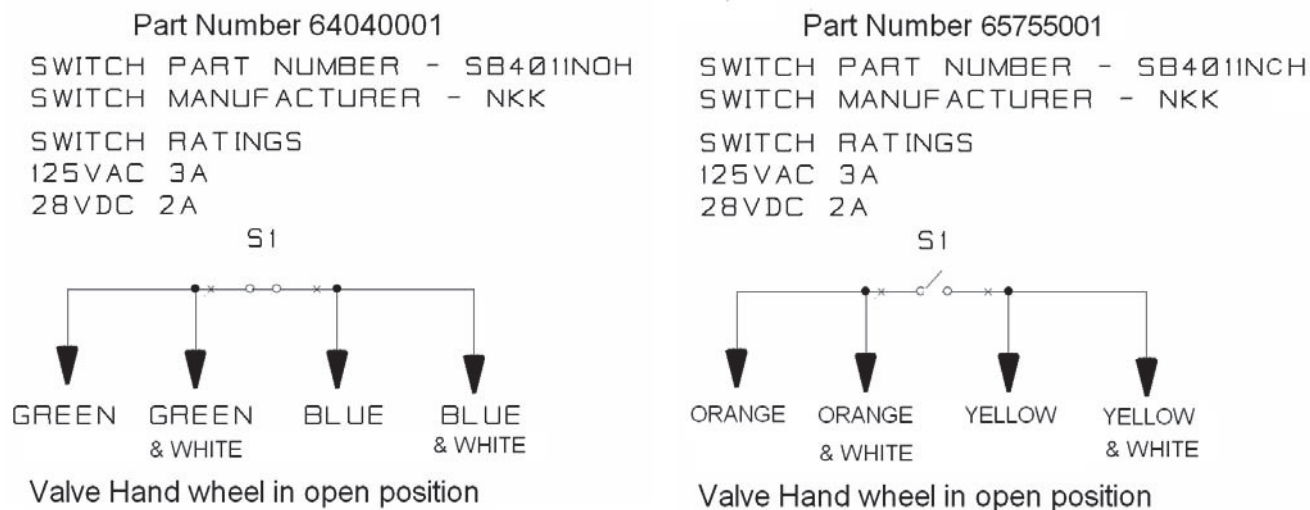
NOTE: Rotating the adjustment cylinder clockwise will increase outlet pressure. Conversely, rotating the adjustment cylinder counter-clockwise will decrease outlet pressure.



## SUPERVISORY SWITCH

Pressure reducing/ controlling valves that are to be used as part of a sprinkler system should include a supervisory switch to signal when a valve is not manually in the fully opened position (refer to NFPA 13 for more details on supervisory requirements). An optional supervisory switch assembly with UL approval for use with URFA valves is available on all models. The supervisory switch may be mounted to either side of the upper bonnet in the  $\frac{3}{4}$  inch tapped holes provided. A cap plug is secured in the upper bonnet tapped holes when the supervisory switch is not installed. A UL Listed conduit elbow is utilized as a water-resistant enclosure for the electronic switch. The conduit elbow provides an opening for fastening conduit to the enclosure, and a lid may be removed to gain access for wiring connections. The lid is attached with two pin-in-hex security screws. A key is provided for installation access into the conduit enclosure. Two switch options are available for the supervisory switch assembly. The first, part number 64040001, will provide a closed circuit when the valve hand wheel is in the full open position. The second option, part number 65755001, will provide an open circuit when the valve hand wheel is in the full open position. Please specify the required switch configuration when ordering. Figure 2 describes wiring details. The two switch options have different colored leads for easy identification. Part number 64040001, the closed circuit switch, has blue and green wire leads. Part number 65755001, the open circuit switch, has yellow and orange wire leads. The solid colored wires act as a primary wiring configuration and the striped wires act as a secondary or back up wiring configuration.

Figure - 2





Note: Supervisory switch rated for Indoor Use Only.

The supervisory switch enclosure may be positioned with the conduit enclosure at various angles so to better meet space requirements (see Figure 3). To reposition the conduit enclosure angle, hold rotation on the hex adaptor fastened to the upper bonnet with the use of an open box wrench. While insuring the hex adaptor remains fully threaded against the upper bonnet, position the conduit enclosure to the desired angle. When completed the hex adaptor **MUST** be fully threaded against the upper bonnet to insure proper function. If the hex adaptor becomes unthreaded the supervisory switch will send an opened signal. Also ensure that the manual handwheel may be fully closed without interference from the supervisory switch assembly.

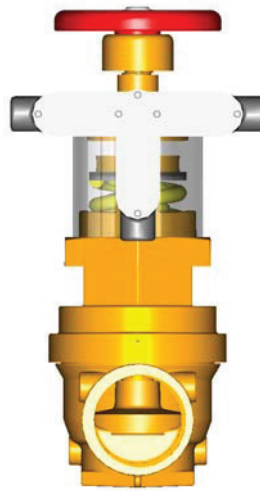


Figure - 3

## **VALVE CARE & MAINTENANCE**

URFA valves require minimal maintenance. However, a routine inspection and test program is essential for any fire protection system to insure that it is in proper operating condition. NFPA 25, standard for the Inspection, Testing and Maintenance of Water-Based Fire Protection Systems should be consulted for a determination of required test frequency and methods.

Below is a summary of the required frequency of inspections and testing for pressure reducing valves:

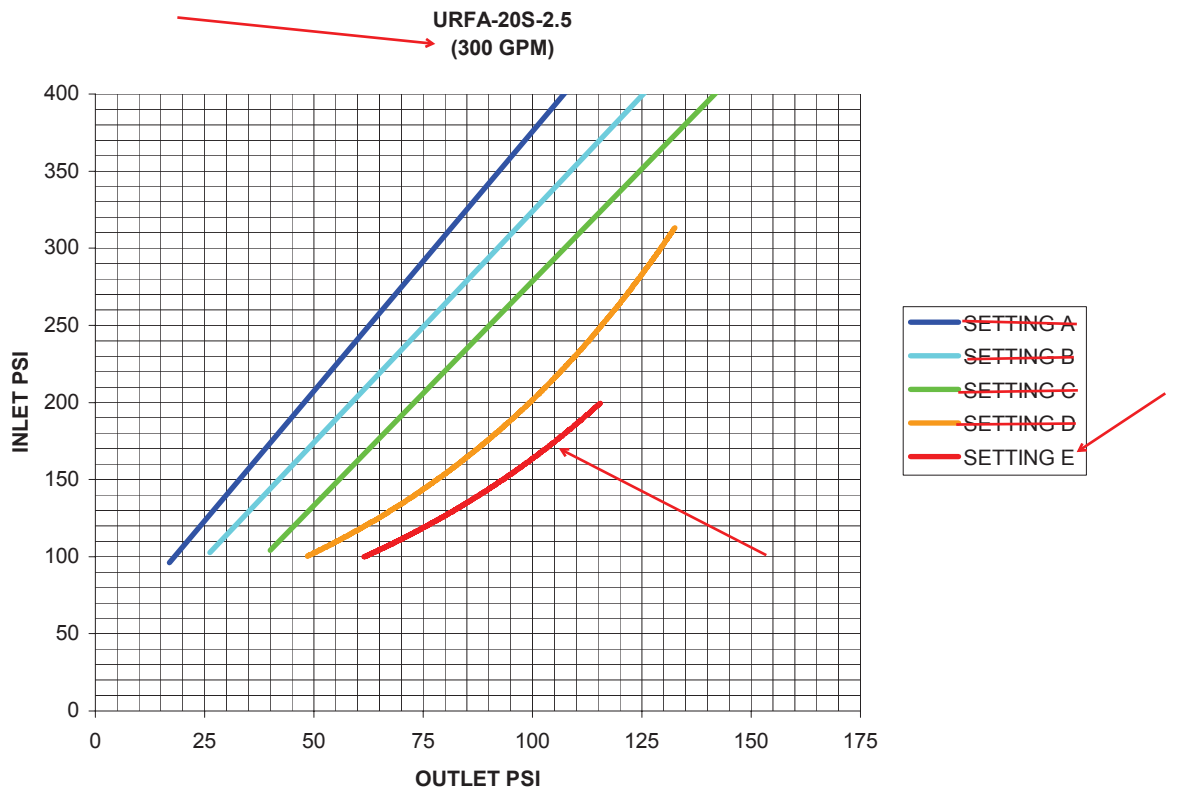
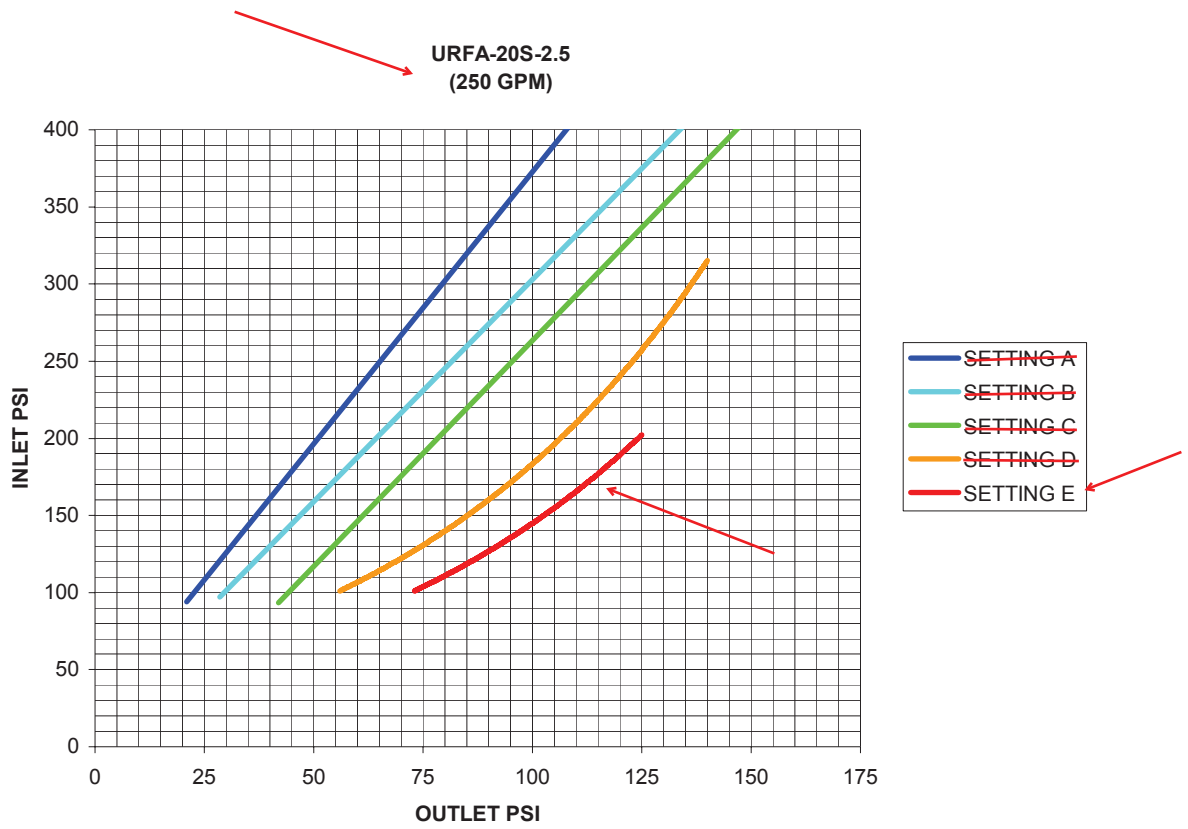
Valve Application	Inspection	Flow Test
Sprinkler System Pressure Regulating Control Valve	Quarterly	Annually
Hose Connection and Hose Rack Assembly Pressure Regulating Valve	Quarterly	5-Years



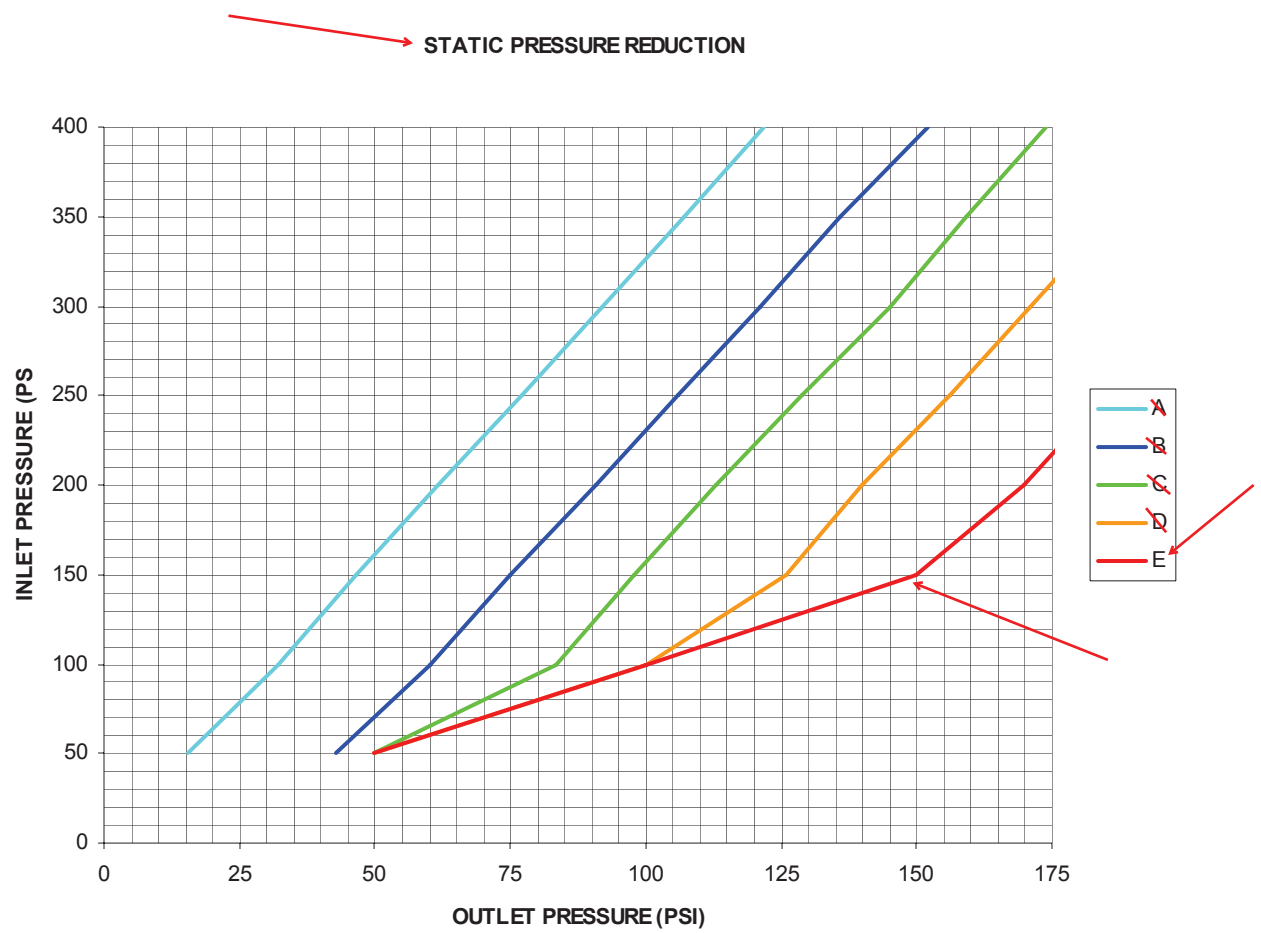
Quarterly inspections should verify that the tamper-resistant cover is properly secured and compare actual valve adjustment settings to documented correct adjustment settings for each valve. If a valve is found to have incorrect valve setting it should be reset to the proper setting and undergo flow and no-flow testing to verify proper pressure reduction is obtained.

Flow test results should be compared to previous test results, and to system performance criteria. If the valve adjustment settings match the original and correct settings for each valve then no significant variance should occur from the original flow testing data.











# Elkhart Brass

## Fire Fighting Equipment

### URFA Valve Calculator

Project Name Cal Poly Center for Science

Floor Location First Floor

Static Inlet Pressure (PSI) \* 183

Residual Inlet Pressure (PSI) \* 174.5

Design Static Outlet Pressure

Design Residual Outlet Pressure

Flow Rate (GPM) \* 250

Valve Body Style URFA-20S-2.5 (IN-LINE BODY)

Indicator Setting	Static Outlet Pressure (PSI)	Residual Outlet Pressure (PSI)
A	56.40	43.77
B	85.56	55.34
C	107.90	69.71
D	135.24	96.64
E	163.20	113.60

PRESSURE LOSS ACROSS VALVE IS

$$174.5 \text{ PSI} - 113.6 \text{ PSI} = 60.9 \text{ PSI}$$

@ 250 GPM



**Elkhart Brass**

Fire Fighting Equipment

**URFA Valve Calculator**

Project Name Cal Poly Center for Science  
Floor Location First Floor [R/A=2]  
Static Inlet Pressure (PSI) \* 183  
Residual Inlet Pressure (PSI) \* 169  
Design Static Outlet Pressure  
Design Residual Outlet Pressure  
Flow Rate (GPM) \* 328  
Valve Body Style URFA-20S-2.5 (IN-LINE BODY)

Indicator Setting	Static Outlet Pressure (PSI)	Residual Outlet Pressure (PSI)
<del>A</del>	<del>56.40</del>	<del>36.38</del>
<del>B</del>	<del>85.56</del>	<del>45.66</del>
<del>C</del>	<del>107.90</del>	<del>54.23</del>
<del>D</del>	<del>135.24</del>	<del>83.89</del>
E	163.20	98.86

PRESSURE LOSS ACROSS VALVE IS

$$169 \text{ PSI} - 98.86 \text{ PSI} = 70.14 \text{ PSI}$$

@ 328 GPM





**AUTOMATIC  
SPRINKLER CO.**

21605 North Central Ave. 623.580.7800  
Phoenix, Arizona 85024 Fax 623.434.3154

AZ-L16-234798 CA-C16-901529  
AZ-C16-234797 NV-C41-69370  
UT-S370-6690455-5501 NM-MS 12-354807



Fire Protection by Computer Design

Aero Automatic Sprinkler Co.  
21605 N. Central Ave.  
Phoenix, Arizona 85024  
623-580-7800

Job Name : Cal Poly Center for Science LVL 1 [R/A=2]  
Building : FP-6.01W  
Location : San Luis Obispo, Ca.  
System : 1-2  
Contract : 10034  
Data File : Cal Poly CFS LVL 1-2.WXF



---

**HYDRAULIC CALCULATIONS**  
**for**

**Project name:** Cal Poly Center For Science  
**Location:** San Luis Obispo, Ca.  
**Drawing no:** FP-6.01W  
**Date:** 9-25-2011

**Design**

**Remote area number:** 1-2  
**Remote area location:** 1 st. Floor Lecture  
**Occupancy classification:** Light Hazard  
**Density:** 0.10 - Gpm/SqFt  
**Area of application:** 1500 - SqFt  
**Coverage per sprinkler:** 163 - SqFt  
**Type of sprinklers calculated:** Tyco; Mod. TY-FRB; 1/2"; 1/2";K=5.6; 155 Deg  
**No. of sprinklers calculated:** 16  
**In-rack demand:** N/A - GPM  
**Hose streams:** 100 - GPM  
**Total water required (including hose streams):** 428.4 - GPM @ 45.59 - Psi  
**Type of system:** WET  
**Volume of dry or preaction system:** N/A - Gal

**Water supply information**

**Date:** 8-19-2011  
**Location:** N. Poly View Drive  
**Source:** Fluid Resource Management

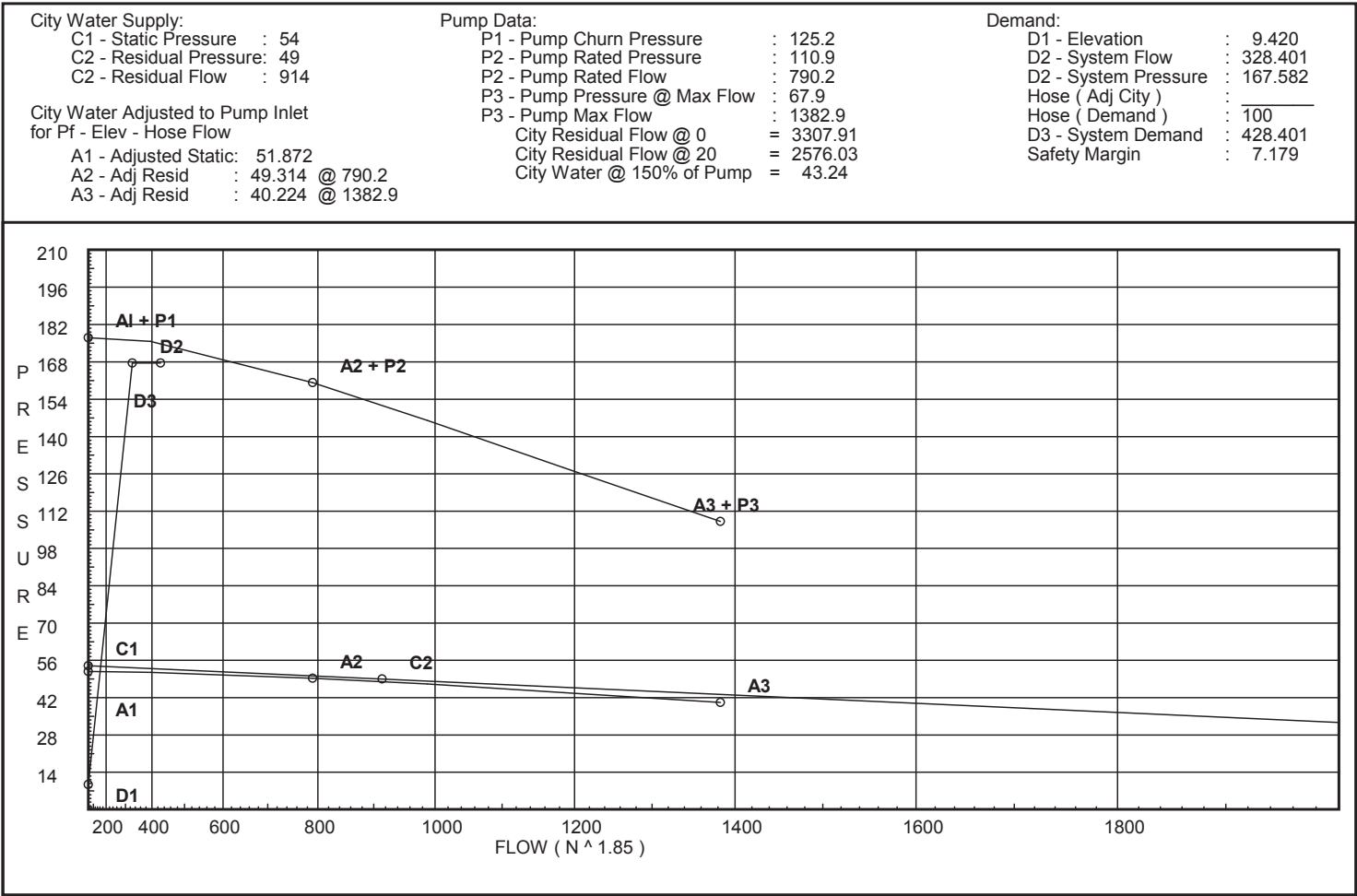
**Name of contractor:** Aero Automatic Sprinkler Co.  
**Address:** 21605 N. Central Ave. Phoenix, Az. 85024  
**Phone number:** 623-580-7847  
**Name of designer:** Neal Larsen  
**Authority having jurisdiction:** C.S.F.M.

**Notes: (Include peaking information or gridded systems here.)** Flow Test Information :  
Hydrant # 63; Static = 60 psi; Res.= 55 psi {Elev.=351.0'}  
Hydrant # 64; Flow = 914 gpm  
FLOW TEST USED IN HYD. CALCS REDUCED BY 10 % [STATIC=54psi; RES.=49psi]



Water Supply Curve (C)

Aero Automatic Sprinkler Co.  
Cal Poly Center for Science LVL 1 [R/A=2]





Fittings Used Summary

Aero Automatic Sprinkler Co.  
Cal Poly Center for Science LVL 1 [R/A=2]

Fitting Legend																					
Abbrev.	Name	½	¾	1	1¼	1½	2	2½	3	3½	4	5	6	8	10	12	14	16	18	20	24
B	Generic Butterfly Valve	0	0	2.25	2	2.5	6	7	10	0	12	9	10	12	19	21	0	0	0	0	0
C	Generic Check Vlv	4	5	5	7	9	11	14	16	19	22	27	32	45	55	65	76	87	98	109	130
E	90° Standard Elbow	2	2	2	3	4	5	6	7	8	10	12	14	18	22	27	35	40	45	50	61
G	Generic Gate Valve	0	0	0	1	0	1	1	1	1	2	2	3	4	5	6	7	8	10	11	13
H	45° Ell Grvd-Vic #11	0	0	1	1.5	2	2	3	3	3.5	3.5	4.5	5	6.5	8.5	10	18	20	23	25	30
I	90° Ell Grvd-Vic #10	0	0	2	3	4	3.5	6	5	8	7	8.5	10	13	17	20	23	25	33	36	40
T	90° Flow Thru Tee	3	4	5	6	8	10	12	15	17	20	25	30	35	50	60	71	81	91	101	121
Zic	Wilkins 350ADA	Fitting generates a Fixed Loss Based on Flow																			

Units Summary

Diameter Units	Inches
Length Units	Feet
Flow Units	US Gallons per Minute
Pressure Units	Pounds per Square Inch



# Pressure / Flow Summary - STANDARD

Aero Automatic Sprinkler Co.  
Cal Poly Center for Science LVL 1 [R/A=2]

Page 4  
Date 9-25-11

Node No.	Elevation	K-Fact	Pt Actual	Pn	Flow Actual	Density	Area	Press Req.
S121	34.75	5.6	7.0	na	14.82	0.1	117	7.0
S122	34.75	5.6	7.93	na	15.77	0.1	124	7.0
S123	34.75	5.6	11.11	na	18.67	0.1	124	7.0
S124	34.75	5.6	12.56	na	19.84	0.1	124	7.0
S125	28.833	5.6	10.5	na	18.15	0.1	143	7.0
S126	28.833	5.6	11.19	na	18.73	0.1	143	7.0
S127	28.833	5.6	14.14	na	21.06	0.1	143	7.0
S128	25.833	5.6	11.6	na	19.07	0.1	143	7.0
S129	25.833	5.6	12.13	na	19.5	0.1	143	7.0
S130	25.833	5.6	15.36	na	21.95	0.1	143	7.0
S131	22.833	5.6	13.67	na	20.71	0.1	143	7.0
S132	22.833	5.6	14.36	na	21.22	0.1	163	7.0
S133	22.833	5.6	18.06	na	23.8	0.1	163	7.0
S134	19.833	5.6	17.51	na	23.43	0.1	143	7.0
S135	19.833	5.6	19.32	na	24.61	0.1	114	7.0
S136	19.833	5.6	23.35	na	27.06	0.1	114	7.0
L121	36.917		6.37	na				
L122	36.917		7.59	na				
L123	36.917		11.0	na				
L124	36.917		12.54	na				
L125	36.0		8.4	na				
L126	36.0		10.01	na				
L127	36.0		13.44	na				
L128	34.5		9.12	na				
L129	34.5		10.59	na				
L130	34.5		14.36	na				
L131	33.0		11.38	na				
L132	33.0		12.71	na				
L133	33.0		17.08	na				
L134	31.5		16.04	na				
L135	31.5		17.74	na				
L136	31.5		22.43	na				
M121	36.917		14.67	na				
M122	36.0		15.16	na				
M123	34.5		16.22	na				
M124	33.0		19.23	na				
M125	31.5		24.65	na				
M105	13.167		71.73	na				
TR01	13.167		86.12	na				
BR01	3.0		162.22	na				
SPC1	12.667		162.45	na	100.0			
SPC2	12.667		162.73	na				
PO	1.833		167.58	na				
PI	1.75		51.42	na				
POC	6.75		49.38	na				
BF1	13.0		46.8	na				
BF2	13.0		52.57	na				
SRC	13.0		52.77	na				

The maximum velocity is 19.32 and it occurs in the pipe between nodes M125 and M105



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Aero Automatic Sprinkler Co.  
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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqv.	Ln.	Pipe Ftng's Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
*FLOWING SPRINKLER R/A # 2												
S121 to L121	34.750 36.917	5.60	14.82 14.82	1 1.049	1E 0.0	2.0 0.0	2.167 2.000	120 0.0749	7.000 -0.939			
			0.0			0.0	4.167		0.312	Vel =	5.50	
L121			14.82						6.373	K Factor =	5.87	
S122 to L122	34.750 36.917	5.60	15.77 15.77	1 1.049	1T 0.0	5.0 0.0	2.167 5.000	120 0.0840	7.930 -0.939			
			0.0			0.0	7.167		0.602	Vel =	5.85	
L122			15.77						7.593	K Factor =	5.72	
S123 to L123	34.750 36.917	5.60	18.67 18.67	1 1.049	1T 0.0	5.0 0.0	2.167 5.000	120 0.1147	11.113 -0.939			
			0.0			0.0	7.167		0.822	Vel =	6.93	
L123			18.67						10.996	K Factor =	5.63	
S124 to L124	34.750 36.917	5.60	19.84 19.84	1 1.049	1T 0.0	5.0 0.0	2.167 5.000	120 0.1284	12.555 -0.939			
			0.0			0.0	7.167		0.920	Vel =	7.37	
L124			19.84						12.536	K Factor =	5.60	
S125 to L125	28.833 36	5.60	18.15 18.15	1 1.049	1E 0.0	2.0 0.0	7.167 2.000	120 0.1088	10.504 -3.104			
			0.0			0.0	9.167		0.997	Vel =	6.74	
L125			18.15						8.397	K Factor =	6.26	
S126 to L126	28.833 36	5.60	18.73 18.73	1 1.049	1E 1T	2.0 5.0	9.667 7.000	120 0.1153	11.192 -3.104			
			0.0			0.0	16.667		1.921	Vel =	6.95	
L126			18.73						10.009	K Factor =	5.92	
S127 to L127	28.833 36	5.60	21.06 21.06	1 1.049	1E 1T	2.0 5.0	9.750 7.000	120 0.1432	14.144 -3.104			
			0.0			0.0	16.750		2.399	Vel =	7.82	
L127			21.06						13.439	K Factor =	5.74	
S128 to L128	25.833 34.500	5.60	19.07 19.07	1 1.049	1E 0.0	2.0 0.0	8.667 2.000	120 0.1192	11.601 -3.754			
			0.0			0.0	10.667		1.271	Vel =	7.08	
L128			19.07						9.118	K Factor =	6.32	
S129 to L129	25.833 34.500	5.60	19.50 19.5	1 1.049	1E 1T	2.0 5.0	10.833 7.000	120 0.1242	12.127 -3.754			
			0.0			0.0	17.833		2.215	Vel =	7.24	
L129			19.50						10.588	K Factor =	5.99	
S130 to L130	25.833 34.500	5.60	21.95 21.95	1 1.049	1E 1T	2.0 5.0	10.833 7.000	120 0.1546	15.361 -3.754			
			0.0			0.0	17.833		2.757	Vel =	8.15	



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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqv.	Ln.	Pipe Ftng's Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
L130			0.0 21.95						14.364		K Factor = 5.79	
S131 to L131	22.833 33	5.60	20.71	1	1T	5.0 0.0	10.167 5.000	120	13.674 -4.403			
			20.71	1.049		0.0	15.167	0.1388	2.105		Vel = 7.69	
L131			0.0 20.71						11.376		K Factor = 6.14	
S132 to L132	22.833 33	5.60	21.22	1	1E 1T	2.0 5.0	11.917 7.000	120	14.362 -4.403			
			21.22	1.049		0.0	18.917	0.1452	2.747		Vel = 7.88	
L132			0.0 21.22						12.706		K Factor = 5.95	
S133 to L133	22.833 33	5.60	23.80	1	1E 1T	2.0 5.0	12.083 7.000	120	18.057 -4.403			
			23.8	1.049		0.0	19.083	0.1794	3.424		Vel = 8.84	
L133			0.0 23.80						17.078		K Factor = 5.76	
S134 to L134	19.833 31.500	5.60	23.44	1	1E 1T	2.0 5.0	13.500 7.000	120	17.512 -5.053			
			23.44	1.049		0.0	20.500	0.1745	3.577		Vel = 8.70	
L134			0.0 23.44						16.036		K Factor = 5.85	
S135 to L135	19.833 31.500	5.60	24.61	1	1T	5.0 0.0	13.167 5.000	120	19.319 -5.053			
			24.61	1.049		0.0	18.167	0.1911	3.471		Vel = 9.14	
L135			0.0 24.61						17.737		K Factor = 5.84	
S136 to L136	19.833 31.500	5.60	27.06	1	1T	5.0 0.0	13.167 5.000	120	23.350 -5.053			
			27.06	1.049		0.0	18.167	0.2276	4.135		Vel = 10.05	
L136			0.0 27.06						22.432		K Factor = 5.71	
*BRANCH LINES R/A # 2												
L121 to L122	36.917		14.82	1	1E	2.0 0.0	14.333 2.000	120	6.373 0.0			
			14.82	1.049		0.0	16.333	0.0747	1.220		Vel = 5.50	
L122 to L123	36.917		15.77	1		0.0 0.0	11.917 0.0	120	7.593 0.0			
			30.59	1.049		0.0	11.917	0.2856	3.403		Vel = 11.36	
L123 to M121	36.917		18.67	1	1T	5.0 0.0	0.333 5.000	120	10.996 0.0			
			49.26	1.049		0.0	5.333	0.6895	3.677		Vel = 18.29	
M121			0.0 49.26						14.673		K Factor = 12.86	
L124 to M121	36.917		19.84	1	1T	5.0 0.0	11.667 5.000	120	12.536 0.0			
			19.84	1.049		0.0	16.667	0.1282	2.137		Vel = 7.37	



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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqv. Ln.	Pipe Ftng's Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
M121			0.0 19.84					14.673		K Factor = 5.18	
L125 to L126	36 36		18.15 18.15	1 1.049	0.0 0.0	14.833 0.0	120 0.1087	8.397 0.0			
L126 to M122	36 36		18.73 36.88	1 1.049	1T 0.0	7.750 5.000	120 0.4038	10.009 0.0		Vel = 6.74	
M122			0.0 36.88					15.157		K Factor = 9.47	
L127 to M122	36 36		21.06 21.06	1 1.049	1T 0.0	7.000 5.000	120 0.1432	13.439 0.0		Vel = 7.82	
M122			0.0 21.06					15.157		K Factor = 5.41	
L128 to L129	34.500 34.500		19.07 19.07	1 1.049	0.0 0.0	12.333 0.0	120 0.1192	9.118 0.0			
L129 to M123	34.500 34.500		19.51 38.58	1 1.049	1T 0.0	7.833 5.000	120 0.4387	10.588 0.0		Vel = 7.08	
M123			0.0 38.58					16.218		K Factor = 9.58	
L130 to M123	34.500 34.500		21.95 21.95	1 1.049	1T 0.0	7.000 5.000	120 0.1545	14.364 0.0		Vel = 8.15	
M123			0.0 21.95					16.218		K Factor = 5.45	
L131 to L132	33 33		20.71 20.71	1 1.049	0.0 0.0	9.583 0.0	120 0.1388	11.376 0.0			
L132 to M124	33 33		21.22 41.93	1 1.049	1T 0.0	7.750 5.000	120 0.5118	12.706 0.0		Vel = 7.69	
M124			0.0 41.93					19.232		K Factor = 9.56	
L133 to M124	33 33		23.80 23.8	1 1.049	1T 0.0	7.000 5.000	120 0.1795	17.078 0.0		Vel = 8.84	
M124			0.0 23.80					19.232		K Factor = 5.43	
L134 to L135	31.500 31.500		23.44 23.44	1 1.049	0.0 0.0	9.750 0.0	120 0.1745	16.036 0.0			
L135 to M125	31.500 31.500		24.61 48.05	1 1.049	1T 0.0	5.500 5.000	120 0.6586	17.737 0.0		Vel = 8.70	
M125						10.500		6.915		Vel = 17.84	



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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqv.	Ln.	Pipe Ftng's Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
M125			0.0 48.05						24.652		K Factor = 9.68	
L136 to M125	31.500 31.500		27.06	1	1T	5.0 0.0	4.750 5.000	120	22.432 0.0			
			27.06	1.049		0.0	9.750	0.2277	2.220		Vel = 10.05	
M125			0.0 27.06						24.652		K Factor = 5.45	
*FEED MAIN												
M121 to M122	36.917 36		69.10	2.5		0.0 0.0	6.000 0.0	120	14.673 0.397			
			69.1	2.635		0.0	6.000	0.0145	0.087		Vel = 4.07	
M122 to M123	36 34.500		57.94	2.5		0.0 0.0	9.167 0.0	120	15.157 0.650			
			127.04	2.635		0.0	9.167	0.0448	0.411		Vel = 7.47	
M123 to M124	34.500 33		60.52	2.5	1T	16.474 0.0	9.167 16.474	120	16.218 0.650			
			187.56	2.635		0.0	25.641	0.0922	2.364		Vel = 11.03	
M124 to M125	33 31.500		65.73	2.5	1H 1T	4.119 16.474	9.083 20.593	120	19.232 0.650			
			253.29	2.635		0.0	29.676	0.1607	4.770		Vel = 14.90	
M125 to M105	31.500 13.167		75.11	2.5	2T 3I	32.948 24.711	92.917 57.659	120	24.652 7.940			
			328.4	2.635		0.0	150.576	0.2599	39.134		Vel = 19.32	
M105 to TR01	13.167 13.167		0.0	3	4I 1T	26.879 20.159	109.083 47.038	120	71.726 0.0			
			328.4	3.26		0.0	156.121	0.0922	14.391		Vel = 12.62	
TR01 to BR01	13.167 3		0.0	3	1I	6.72 0.0	10.167 6.720	120	86.117 74.543		* Fixed loss = 70.14	
			328.4	3.26		0.0	16.887	0.0922	1.557		Vel = 12.62	
BR01 to SPC1	3 12.667		0.0	3	2I 1T	13.44 20.159	14.333 33.599	120	162.217 -4.187			
			328.4	3.26		0.0	47.932	0.0922	4.419		Vel = 12.62	
SPC1 to SPC2	12.667 12.667	H100	100.00	6	1T	30.0 0.0	7.917 30.000	120	162.449 0.0			
			428.4	6.065		0.0	37.917	0.0073	0.278		Vel = 4.76	
SPC2 to PO	12.667 1.833		0.0	8	1I 1B 1C	13.0 12.0 45.0	14.750 70.000 84.750	120	162.727 4.692			
			428.4	7.981				0.0019	0.163		Vel = 2.75	
PO			0.0 428.40						167.582		K Factor = 33.09	
System Demand Pressure						167.582						
Safety Margin						7.179						
Continuation Pressure						174.761						
Pressure @ Pump Outlet						174.761						
Pressure From Pump Curve						-123.339						
Pressure @ Pump Inlet						51.422						
PI to POC	1.750 6.750		0.0	8	1G 1I 1T	4.0 13.0 35.0	14.000 52.000 66.000	120	51.422 -2.166			
			428.4	7.981				0.0019	0.127		Vel = 2.75	



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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqv. Ln.	Pipe Ftng's Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
POC to BF1	6.750 13		0.0 428.4	8 8.27	2E 56.936 0.0	41.000 56.936 97.936	140 0.0012	49.383 -2.707 0.120		Vel = 2.56	
BF1 to BF2	13 13		0.0 428.4	8 7.981	1Zic 0.0 0.0	4.000 0.0 4.000	120 0.0018	46.796 5.766 0.007	* Fixed loss = 5.766	Vel = 2.75	
BF2 to SRC	13 13		0.0 428.4	8 8.27	2E 1G 1T	56.936 6.326 55.354	46.000 118.616 164.616	140 0.0 0.200	52.569 0.0	Vel = 2.56	
SRC			0.0 428.40					52.769	K Factor = 58.97		





## FIRE ALARM AND EMERGENCY COMMUNICATION SYSTEM RECORD OF COMPLETION

To be completed by the system installation contractor at the time of system acceptance and approval.

It shall be permitted to modify this form as needed to provide a more complete and/or clear record.  
Insert N/A in all unused lines.

Attach additional sheets, data, or calculations as necessary to provide a complete record.

### 1. PROPERTY INFORMATION

Name of property: Cal Poly Center For Math And Science 180

Address: 01 Grand AVE, SAN LUIS OBISPO, CA 93407

Description of property: CLASSROOM LABS, LECTURE HALLS, FACULTY OFFICES

Occupancy type: A, B, H3

Name of property representative: GILBANECCO - CONTRACTOR, CAL POLY FACILITIES + CAPITOL PROJECTS

Address: 1 GRAND AVE, BLDG 70 - SAN LUIS OBISPO, CA 93407

Phone: 805-441-2186

Fax:

E-mail: PJUDD@CALPOLY.EDU

Authority having jurisdiction over this property: OSFM

1234 E. SHAW AVE FRESNO, CA 93710

Phone: 916-825-7880

Fax:

E-mail: POLY.PARENTI@FIRE.CA.GOV

### 2. INSTALLATION, SERVICE, AND TESTING CONTRACTOR INFORMATION

Installation contractor for this equipment: Deep Blue Integration Inc.

Address: 3442 Empresa Dr., Suite C, San Luis Obispo, California, 93401

License or certification number: B, C-10, C-16 #943465

Phone: 1-888-600-0324

Fax: 805-791-2037

E-mail: info@deepblueintegration.com

Service organization for this equipment: Deep Blue Integration Inc.

Address: 3442 Empresa Dr., Suite C, San Luis Obispo, California, 93401

License or certification number: B, C-10, C-16 #943465

Phone: 888-600-0324

Fax: 805-791-2037

E-mail: info@deepblueintegration.com

A contract for test and inspection in accordance with NFPA standards is in effect as of:

Contracted testing company: N/A

Address:

Phone:

Fax:

E-mail:

Contract expires:

Contract number:

Frequency of routine inspections:

### 3. DESCRIPTION OF SYSTEM OR SERVICE

☐ Fire alarm system (nonvoice)

☒ Fire alarm with in-building fire emergency voice alarm communication system (EVACS)

☐ Mass notification system (MNS)

☐ Combination system, with the following components:

☐ Fire alarm

☐ EVACS

☐ MNS

☐ Two-way, in-building, emergency communication system

☐ Other (specify):

NFPA 72, Fig. 10.18.2.1.1 (p. 1 of 12)



### 3. DESCRIPTION OF SYSTEM OR SERVICE *(continued)*

NFPA 72 edition:

Additional description of system(s):

#### 3.1 Control Unit

Manufacturer: *Honeywell Notifier*

Model number: *NFS2-640*

#### 3.2 Mass Notification System

☐ This system does not incorporate an MNS

##### 3.2.1 System Type:

☒ In-building MNS—combination

☐ In-building MNS—stand-alone

☐ Wide-area MNS

☐ Distributed recipient MNS

☐ Other (specify):

##### 3.2.2 System Features:

☒ Combination fire alarm/MNS

☐ MNS autonomous control unit

☐ Wide-area MNS to regional national alerting interface

☐ Local operating console (LOC)

☐ Direct recipient MNS (DRMNS)

☐ Wide-area MNS to DRMNS interface

☐ Wide-area MNS to high-power speaker array (HPSA) interface

☐ In-building MNS to wide-area MNS interface

☐ Other (specify):

#### 3.3 System Documentation

☒ An owner's manual, a copy of the manufacturer's instructions, a written sequence of operation, and a copy of the numbered record drawings are stored on site. Location: *At Alarm Panel*

#### 3.4 System Software

☒ This system does not have alterable site-specific software.

Operating system (executive) software revision level:

Site-specific software revision date: *2-2013*

Revision completed by: *Honeywell*

☐ A copy of the site-specific software is stored on site. Location:

#### 3.5 Off-Premises Signal Transmission

☐ This system does not have off-premises transmission.

Name of organization receiving alarm signals with phone numbers:

Alarm: *Cal Poly Dispatch Center*

Phone: *805-756-2281*

Supervisory: *Cal Poly Dispatch Center*

Phone: *805-756-2281*

Trouble: *Cal Poly Dispatch Center*

Phone: *805-756-2281*

Entity to which alarms are retransmitted:

*Direct*

Phone:

Method of retransmission: ~~2-way~~

If Chapter 26, specify the means of transmission from the protected premises to the supervising station:

If Chapter 27, specify the type of auxiliary alarm system: ☐ Local energy ☐ Shunt ☐ Wired ☐ Wireless



#### 4. CIRCUITS AND PATHWAYS

##### 4.1 Signaling Line Pathways

###### 4.1.1 Pathways Class Designations and Survivability

Pathways class: B Survivability level: 1 Quantity: 2  
(See NFPA 72, Sections 12.3 and 12.4)

###### 4.1.2 Pathways Utilizing Two or More Media

Quantity: Description:

###### 4.1.3 Device Power Pathways

- ☒ No separate power pathways from the signaling line pathway
- ☐ Power pathways are separate but of the same pathway classification as the signaling line pathway
- ☐ Power pathways are separate and different classification from the signaling line pathway

###### 4.1.4 Isolation Modules

Quantity:

##### 4.2 Alarm Initiating Device Pathways

###### 4.2.1 Pathways Class Designations and Survivability

Pathways class: Survivability level: Quantity:  
(See NFPA 72, Sections 12.3 and 12.4)

###### 4.2.2 Pathways Utilizing Two or More Media

Quantity: Description:

###### 4.2.3 Device Power Pathways

- ☒ No separate power pathways from the initiating device pathway
- ☐ Power pathways are separate but of the same pathway classification as the initiating device pathway
- ☐ Power pathways are separate and different classification from the initiating device pathway

##### 4.3 Non-Voice Audible System Pathways

###### 4.3.1 Pathways Class Designations and Survivability

Pathways class: B Survivability level: 1 Quantity: 22  
(See NFPA 72, Sections 12.3 and 12.4)

###### 4.3.2 Pathways Utilizing Two or More Media

Quantity: Description:

###### 4.3.3 Device Power Pathways

- ☒ No separate power pathways from the notification appliance pathway
- ☐ Power pathways are separate but of the same pathway classification as the notification appliance pathway
- ☐ Power pathways are separate and different classification from the notification appliance pathway



## 5. ALARM INITIATING DEVICES

### 5.1 Manual Initiating Devices

#### 5.1.1 Manual Fire Alarm Boxes

☐ This system does not have manual fire alarm boxes.

Type and number of devices: Addressable: ~~20~~ 30 Conventional: Coded: Transmitter:

Other (specify):

#### 5.1.2 Other Alarm Boxes

☒ This system does not have other alarm boxes.

Description:

Type and number of devices: Addressable: Conventional: Coded: Transmitter:

Other (specify):

### 5.2 Automatic Initiating Devices

#### 5.2.1 Smoke Detectors

☐ This system does not have smoke detectors.

Type and number of devices: Addressable: 30 Conventional: BEAM SMOKE DETECTION -  
11 IMAGERS AND EMITTERS

Other (specify):

Type of coverage: ☐ Complete area ☒ Partial area ☐ Nonrequired partial area

Other (specify):

Type of smoke detector sensing technology: ☐ Ionization ☒ Photoelectric ☐ Multicriteria ☐ Aspirating ☒ Beam

Other (specify):

#### 5.2.2 Duct Smoke Detectors

☐ This system does not have alarm-causing duct smoke detectors.

Type and number of devices: Addressable: 62 Conventional:

Other (specify):

Type of coverage: Partial Area - LOCAL @ SFD LOCATIONS

Type of smoke detector sensing technology: ☐ Ionization ☒ Photoelectric ☐ Aspirating ☐ Beam

#### 5.2.3 Radiant Energy (Flame) Detectors

☒ This system does not have radiant energy detectors.

Type and number of devices: Addressable: Conventional:

Other (specify):

Type of coverage:

#### 5.2.4 Gas Detectors

☒ This system does not have gas detectors.

Type of detector(s):

Number of devices: Addressable: Conventional:

Type of coverage:

#### 5.2.5 Heat Detectors

☒ This system does not have heat detectors.

Type and number of devices: Addressable: Conventional:

Type of coverage: ☐ Complete area ☐ Partial area ☐ Nonrequired partial area ☐ Linear ☐ Spot

Type of heat detector sensing technology: ☐ Fixed temperature ☐ Rate-of-rise ☐ Rate compensated



## 5. ALARM INITIATING DEVICES (continued)

### 5.2.6 Addressable Monitoring Modules

☐ This system does not have monitoring modules.

Number of devices: 29 — TROUBLE MONITORS, NON-ALARM POINTS

### 5.2.7 Waterflow Alarm Devices

☐ This system does not have waterflow alarm devices.

Type and number of devices: Addressable: 7 Conventional: Coded: Transmitter:

### 5.2.8 Alarm Verification

☒ This system does not incorporate alarm verification.

Number of devices subject to alarm verification: Alarm verification set for: seconds

### 5.2.9 Presignal

☒ This system does not incorporate pre-signal.

Number of devices subject to presignal:

Describe presignal functions:

### 5.2.10 Positive Alarm Sequence (PAS)

☒ This system does not incorporate PAS.

Describe PAS:

### 5.2.11 Other Initiating Devices

☒ This system does not have other initiating devices.

Describe:

## 6. SUPERVISORY SIGNAL-INITIATING DEVICES

### 6.1 Sprinkler System Supervisory Devices

☐ This system does not have sprinkler supervisory devices.

Type and number of devices: Addressable: 12 Conventional: Coded: Transmitter:

Other (specify):

### 6.2 Fire Pump Description and Supervisory Devices

☐ This system does not have a fire pump.

Type fire pump: ☒ Electric pump ☐ Engine

Type and number of devices: Addressable: 3 Conventional: Coded: Transmitter:

Other (specify):

#### 6.2.1 Fire Pump Functions Supervised

☒ Power ☒ Running ☒ Phase reversal ☐ Selector switch not in auto ☐ Engine or control panel trouble ☐ Low fuel

Other (specify):

### 6.3 Duct Smoke Detectors (DSDs)

☐ This system does not have DSDs causing supervisory signals.

Type and number of devices: Addressable: Conventional:

Other (specify):

Type of coverage:

Type of smoke detector sensing technology: ☐ Ionization ☐ Photoelectric ☐ Aspirating ☐ Beam

### 6.4 Other Supervisory Devices

☐ This system does not have other supervisory devices.

Describe: SMOKE FIRE DAMPER POSITION INDICATORS  
FIREFIGHTER SMOKE CONTROL PANEL

152  
11



## 7. MONITORED SYSTEMS

### 7.1 Engine-Driven Generator

☒ This system does not have a generator.

#### 7.1.1 Generator Functions Supervised

☐ Engine or control panel trouble    ☐ Generator running    ☐ Selector switch not in auto    ☐ Low fuel  
☐ Other (specify):

### 7.2 Special Hazard Suppression Systems

☒ This system does not monitor special hazard systems.

Description of special hazard system(s):

### 7.3 Other Monitoring Systems

☒ This system does not monitor other systems.

Description of special hazard system(s):

## 8. ANNUNCIATORS

☐ This system does not have annunciators.

### 8.1 Location and Description of Annunciators

Location 1: *Floor 2 North Lobby*

Location 2: *Floor 1 West Lobby*

Location 3:

## 9. ALARM NOTIFICATION APPLIANCES

### 9.1 In-Building Fire Emergency Voice Alarm Communication System

☐ This system does not have an EVACS.

Number of single voice alarm channels: *1*

Number of multiple voice alarm channels:

Number of speakers: *172*

Number of speaker circuits: *9*

Location of amplification and sound-processing equipment: *Electrical Rooms at FAPS Locations*

Location of paging microphone stations:

Location 1: *AT FACU, Room 122*

Location 2:

Location 3:

### 9.2 Nonvoice Notification Appliances

☐ This system does not have nonvoice notification appliances.

Horns: *0*

With visible: *—*

Bells: *1*

With visible: *0*

Chimes: *0*

With visible: *—*

Visible only: *66*

Other (describe):

### 9.3 Notification Appliance Power Extender Panels

☐ This system does not have power extender panels.

Quantity: *4*

Locations: *Rooms 267, 332, 467, 632*



## 10. MASS NOTIFICATION CONTROLS, APPLIANCES, AND CIRCUITS

☒ This system does not have an MNS.

### 10.1 MNS Local Operating Consoles

Location 1:

Location 2:

Location 3:

### 10.2 High-Power Speaker Arrays

Number of HPSA speaker initiation zones:

Location 1:

Location 2:

Location 3:

### 10.3 Mass Notification Devices

Combination fire alarm/MNS visible appliances:

MNS-only visible appliances:

Textual signs:

Other (describe):

Supervision class:

#### 10.3.1 Special Hazard Notification

☐ This system does not have special suppression predischARGE notification.

☐ MNS systems DO NOT override notification appliances required to provide special suppression predischARGE notification.

## 11. TWO-WAY EMERGENCY COMMUNICATION SYSTEMS

### 11.1 Telephone System

☐ This system does not have a two-way telephone system.

Number of telephone jacks installed:

12

Number of warden stations installed:

0

Number of telephone handsets stored on site:

5

Type of telephone system installed: ☐ Electrically powered ☒ Sound powered

### 11.2 Two-Way Radio Communications Enhancement System

☒ This system does not have a two-way radio communications enhancement system.

Percentage of area covered by two-way radio service: Critical areas:

%

General building areas:

%

Amplification component locations:

Inbound signal strength:

dBm

Outbound signal strength:

dBm

Donor antenna isolation is:

dB above the signal booster gain

Radio frequencies covered:

Radio system monitor panel location:



## 11. TWO-WAY EMERGENCY COMMUNICATION SYSTEMS (continued)

### 11.3 Area of Refuge (Area of Rescue Assistance) Emergency Communications Systems

☒ This system does not have an area of refuge (area of rescue assistance) emergency communications system.

Number of stations:

Location of central control point:

Days and hours when central control point is attended:

Location of alternate control point:

Days and hours when alternate control point is attended:

### 11.4 Elevator Emergency Communications Systems

☒ This system does not have an elevator emergency communications system.

Number of elevators with stations:

Location of central control point:

Days and hours when central control point is attended:

Location of alternate control point:

Days and hours when alternate control point is attended:

### 11.5 Other Two-Way Communication Systems

Describe:

## 12. CONTROL FUNCTIONS

This system activates the following control functions:

☒ Hold-open door releasing devices    ☒ Smoke management    ☒ HVAC shutdown    ☒ F/S dampers

☐ Door unlocking    ☒ Elevator recall    ☐ Fuel source shutdown    ☐ Extinguishing agent release

☐ Elevator shunt trip    ☐ Mass notification system override of fire alarm notification appliances

Other (specify):

### 12.1 Addressable Control Modules

☐ This system does not have control modules.

Number of devices:

90 - RELAY + CONTROL FUNCTIONS

Other (specify):

## 13. SYSTEM POWER

### 13.1 Control Unit

#### 13.1.1 Primary Power

Input voltage of control panel:

120 VAC

Control panel amps:

6 AMP

Overcurrent protection:

Type:

BREAKER

Amps:

20 AMP

Location (of primary supply panel board):

PANEL 1D W, CIRCUIT #

Disconnecting means location:

TEL/DATA ROOM #106

#### 13.1.2 Engine-Driven Generator

☒ This system does not have a generator.

Location of generator:

Location of fuel storage:

Type of fuel:



### 13. SYSTEM POWER (continued)

#### 13.1.3 Uninterruptible Power System

☒ This system does not have a UPS.

Equipment powered by a UPS system:

Location of UPS system:

Calculated capacity of UPS batteries to drive the system components connected to it:

In standby mode (hours):

In alarm mode (minutes):

#### 13.1.4 Batteries

Location: AT FACU Type: SLA Nominal voltage: 12VDC Amp/hour rating: 55AH

Calculated capacity of batteries to drive the system:

In standby mode (hours): 24

In alarm mode (minutes): 15

☒ Batteries are marked with date of manufacture ☐ Battery calculations are attached ON AS-BUILT PLANS

#### 13.2 In-Building Fire Emergency Voice Alarm Communication System or Mass Notification System

☐ This system does not have an EVACS or MNS system.

##### 13.2.1 Primary Power

Input voltage of EVACS or MNS panel: 120VAC EVACS or MNS panel amps: 3AMP

Overcurrent protection: Type: BREAKER Amps: 20AMP

Location (of primary supply panel board): PANEL 1 DW CIRCUIT#

Disconnecting means location: TEL/DATA Room 106

##### 13.2.2 Engine-Driven Generator

☒ This system does not have a generator.

Location of generator:

Location of fuel storage:

Type of fuel:

##### 13.2.3 Uninterruptible Power System

☒ This system does not have a UPS.

Equipment powered by a UPS system:

Location of UPS system:

Calculated capacity of UPS batteries to drive the system components connected to it:

In standby mode (hours):

In alarm mode (minutes):

##### 13.2.4 Batteries

Location: AT FACU Type: SLA Nominal voltage: 12VDC Amp/hour rating: 55AH

Calculated capacity of batteries to drive the system:

In standby mode (hours): 24

In alarm mode (minutes): 15

☒ Batteries are marked with date of manufacture ☐ Battery calculations are attached ON AS-BUILT PLAN



### 13. SYSTEM POWER (continued)

#### 13.3 Notification Appliance Power Extender Panels

☐ This system does not have power extender panels.

##### 13.3.1 Primary Power

Input voltage of power extender panel(s): 120 VAC

Power extender panel amps: 6 AMP

Overcurrent protection: Type: BREAKER

Amps: 20 AMP

Location (of primary supply panel board): PANEL 2SB-W#1

ROOMS 267,

Disconnecting means location:

PANEL 3SB-E#6

332, 467, 632

PANEL 4SB-W#9

##### 13.3.2 Engine-Driven Generator

PANEL 6SB-W#27

☒ This system does not have a generator.

Location of generator:

Location of fuel storage:

Type of fuel:

##### 13.3.3 Uninterruptible Power System

☒ This system does not have a UPS.

Equipment powered by a UPS system:

Location of UPS system:

Calculated capacity of UPS batteries to drive the system components connected to it:

In standby mode (hours):

In alarm mode (minutes):

##### 13.3.4 Batteries

Location:

Type:

Nominal voltage:

Amp/hour rating:

Calculated capacity of batteries to drive the system:

In standby mode (hours):

In alarm mode (minutes):

☐ Batteries are marked with date of manufacture

☐ Battery calculations are attached

### 14. RECORD OF SYSTEM INSTALLATION

Fill out after all installation is complete and wiring has been checked for opens, shorts, ground faults, and improper branching, but before confuting operational acceptance tests.

This is a: ☒ New system ☐ Modification to an existing system Permit number:

The system has been installed in accordance with the following requirements: (Note any or all that apply.)

☒ NFPA 72, Edition: 2007

☒ NFPA 70, National Electrical Code, Article 760, Edition: 2005, NEC 2007

☒ Manufacturer's published instructions

Other (specify): CBC 2007, CFC 2007, PARTS OF CFC 2010

System deviations from referenced NFPA standards: NONE

APPROVED PLANS  
+ SPECIFICATION

Signed:



Printed name:

CURTIS STREETER

Date:

Organization:

DEEP BLUE INTEGRATION, INC.

Title:

PRESIDENT

Phone:

888-600-0324



## 15. RECORD OF SYSTEM OPERATIONAL ACCEPTANCE TEST

☒ New system

All operational features and functions of this system were tested by, or in the presence of, the signer shown below, on the date shown below, and were found to be operating properly in accordance with the requirements for the following:

☐ Modifications to an existing system

All newly modified operational features and functions of the system were tested by, or in the presence of, the signer shown below, on the date shown below, and were found to be operating properly in accordance with the requirements of the following:

☒ NFPA 72, Edition: 2007

☒ NFPA 70, National Electrical Code, Article 760, Edition: 2005, CEC 2007

☒ Manufacturer's published instructions

APPROVED PLANS + SPECIFICATIONS  
Other (specify): CBC 2007, CFC 2007, PARTS OF CFC 2010

☒ Individual device testing documentation [Inspection and Testing Form (Figure 14.6.2.4) is attached] ON CD ROM

Signed:



Printed name:

CURTIS STREETER

Date:

8-15-13

Organization:

DEEP BLUE INTEGRATION  
INC.

Title:

PRESIDENT

Phone:

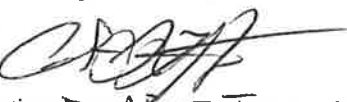
888-600-0324

## 16. CERTIFICATIONS AND APPROVALS

### 16.1 System Installation Contractor:

This system, as specified herein, has been installed and tested according to all NFPA standards cited herein.

Signed:



Printed name:

CURTIS STREETER

Date:

8-15-13

Organization:

DEEP BLUE INTEGRATION  
INC.

Title:

PRESIDENT

Phone:

888-600-0324

### 16.2 System Service Contractor:

The undersigned has a service contract for this system in effect as of the date shown below.

Signed:



Printed name:

CURTIS STREETER

Date:

8-15-13

Organization:

DEEP BLUE INTEGRATION  
INC.

Title:

PRESIDENT

Phone:

888-600-0324

### 16.3 Supervising Station:

This system, as specified herein, will be monitored according to all NFPA standards cited herein.

Signed:



Printed name:

CURTIS STREETER

Date:

8-15-13

Organization:

DEEP BLUE INTEGRATION  
INC.

Title:

PRESIDENT

Phone:

888 600 0324

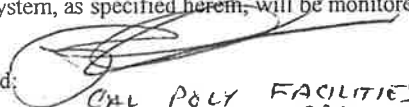


## 16. CERTIFICATIONS AND APPROVALS (continued)

### 16.4 Property or Owner Representative:

This system, as specified herein, will be monitored according to all NFPA standards cited herein.

Signed:

  
Organization: CAL POLY FACILITIES  
\* CAPITAL PROJECTS

Printed name:

PERRY JUDD

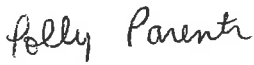
Date:

Phone: 805-441-2186

### 16.5 Authority Having Jurisdiction:

I have witnessed a satisfactory acceptance test of this system and find it to be installed and operating properly in accordance with its approved plans and specifications, with its approved sequence of operations, and with all NFPA standards cited herein.

Signed:

  
Organization: OSFM

Printed name:

Polly Parenti

Date: 8-15-13

Title:

DEPUTY STATE FIRE MARSHAL

Phone:

916-825-7880



GENERAL NOTES

1. NOTIFICATION DEVICES CANNOT BE T-TAPPED. ADDRESSABLE (IDC) DEVICES CAN BE T-TAPPED. ALL FIRE ALARM CABLING SHALL BE RUN FROM DEVICE TO DEVICE, WITH NO SPLICES. ANY REQUIRED TERMINATIONS MUST BE MADE IN APPROVED BOX.
2. ALL INTERIOR INITIATING DEVICES, NOTIFICATION DEVICES, AND MODULES REQUIRE 4"SQUARE SPECIAL DEEP BACK BOXES U.O.N.
3. PANEL BACK BOXES AND OTHER LISTED BACK BOXES SHALL BE PROVIDED TO THE EC BY DBI. ALL CONTROL PANELS, POWER SUPPLIES, AND BATTERY BOXES SHALL UTILIZE ONLY FACTORY KNOCKOUTS NEAR THE TOP OF THE CAN TO ALLOW PLACEMENT OF BATTERIES.
4. ALL FIRE ALARM CONDUIT TO BE 3/4" EMT MINIMUM U.O.N. FIRE ALARM CONDUIT SHALL BE SEPARATE FROM CONDUIT SYSTEM FOR SECURITY ALARM CABLING AND OTHER SYSTEMS.
5. WALL MOUNT AUDIO/VISUAL DEVICES SHALL BE MOUNTED 80" AFF TO BOTTOM OF THE STROBE LENS.
6. MANUAL PULL STATIONS SHALL BE MOUNTED 48" AFF TO CENTERLINE OF BOX. MPS SHALL BE DOUBLE ACTION AND KEYED THE SAME AS THE FACP.
7. DEDICATED 120 VAC CIRCUIT WITH LOCKOUT @ BREAKER TO BE PROVIDED BY OTHERS AT LOCATION OF PANELS AND POWER SUPPLIES.
8. KNOX BOX, PIV, SUPERVISORY SWITCHES, FLOW SWITCHES, SOLENOIDS, AND SPRINKLER BELLS SHALL BE PROVIDED BY OTHERS.
9. SMOKE DETECTORS SHALL NOT BE PLACED WITHIN 3' OF ANY SUPPLY AIR REGISTER OR WHERE THE AIR MOVEMENT EXCEEDS THE MANUFACTURER'S LISTING.
10. FIRE FIGHTER TELEPHONE RISER IS CLASS A, STYLE Z
11. VOLTAGE DROP CALCULATIONS FOR NOTIFICATION DEVICES ARE BASED ON THE LAYOUT SHOWN. DEVIATION FROM THESE PLANS COULD RESULT IN ADDITIONAL CONDUIT WORK, REENGINEERING, UPSIZED CABLE AND/OR ADDITIONAL POWER REQUIREMENTS.
12. PAINT ALL FIRE ALARM JUNCTION BOXES AND COVERS RED IN UNFINISHED AREAS (IE ABOVE CEILINGS, MECHANICAL ROOMS ETC.) IN FINISHED AREAS CONDUIT AND JUNCTION BOXES CAN BE PAINTED TO MATCH THE ROOM FINISH, THE INSIDE COVER IF THE JUNCTION BOX MUST BE IDENTIFIED AS "FIRE ALARM" AND THE CONDUIT MUST HAVE PAINTED RED BANDS 3/4" WIDE AT 10' CENTERS AND AT EACH SIDE OF A FLOOR, WALL, OR CEILING PENETRATION.

13. UPON COMPLETION OF INSTALLATION OF THE FIRE ALARM SYSTEM A SATISFACTORY TEST OF THE ENTIRE SYSTEM SHALL BE MADE IN THE PRESENCE OF THE AUTHORITY HAVING JURISDICTION (AHJ).

14. ALL NOTIFICATION DEVICES SHALL BE SYNCHRONIZED.

15. A STAMPED SET OF APPROVED FIRE ALARM PLANS SHALL BE AT THE JOBSITE AND USED FOR INSTALLATION.

16. SIGNALING LINE CIRCUIT IS CLASS B, STYLE 4

17. NOTIFICATION APPLIANCE CIRCUIT IS CLASS B, STYLE Y

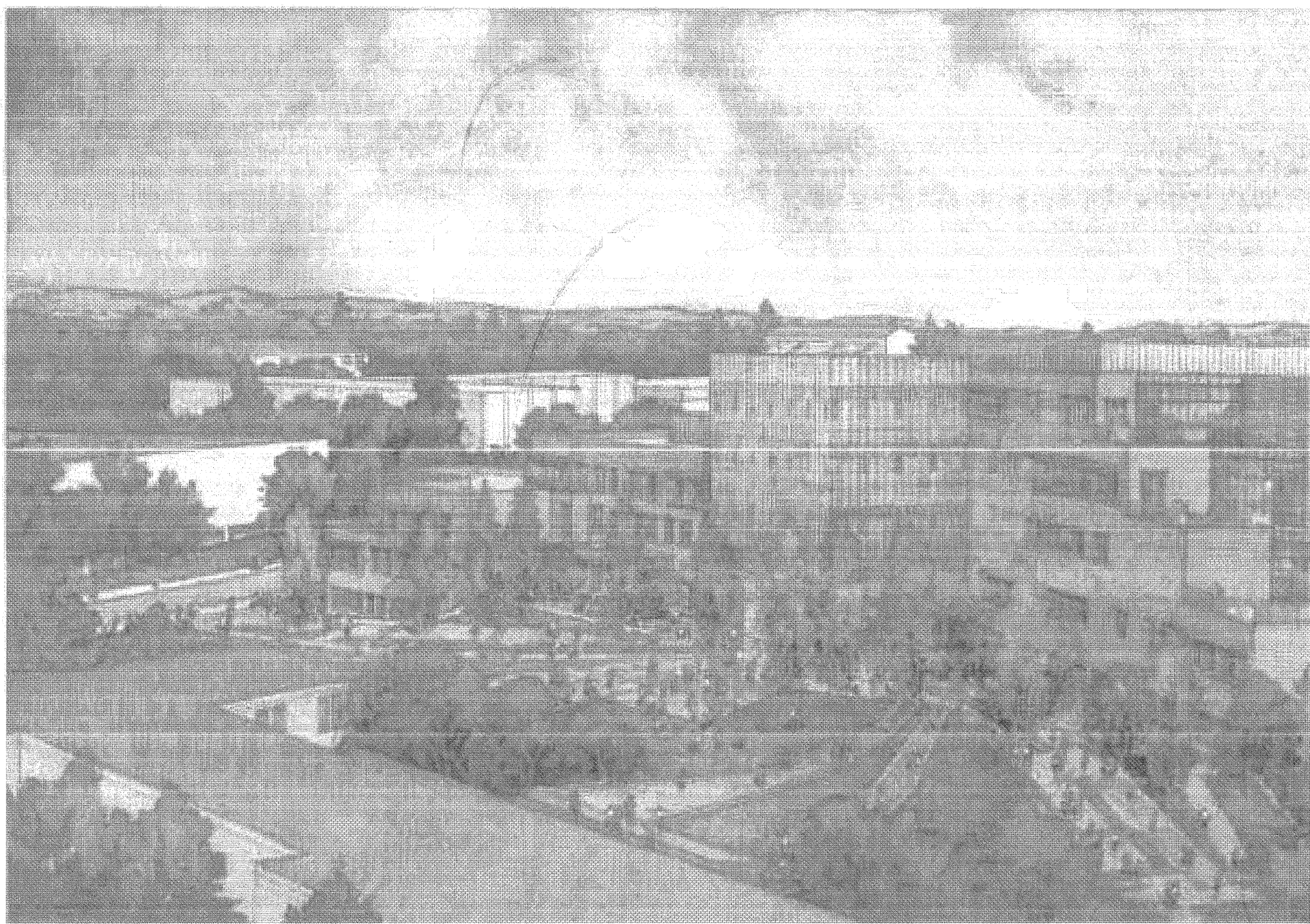
18. ALL SMOKE DETECTORS SHALL BE INSTALLED AT LEAST 1'-0" FROM FLUORESCENT LIGHT FIXTURES TO AVOID UNWANTED ALARMS AND SHALL BE INSTALLED IN AREAS THAT DO NOT EXCEED THE MANUFACTURE'S OPERATING TEMPERATURE RANGE BETWEEN 32°F AND 120°F.

CODE REGULATIONS

CALIFORNIA CODE REGULATIONS	
APPLICABLE CODES	
2007 BUILDING STANDARDS ADMINISTRATIVE CODE	TITLE 24 PART 1
2007 CALIFORNIA BUILDING CODE (CBC)	TITLE 24 PART 2
2007 CALIFORNIA ELECTRICAL CODE (CEC)	TITLE 24 PART 3
2007 CALIFORNIA MECHANICAL CODE (CMC)	TITLE 24 PART 4
2007 CALIFORNIA PLUMBING CODE (CPC)	TITLE 24 PART 5
2007 CALIFORNIA ENERGY CODE	TITLE 24 PART 6
2007 CALIFORNIA ELEVATOR SAFETY CONSTRUCTION CODE	TITLE 24 PART 7
2007 CALIFORNIA HISTORICAL BUILDING CODE	TITLE 24 PART 8
2007 CALIFORNIA FIRE CODE (CFC)	TITLE 24 PART 9
2007 CALIFORNIA REFERENCED STANDARDS CODE	TITLE 24 PART 12
APPLICABLE STANDARDS & GUIDELINES	
2007 AUTOMATIC SPRINKLER SYSTEMS	NFPA 13
2007 STATIONARY PUMPS	NFPA 20
2007 NATIONAL FIRE ALARM CODES (CALIFORNIA AMENDED)	NFPA 72
2007 STANDARD FOR INSTALLATION OF AIR-CONDITIONING	NFPA 90A
2007 STANDARD FOR INSTALLATION OF WARM AIR HEATING	NFPA 90B
2006 STANDARD FOR SMOKE-CONTROL SYSTEMS UTILIZING BARRIERS	NFPA 92A
2006 AND PRESSURE DIFFERENCES	
2005 STANDARD FOR SMOKE MANAGEMENT SYSTEMS IN MALLS, ATRIA, AND LARGE SPACES	NFPA 92B

CENTER FOR SCIENCE AND MATHEMATICS  
CALIFORNIA STATE POLYTECHNIC UNIVERSITY  
SAN LUIS OBISPO, CALIFORNIA 93407  
FIRE ALARM & EMERGENCY COMMUNICATION SYSTEM

SITE PLAN



CENTER FOR SCIENCE

PROJECT DESCRIPTION

1. OCCUPANCY TYPE: A, B, AND H3
2. SYSTEM TYPE: CLASS B, ADDRESSABLE, MANUAL
3. METHOD OF COMMUNICATION: TELEPHONE
4. SCOPE OF WORK: FIRE ALARM & VOICE EVACUATION SYSTEMS

SEQUENCE OF OPERATIONS MATRIX

EVENT	ACTION													
	TROUBLE CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)	ALARM CONDITION (T FACD)
PANEL SUPERVISORY CONDITION (TEST BYPASS) ON ACM-24 AT	X													
PANEL TROUBLE CONDITION (AC POWER FAIL, LOW BATTERY, OPEN CIRCUIT, GROUND FAULT, ETC.)		X	X	X					X	X				
PANEL ALARM CONDITION			X	X	X					X	X			
MANUAL PULL STATION ACTIVATION			X	X	X					X	X			
SPOT SMOKE DETECTOR ACTIVATION			X	X	X					X	X			
DUCT SMOKE DETECTOR ACTIVATION			X	X	X					X	X			
AIR HANDLING UNIT DUCT SMOKE DETECTOR ACTIVATION			X	X	X	X				X	X			
SPRINKLER WATER FLOW ACTIVATION	X		X	X	X					X	X			
FIRE PUMP RUNNING		X	X	X	X					X	X			
FIRE PUMP LOSS OF PHASE		X	X	X	X					X	X			
FIRE PUMP PHASE REVERSAL		X	X	X	X					X	X			
HEAT DETECTOR ACTIVATION (ELEVATOR EQUIPMENT)		X	X	X	X					X	X			
ELEVATOR LOBBY (SMR SMOKE) ELEVATOR HOISTWAYS		X	X	X	X	X				X	X			
SHUNT TRIP POWER SUPERVISION		X	X	X	X					X	X			
GENERAL ALARM (ANYWHERE WITHIN THE BUILDING)		X	X	X	X					X	X		X	X
ATRILUM SMOKE CONTROL SYSTEM ALARM		X	X	X	X					X	X		X	X
BEAM SMOKE DETECTION WITHIN ATRILUM		X	X	X	X					X	X		X	X
PULL STATION WITHIN ATRILUM		X	X	X	X					X	X		X	X
SPRINKLER WATER FLOW WITHIN ATRILUM		X	X	X	X					X	X		X	X

SYMBOL LEGEND

COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #
31	[F] MANUAL PULL STATION	NBG-12LX	7150-0028:0199
73	[F] STROBE ONLY	SW	7320-1653:201
165	[F] SPEAKER/STROBE	SPWS	7320-1653:201
6	[F] SPEAKER ONLY	SPW	7320-1653:201
7	WP [F] SPEAKER - WEATHER PROOF	SPWK	7320-1653:201
0	[H] HEAT DETECTOR	FST-851	7270-0028:196
18	[S] SMOKE DETECTOR	FSP-851	7272-0028:206
64	[S] <sub>D</sub> SMOKE DETECTOR - DUCT	DNR	3242-1653:209
23	[S] <sub>BT</sub> BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728:0121
15	[S] <sub>BR</sub> BEAM SMOKE DETECTOR- RECEIVER	OSI-90	7260-1728:0121
1	[FACP] FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028:0243
5	[RNPS] REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028:248
4	[FATC] FIRE ALARM TERMINAL CABINET	N/A	N/A
32	[EOL] END OF LINE RESISTOR	N/A	N/A
2	[RA] REMOTE ANNUNCIATOR	FDU-80	7120-0028:209
8	[MD] MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	[AM] ADDRESSABLE MODULE	FMM-1	7300-0028:0219
12	[RM] RELAY MODULE	FRM-1	7300-0028:219
16	[WFS] WATER FLOW SWITCH	N/A	BY OTHERS
10	[VTS] VALVE TAMPER SWITCH	N/A	BY OTHERS
21	[FDM] DUAL MONITOR MODULE	FDM-1	7300-0028:0219
64	[FDRM] DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028:0219
12	[FJ] FIRE FIGHTER'S PHONE JACKS	FTM-1	7300-1652:0182
4	[DAA2] DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028:223 7170-0028:224
1	[XP6-R] SIX RELAY CONTROL MODULE	XP6-R	7300-0028:0219
1	[XP10-M] TEN-INPUT MONITOR MODULE	XP10-M	7300-0028:0219

WIRING LEGEND

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2	UTP SLC	WEST PENN D990
B	16/2	TSP	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4	TS ANNUNCIATOR	WEST PENN 993
F	14/2	TSP FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX

1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0

A5-BUILT  
SET COVER SHEET

**Deep Blue Integration**

Consulting - Design - Installation  
Service - Monitoring

Deep Blue Integration, Inc.  
3442 Empress Drive Suite C  
San Luis Obispo, CA 93401  
C-10, C-16 #943465 ACO#8864  
Toll Free: 888-830-0091 DBI FAX: 805-791-2037  
www.deepblueintegration.com

Revisions		DATE	DESCRIPTION
REVIEW COMMENTS			
CRB 1 08/11 & F1 99		8/20/2012	
SPM REVIEW COMMENTS		8/20/2012	
CRB 8.2		1/15/2013	
FA & SMOKE CONTROL SPM COMMENTS		4/2/2013	
AS-BUILT DRAWINGS		8/23/2013	

DESIGNED BY: Curtis Streeter	DATE: 08/23/2013	SCALE:	DRAWING CODE: FA ALL DRAWINGS CPFS
DRAWN BY: Derek Richardson			
CHECKED BY: CURTIS STREETER, SET INSET IV #102872			
PROJECT ENGINEER: Integral Design Associates, INC.			

CENTER FOR SCIENCE AND MATHEMATICS  
CALIFORNIA STATE POLYTECHNIC UNIVERSITY  
SAN LUIS OBISPO, CA

CSFM #18-40-03-0001



SYMBOL LEGEND

COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #
31	[MANUAL PULL STATION]	NBG-12LX	7150-0028-0199
73	[STROBE ONLY]	SW	7320-1653-201
185	[SPEAKER/STROBE]	SPWS	7320-1653-201
6	[SPEAKER ONLY]	SPW	7320-1653-201
7	[SPEAKER - WEATHER PROOF]	SPWK	7320-1653-201
0	[HEAT DETECTOR]	FST-851	7270-0028-196
18	[SMOKE DETECTOR]	FSP-851	7272-0028-206
64	[SMOKE DETECTOR - DUCT]	DNR	3242-1653-209
23	[BEAM SMOKE DETECTOR - TRANSMITTER]	OSE-SPW	7260-1728-0121
15	[BEAM SMOKE DETECTOR - RECEIVER]	OSI-90	7260-1728-0121
1	[FIRE ALARM CONTROL PANEL]	NFS2-640	7165-0028-0243
5	[REMOTE NOTIFICATION POWER SUPPLY]	ACPS-610	7315-0028-248
4	[FIRE ALARM TERMINAL CABINET]	N/A	N/A
32	[END OF LINE RESISTOR]	N/A	N/A
2	[REMOTE ANNUNCIATOR]	FDU-80	7120-0028-209
8	[MAGNETIC DOOR HOLDER]	N/A	BY OTHERS
21	[ADDRESSABLE MODULE]	FMM-1	7300-0028-0219
12	[RELAY MODULE]	FRM-1	7300-0028-219
16	[WATER FLOW SWITCH]	N/A	BY OTHERS
10	[VALVE TAMPER SWITCH]	N/A	BY OTHERS
21	[DUAL MONITOR MODULE]	FDM-1	7300-0028-0219
64	[DUAL RELAY / MONITOR MODULE]	FDRM-1	7300-0028-0219
12	[FIRE FIGHTERS PHONE JACKS]	FTM-1	7300-1652-0182
4	[DIGITAL AUDIO AMPLIFIERS]	DAA2	7170-0028-223 7170-0028-224
1	[SIX RELAY CONTROL MODULE]	XP6-R	7300-0028-0219
1	[TEN-INPUT MONITOR MODULE]	XP10-M	7300-0028-0219

GENERAL NOTES:

- The Notification Appliance Circuits vary between 14 AWG and 12 AWG, see voltage drops for correct sizing.
- All smoke detectors shall be placed at least 1'-0" from fluorescent light fixtures to avoid unwanted alarms and in areas that will not exceed manufacturer's specified operating temperature 32°F to 120°F.

SHEET NOTES:

- The fire alarm control panel shall be connected to a separate dedicated branch circuit, maximum 20 amperes. This circuit shall be labeled at the main power distribution panel as FIRE ALARM. Fire alarm control panel primary power wiring shall be 12 AWG. The control panel cabinet shall be grounded securely to either a cold water pipe or grounding rod.
  - The riser going between floors will be in 2" conduit or larger.
  - 6.10.1.16\* All circuits necessary for the operation of two-way telephone communication systems shall be installed using one of the following methods:
    - A 2-hour fire rated circuit integrity (CI) cable
    - A 2-hour fire rated cable system (electrical circuit protective system)
    - A 2-hour fire rated enclosure
    - Performance alternatives approved by the authority having jurisdiction
    - Buildings fully protected by an automatic sprinkler system installed in accordance with NFPA 13, Standard for the Installation of Sprinkler Systems, with the wiring or cables installed in metal raceways and in accordance with Article 760 of NFPA 70
- A.6.10.1.16 One or more of the following means might be considered acceptable to provide a level of survivability consistent with the intent of this requirement:
  - Routing two-way telephone circuits separately
  - Using short-circuit fault tolerant circuits

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Service - Monitoring  
Deep Blue Integration, Inc.  
3442 Empress Drive Suite C  
San Luis Obispo, CA 93401  
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Toll Free: 888-6000-DBI FAX:  
805-791-2037  
www.deepblueintegration.com

Revisions

REVIEW COMMENTS	DATE	SYMBOL	DESCRIPTION	APPR.
1. REVIEW COMMENTS	8/4/2013			
2. CRP # 095.1 & F1 99	8/17/2013			
3. SFM REVIEW COMMENTS	8/20/2013			
4. CRP 93.2	11/5/2013			
5. FA & SMOKE CONTROL SFM COMMENTS	4/2/2013			
6. AS-BUILT DRAWINGS	8/23/2013			

DESIGNED BY: Curtis Streeter	DATE: 08/23/2013	DRAWN BY: Derek Richardson	SCALE: AS SHOWN
CHECKED BY: CURTIS STREETER, SET NICET IV #102872		DRAWING CODE: FA-ALL DRAWINGS CPCS	PROJECT ENGINEER: Integral Design Associates INC.

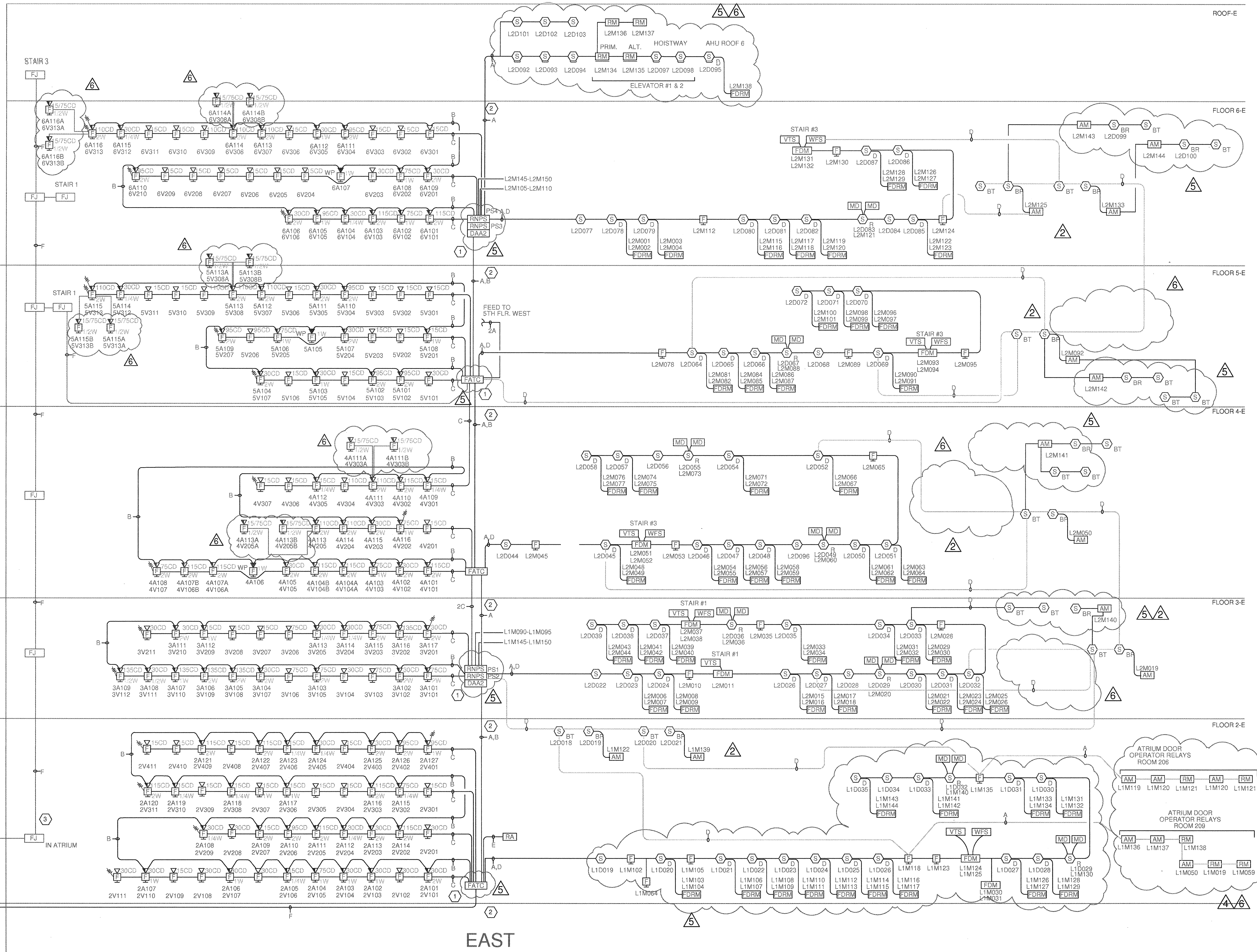
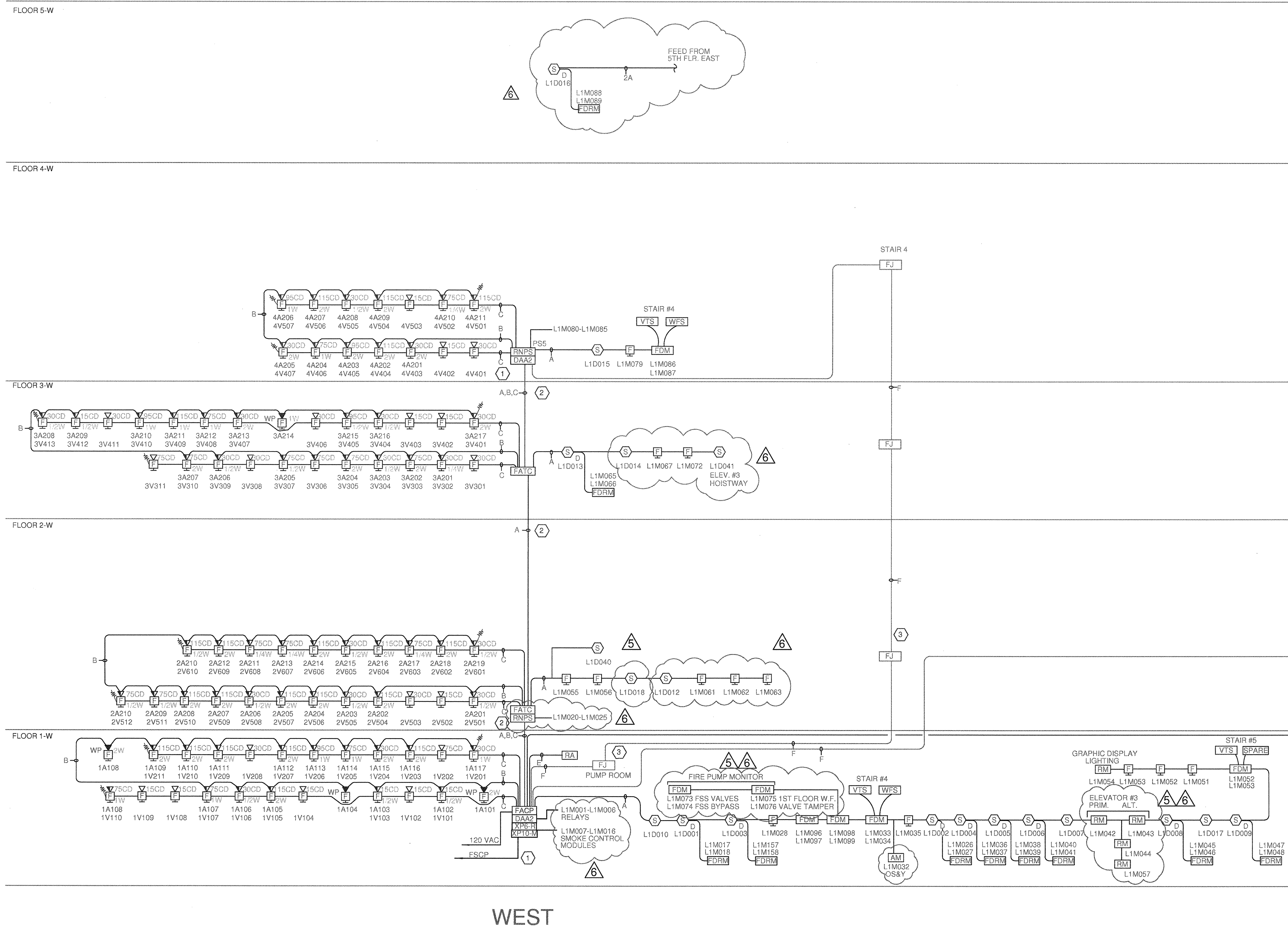
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CALIFORNIA STATE POLYTECHNIC UNIVERSITY  
SAN LUIS OBISPO, CA

CSFM #18-40-03-0001

SHEET ID

FA 1.0

SHEET 2 OF 15



WIRING LEGEND

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2	UTP SLC	WEST PENN D990
B	16/2	TSP SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4	TS ANNUNCIATOR	WEST PENN 993
F	14/2	TSP FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX

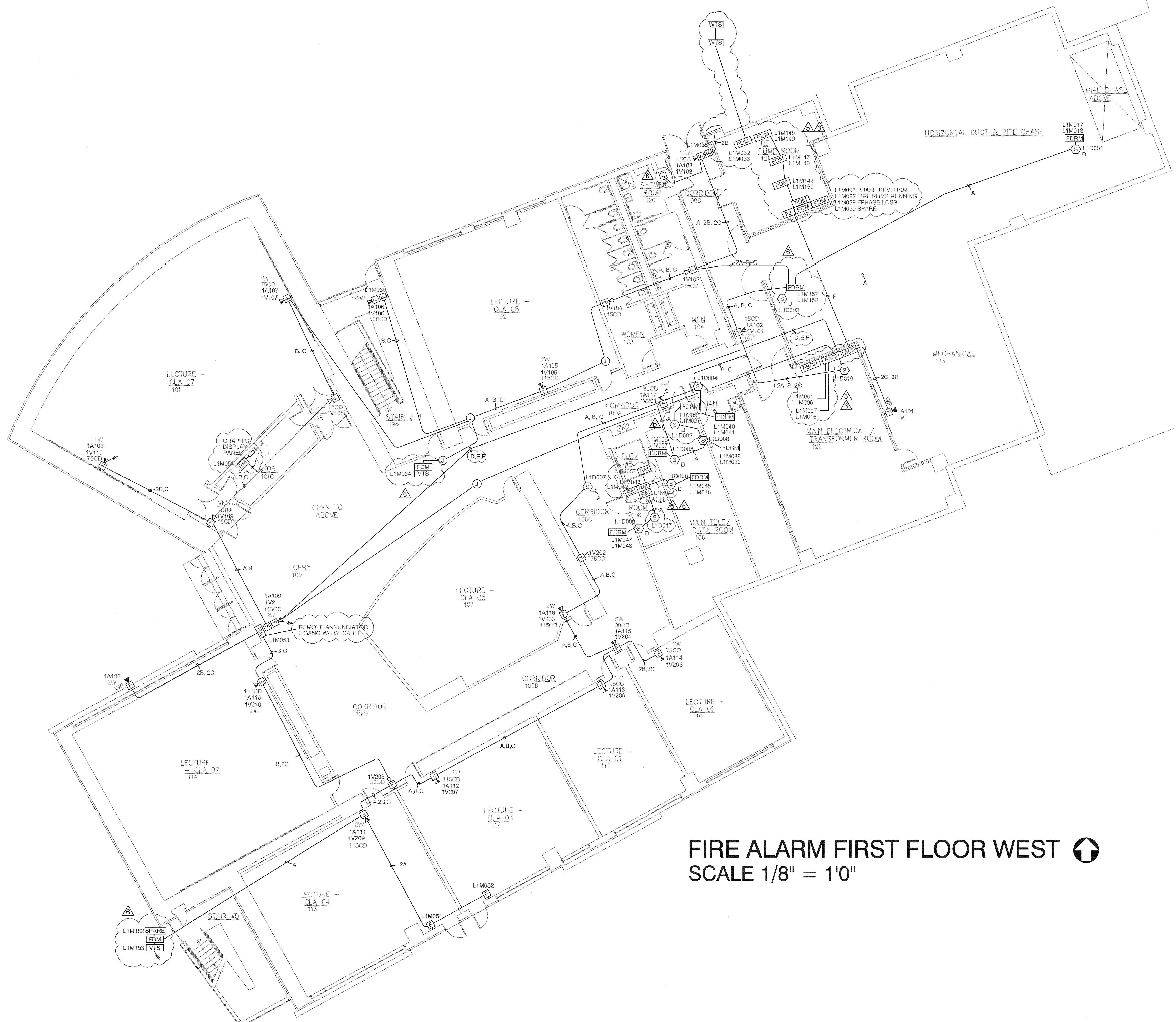
1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0



REVISIONS		DATE	DESCRIPTION	APPR.
1	REVIEW COMMENTS	6/14/2011		
2	CRB # 053.1 & F1 99	5/19/2012		
3	SFM REVIEW COMMENTS	8/20/2012		
4	CRB # 2	1/15/2013		
5	FA & SMOKE CONTROL SFM COMMENTS	4/2/2013		
6	AS-BUILT DRAWINGS	8/23/2013		

DESIGNED BY: Curt Streever	DATE: 08/23/2013	SCALE:	DRAWING CODE: FA ALL DRAWINGS CPDPS	PROJECT ENGINEER: Integral Design Associates INC.
DRAWN BY: Derek Richardson				
CHECKED BY: CURTIS STREEVER, SET NICETV #102672				

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SAN LUIS OBISPO, CA  
CSFM #18-40-03-0001



FIRE ALARM FIRST FLOOR WEST  
SCALE 1/8" = 1'0"

SYMBOL LEGEND

COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #
31	MANUAL PULL STATION	NBG-12LX	7150-0028-0199
73	STROBE ONLY	SW	7320-1653-201
165	SPEAKER/STROBE	SPWS	7320-1653-201
6	SPEAKER ONLY	SPW	7320-1653-201
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653-201
0	HEAT DETECTOR	FST-951	7270-0028-196
18	SMOKE DETECTOR	FSP-851	7272-0028-206
84	SMOKE DETECTOR - DUCT	DNR	3242-1653-209
28	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728-0121
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-80	7260-1728-0121
1	FACP FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028-0243
5	RNPS REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028-248
4	FATC FIRE ALARM TERMINAL CABINET	N/A	N/A
32	END OF LINE RESISTOR	N/A	N/A
2	RA REMOTE ANNUNCIATOR	FDU-80	7120-0028-209
8	MD MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	AM ADDRESSABLE MODULE	FMM-1	7300-0028-0219
12	RM RELAY MODULE	FRM-1	7300-0028-219
16	WFS WATER FLOW SWITCH	N/A	BY OTHERS
10	VTS VALVE TAMPER SWITCH	N/A	BY OTHERS
21	FDM DUAL MONITOR MODULE	FDM-1	7300-0028-0219
64	FDRM DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028-0219
12	FJ FIRE FIGHTERS PHONE JACKS	FTM-1	7300-1652-0182
4	DAA2 DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028-223 7170-0028-224
1	XP6-R SIX RELAY CONTROL MODULE	XP6-R	7300-0028-0219
1	XP10-M TEN-INPUT MONITOR MODULE	XP10-M	7300-0028-0219

WIRING LEGEND

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4 TS	ANNUNCIATOR	WEST PENN 993
F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX

1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0



Revisions		DATE	DESCRIPTION
1	REVIEW COMMENTS	6/14/2011	
2	CRB # 882.1 & F 89	5/15/2012	
3	SFM REVIEW COMMENTS	8/20/2012	
4	CRB # 832	1/15/2013	
5	FA1 SMOKE CONTROL SFM COMMENTS	4/23/2013	
6	AS-BUILT DRAWINGS	8/23/2013	

DESIGNED BY: Curtis Streeter	DATE: 09/23/2013	SCALE: AS SHOWN	DRAWING CODE: FA ALL DRAWINGS CPCS
DRAWN BY: Derek Richardson			
CHECKED BY: CURTIS STREETER, SET NCET 11/16/2012			
PROJECT ENGINEER: Integral Design Associates INC.			

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SAN LUIS OBISPO, CA  
CSPM #18-40-03-0001



FIRE ALARM SECOND FLOOR WEST  
SCALE 1/8" = 1'0"

SYMBOL LEGEND			
COUNT	FIRE ALARM SYMBOLS	MODEL #	CSPM LISTING #
31	MANUAL PULL STATION	NBG-12LX	7150-0028:0199
73	STROBE ONLY	SW	7320-1653:201
165	SPEAKER/STROBE	SPWS	7320-1653:201
6	SPEAKER ONLY	SPW	7320-1653:201
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653:201
0	HEAT DETECTOR	FST-851	7270-0028:196
18	SMOKE DETECTOR	FSP-851	7272-0028:206
64	SMOKE DETECTOR - DUCT	DNR	3242-1653:209
23	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728:0121
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-90	7260-1728:0121
1	FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028:0243
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028:248
4	FIRE ALARM TERMINAL CABINET	N/A	N/A
32	END OF LINE RESISTOR	N/A	N/A
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028:209
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	ADDRESSABLE MODULE	FMM-1	7300-0028:0219
12	RELAY MODULE	FRM-1	7300-0028:219
16	WATER FLOW SWITCH	N/A	BY OTHERS
10	VALVE TAMPER SWITCH	N/A	BY OTHERS
21	DUAL MONITOR MODULE	FDM-1	7300-0028:0219
64	DUAL RELAY / MONITOR MODULE	FORM-1	7300-0028:0219
12	FIRE FIGHTER'S PHONE JACKS	FTM-1	7300-1652:0182
4	DIGITAL AUDIO AMPLIFIERS	DA2-R	7170-0028:223 7170-0028:224
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028:0219
1	TEN-INPUT MONITOR MODULE	XP10-M	7300-0028:0219

WIRING LEGEND			
LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4 TS	ANNUNCIATOR	WEST PENN 993
F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX		
1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0



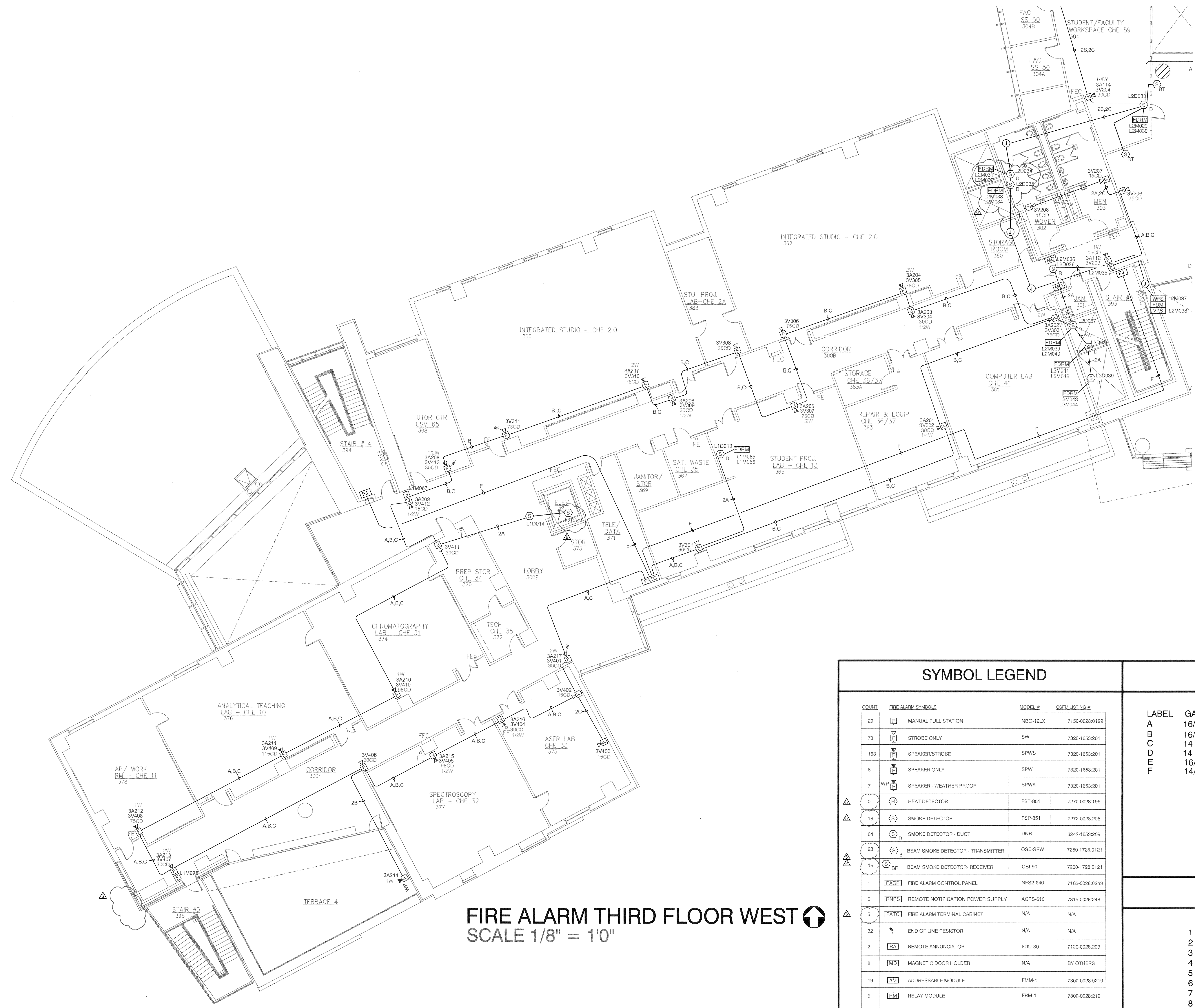
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Revisions		DATE	DESCRIPTION	APPROVED
1	REVIEW COMMENTS	8/14/2011		
2	CRB # 0831 & F19	5/18/2012		
3	SPM REVIEW COMMENTS	4/11/2012		
4	CRB # 932	8/20/2012		
5	FA & SMOKE CONTROL SPM COMMENTS	1/15/2013		
6	AS-BUILT DRAWINGS	4/2/2013		
7		8/22/2013		

DESIGNED BY: Curtis Steiner	DATE: 08/22/2013	SCALE: AS SHOWN	DRAWING CODE: FALL DRAWINGS CRCS
DRAWN BY: Derek Richardson			
CHECKED BY: CURTIS STEINER, SET NCE/TT #162672			
PROJECT ENGINEER: Integral Design Associates INC.			

CENTER FOR SCIENCE AND MATHEMATICS  
CALIFORNIA STATE POLYTECHNIC UNIVERSITY  
SAN LUIS OBISPO, CA  
CSFM #18-40-03-0001



FIRE ALARM THIRD FLOOR WEST  
SCALE 1/8" = 1'0"

SYMBOL LEGEND			
COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #
29	MANUAL PULL STATION	NBG-12LX	7150-0028:0199
73	STROBE ONLY	SW	7320-1653:201
153	SPEAKER/STROBE	SPWS	7320-1653:201
6	SPEAKER ONLY	SPW	7320-1653:201
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653:201
0	HEAT DETECTOR	FST-851	7270-0028:196
18	SMOKE DETECTOR	FSP-851	7272-0028:206
64	SMOKE DETECTOR - DUCT	DNR	3242-1653:209
23	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728:0121
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-90	7260-1728:0121
1	FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028:0243
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028:248
5	FIRE ALARM TERMINAL CABINET	N/A	N/A
32	END OF LINE RESISTOR	N/A	N/A
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028:209
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS
19	ADDRESSABLE MODULE	FM-1	7300-0028:0219
9	RELAY MODULE	FRM-1	7300-0028:219
16	WATER FLOW SWITCH	N/A	BY OTHERS
22	VALVE TAMPER SWITCH	N/A	BY OTHERS
21	DUAL MONITOR MODULE	FDM-1	7300-0028:0219
64	DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028:0219
12	FIRE FIGHTERS PHONE JACKS	FTM-1	7300-1652:0182
4	DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028:223 7170-0028:224
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028:0219
1	TEN-INPUT MONITOR MODULE	XP10-M	7300-0028:0219

WIRING LEGEND			
LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4 TS	ANNUNCIATOR	WEST PENN 993
F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX		
1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0



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Toll Free: 888-660-0001 DBI FAX:  
805-781-2037  
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Revisions

REVIEW COMMENTS	DATE	SYMBOL	DESCRIPTION	DATE	APPROV.
6/14/2011					
5/18/2012					
4/17/2012					
8/20/2012					
1/15/2013					
4/3/2013					
8/23/2013					

DATE: 08/22/2013

SCALE:

DRAWING CODE: FA ALL DRAWINGS CPFS

DESIGNED BY:  
Curtis Streever

DRAWN BY:  
Derek Richardson

CHECKED BY:  
Curtis Streever  
INCE 11/1/2012

PROJECT ENGINEER:  
Integral Design Associates INC.

CENTER FOR SCIENCE AND MATHEMATICS  
CALIFORNIA STATE POLYTECHNIC UNIVERSITY  
SAN LUIS OBISPO, CA

CSFM #18-40-03-0001

SHEET ID

FA 3.03E

SHEET 7 OF 15

SHEET NOTES

- 1 PROVIDE FIRE ALARM BEAM DETECTORS TRANSMITTER AND RECEIVER. INTERLOCK WITH SMOKE EVACUATION SYSTEM SUCH THAT WHEN BEAM DETECTOR IS ACTIVATED, SMOKE EVACUATION SYSTEM IS ACTIVATED. REFER TO DETAIL 4 & 5/FA5.0.
- 2 ACTIVATION OF A MANUAL PULL STATION, BEAM DETECTOR OR SPRINKLER WATER FLOW WITHIN THE ATRIUM SHALL ACTIVATE ATRIUM SMOKE EVACUATION SYSTEM. SMOKE EVACUATION SYSTEM SHALL FUNCTION AS DIRECTED BY MECHANICAL DOCUMENTS. REFER TO DETAIL 9/M5.05 FOR ADDITIONAL INFORMATION.
- 3 ACTIVATION OF AN ALARM ANYWHERE WITHIN THE BUILDING SHALL SHUT DOWN ALL AIR HANDLING UNITS.
- 4 ACTIVATION OF THE ATRIUM SMOKE CONTROL SYSTEM SHALL OPEN ALL ATRIUM DOORS WITH MOTORIZED DOOR OPERATORS.

SYMBOL LEGEND

COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #
31	MANUAL PULL STATION	NBG-12LX	7150-0028-0199
73	STROBE ONLY	SW	7320-1653-201
165	SPEAKER/STROBE	SPWS	7320-1653-201
6	SPEAKER ONLY	SPW	7320-1653-201
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653-201
0	HEAT DETECTOR	FST-851	7270-0028-196
18	SMOKE DETECTOR	FSP-851	7272-0028-206
64	SMOKE DETECTOR - DUCT	DNR	3242-1653-209
23	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728-0121
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-90	7260-1728-0121
1	FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028-0243
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028-248
4	FIRE ALARM TERMINAL CABINET	N/A	N/A
32	END OF LINE RESISTOR	N/A	N/A
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028-209
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	ADDRESSABLE MODULE	FMM-1	7300-0028-0219
12	RELAY MODULE	FRM-1	7300-0028-219
16	WATER FLOW SWITCH	N/A	BY OTHERS
10	VALVE TAMPER SWITCH	N/A	BY OTHERS
21	DUAL MONITOR MODULE	FDM-1	7300-0028-0219
64	DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028-0219
12	FIRE FIGHTERS PHONE JACKS	FTM-1	7300-1652-0182
4	DIGITAL AUDIO AMPLIFIERS	DA2	7170-0028-223 7170-0028-224
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028-0219
1	TEN-INPUT MONITOR MODULE	XP10-M	7300-0028-0219

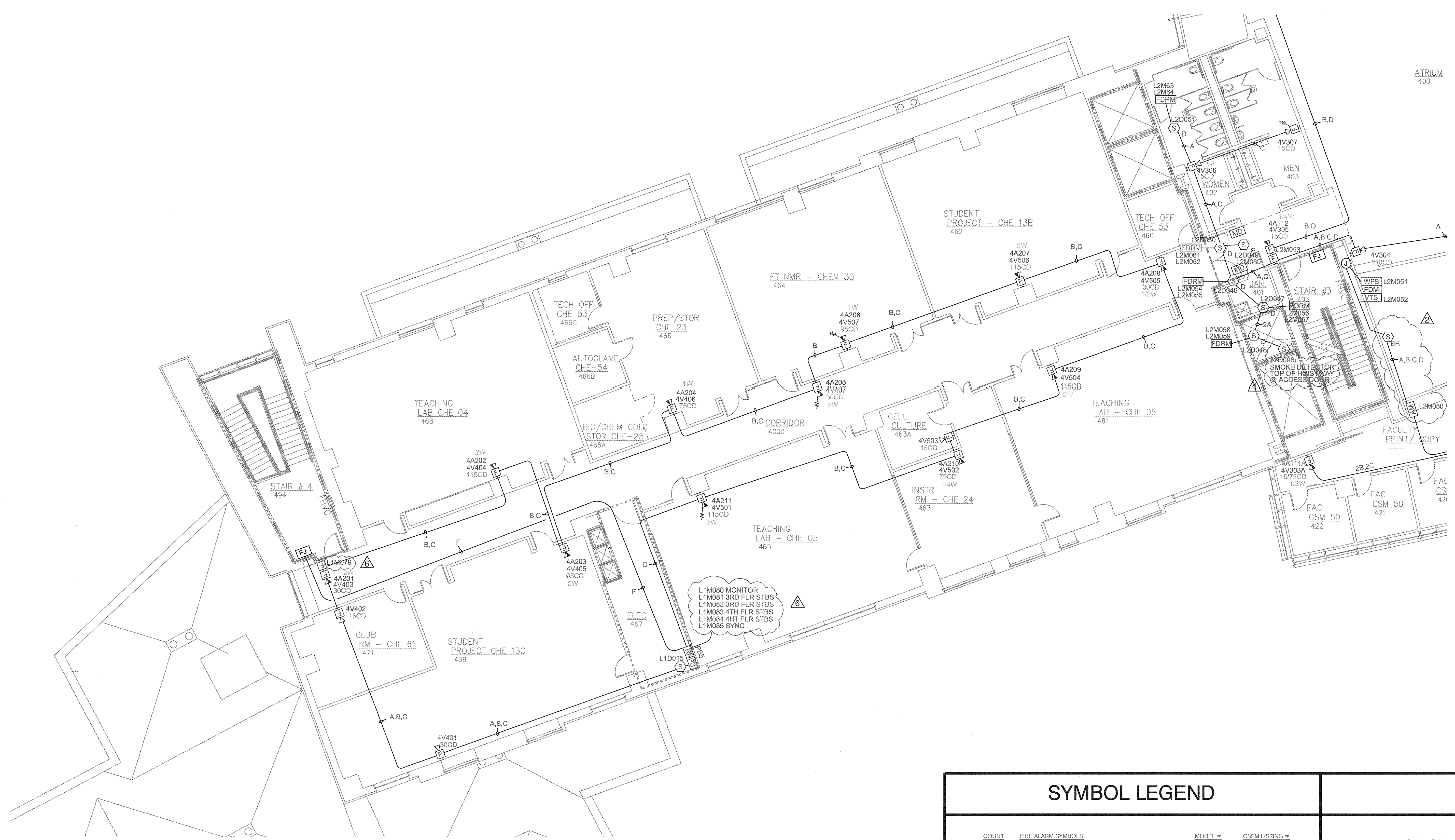
WIRING LEGEND

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4 TS	ANNUNCIATOR	WEST PENN 993
F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX

1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0





FIRE ALARM FOURTH FLOOR WEST  
SCALE 1/8" = 1'0"

SYMBOL LEGEND				WIRING LEGEND			
COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #	LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
31	MANUAL PULL STATION	NBG-12LX	7150-0028:0199	A	16/2 UTP	SLO	WEST PENN D990
73	STROBE ONLY	SW	7320-1653:201	B	16/2 TSP	SPEAKER	WEST PENN D991
165	SPEAKER/STROBE	SPWS	7320-1653:201	C	14	NAC VISUAL	THHN
6	SPEAKER ONLY	SPW	7320-1653:201	D	14	24 VDC	THHN
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653:201	E	16/4 TS	ANNUNCIATOR	WEST PENN 993
0	HEAT DETECTOR	FST-851	7270-0028:196	F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995
18	SMOKE DETECTOR	FSP-851	7272-0028:206				
64	SMOKE DETECTOR - DUCT	DNR	3242-1653:209				
23	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7280-1728:0121				
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-90	7280-1728:0121				
1	FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028:0243				
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028:248				
4	FIRE ALARM TERMINAL CABINET	N/A	N/A				
32	END OF LINE RESISTOR	N/A	N/A				
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028:209				
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS				
21	ADDRESSABLE MODULE	FMM-1	7300-0028:0219				
12	RELAY MODULE	FRM-1	7300-0028:219				
16	WATER FLOW SWITCH	N/A	BY OTHERS				
10	VALVE TAMPER SWITCH	N/A	BY OTHERS				
21	DUAL MONITOR MODULE	FDM-1	7300-0028:0219				
64	DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028:0219				
12	FIRE FIGHTERS PHONE JACKS	FTM-1	7300-1652:0182				
4	DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028:223 7170-0028:224				
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028:0219				
1	TEN-INPUT MONITOR MODULE	XP10-M	7300-0028:0219				

DRAWING INDEX			
1	COVER SHEET	FA 0.0	
2	RISER DIAGRAM	FA 1.0	
3	FIRST FLOOR WEST	FA 3.01W	
4	SECOND FLOOR EAST	FA 3.02E	
5	SECOND FLOOR WEST	FA 3.02W	
6	THIRD FLOOR EAST	FA 3.03E	
7	THIRD FLOOR WEST	FA 3.03W	
8	FOURTH FLOOR EAST	FA 3.04E	
9	FOURTH FLOOR WEST	FA 3.04W	
10	FIFTH FLOOR EAST	FA 3.05E	
11	FIFTH FLOOR WEST	FA 3.05W	
12	SIXTH FLOOR EAST	FA 3.06E	
13	SEVENTH FLOOR EAST	FA 3.07E	
14	CALCULATIONS	FA 4.0	
15	DETAILS	FA 5.0	

Revisions		DATE	DESCRIPTION	APPROVED
REVIEW COMMENTS	8/14/2011			
CBP # 0951 & F1 99	4/11/2012			
SFM REVIEW COMMENTS	8/20/2012			
CSB # 92	1/15/2013			
FA & SMOKE CONTROL SFM COMMENTS	4/23/2013			
AS-BUILT DRAWINGS	8/23/2013			

DESIGNED BY: Curtis Streever	DATE: 08/23/2013		
DRAWN BY: Derek Richardson	SCALE:		
CHECKED BY: CURTIS STREEVER NICET IV #10272	DRAWING CODE: FALL DRAWINGS CPCS		
PROJECT ENGINEER: Integral Design Associates INC.			

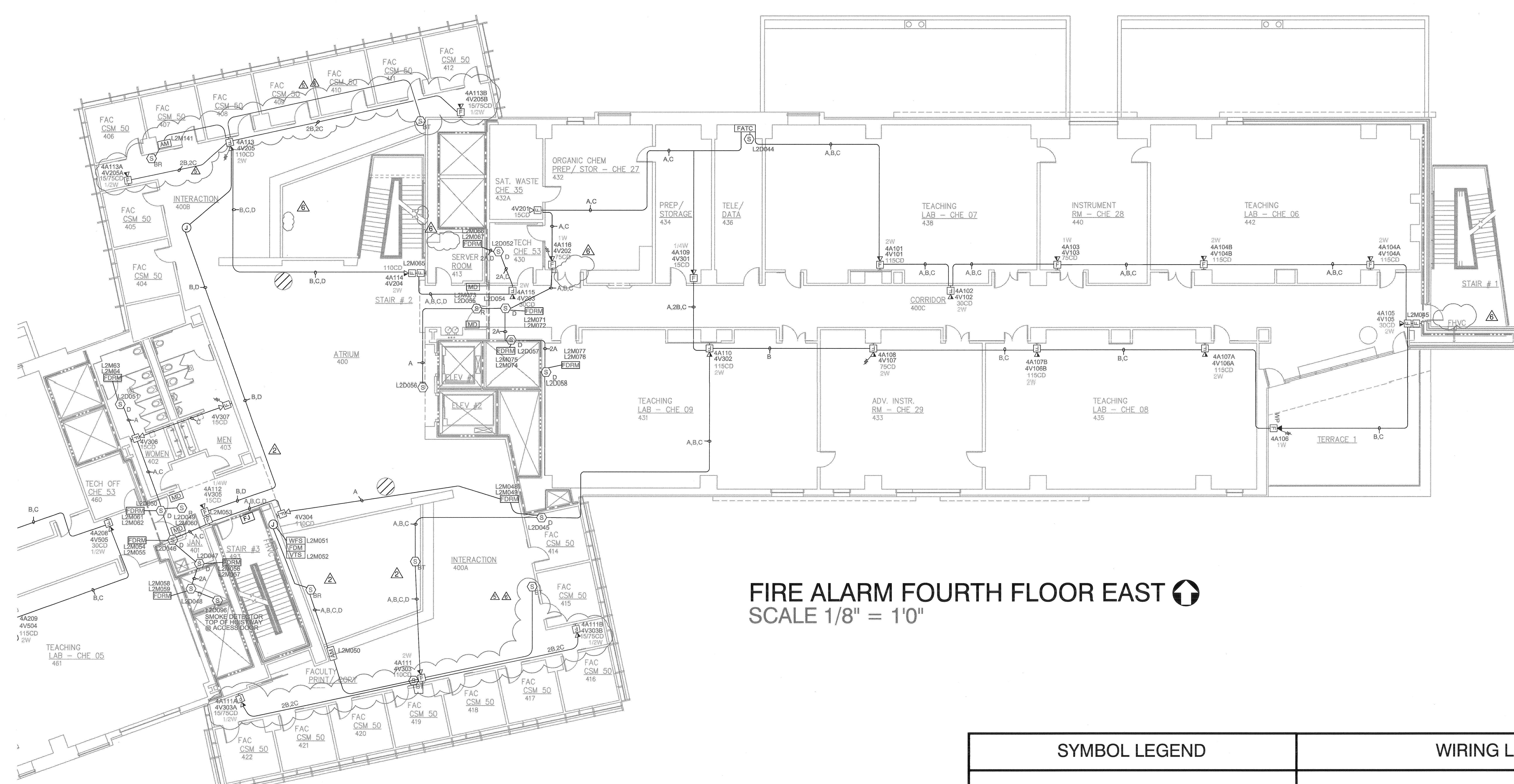
CENTER FOR SCIENCE AND MATHEMATICS  
CALIFORNIA STATE POLYTECHNIC UNIVERSITY  
SAN LUIS OBISPO, CA  
CSFM #18-40-03-0001



Revisions		REVIEW COMMENTS	DATE	SYMBOL	DESCRIPTION	APPROVAL
6/14/2011	1	REVIEW COMMENTS	6/14/2011			
5/18/2012	2	CRB # 083.1 & 99	5/18/2012			
4/11/2012	3	SPM REVIEW COMMENTS	4/11/2012			
8/20/2012	4	CRB 83.2	8/20/2012			
1/15/2013	5	FA 4 SMOKE CONTROL SPM COMMENTS	1/15/2013			
4/20/2013	6	AS-BUILT DRAWINGS	4/20/2013			
8/23/2013	7		8/23/2013			

DESIGNED BY: Curtis Streever	DATE: 08/23/2013	SCALE: AS SHOWN	DRAWING CODE: FA 4 ALL DRAWINGS CPFS
DRAWN BY: Derek Richardson			
CHECKED BY: Curtis Streever INCH 1/16" = 1/8"			
PROJECT ENGINEER: Integral Design Associates INC.			

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SAN LUIS OBISPO, CA  
CSFM #18-40-03-0001



FIRE ALARM FOURTH FLOOR EAST  
SCALE 1/8" = 1'0"

SHEET NOTES

1. PROVIDE FIRE ALARM BEAM DETECTORS TRANSMITTER AND RECEIVER. INTERLOCK WITH SMOKE EVACUATION SYSTEM SUCH THAT WHEN BEAM DETECTOR IS ACTIVATED, SMOKE EVACUATION SYSTEM IS ACTIVATED. REFER TO DETAIL 4 & 5/FA5.0.
2. ACTIVATION OF A MANUAL PULL STATION, BEAM DETECTOR OR SPRINKLER WATER FLOW WITHIN THE ATRIUM SHALL ACTIVATE ATRIUM SMOKE EVACUATION SYSTEM. SMOKE EVACUATION SYSTEM SHALL FUNCTION AS DIRECTED BY MECHANICAL DOCUMENTS. REFER TO DETAIL 9/M5.05 FOR ADDITIONAL INFORMATION.
3. ACTIVATION OF AN ALARM ANYWHERE WITHIN THE BUILDING SHALL SHUT DOWN ALL AIR HANDLING UNITS.
4. ACTIVATION OF THE ATRIUM SMOKE CONTROL SYSTEM SHALL OPEN ALL ATRIUM DOORS WITH MOTORIZED DOOR OPERATORS.

SYMBOL LEGEND				WIRING LEGEND			
COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #	LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
31	MANUAL PULL STATION	NBG-12LX	7150-0028-0199	A	16/2 UTP	SLC	WEST PENN D990
73	STROBE ONLY	SW	7320-1653-201	B	16/2 TSP	SPEAKER	WEST PENN D991
165	SPEAKER/STROBE	SPWS	7320-1653-201	C	14	NAC VISUAL	THHN
6	SPEAKER ONLY	SPW	7320-1653-201	D	14	24 VDC	THHN
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653-201	E	16/4 TS	ANNUNCIATOR	WEST PENN 993
0	HEAT DETECTOR	FST-851	7270-0028-196	F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995
18	SMOKE DETECTOR	FSP-851	7272-0028-206				
64	SMOKE DETECTOR - DUCT	DNR	8242-1653-209				
23	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7280-1728-0121				
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-90	7280-1728-0121				
1	FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028-0243				
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028-248				
4	FIRE ALARM TERMINAL CABINET	N/A	N/A				
32	END OF LINE RESISTOR	N/A	N/A				
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028-209				
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS				
21	ADDRESSABLE MODULE	FMM-1	7300-0028-0219				
12	RELAY MODULE	FRM-1	7300-0028-219				
16	WATER FLOW SWITCH	N/A	BY OTHERS				
10	VALVE TAMPER SWITCH	N/A	BY OTHERS				
21	DUAL MONITOR MODULE	FDM-1	7300-0028-0219				
64	DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028-0219				
12	FIRE FIGHTERS PHONE JACKS	FTM-1	7300-1652-0182				
4	DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028-223				
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028-0219				
1	TEN-INPUT MONITOR MODULE	XP10-M	7300-0028-0219				

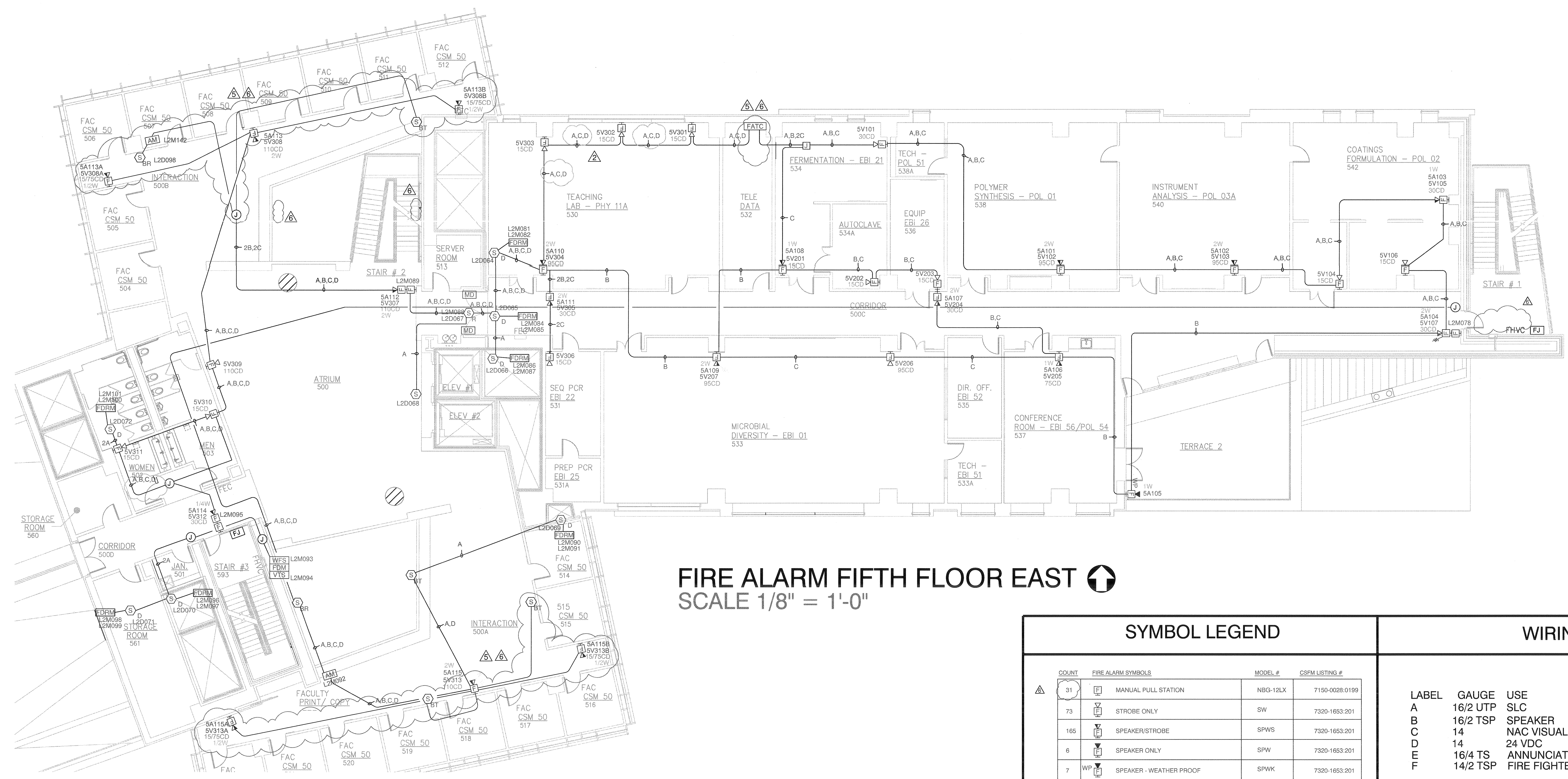
DRAWING INDEX			
1	COVER SHEET	FA 0.0	
2	RISER DIAGRAM	FA 1.0	
3	FIRST FLOOR WEST	FA 3.01W	
4	SECOND FLOOR EAST	FA 3.02E	
5	SECOND FLOOR WEST	FA 3.02W	
6	THIRD FLOOR EAST	FA 3.03E	
7	THIRD FLOOR WEST	FA 3.03W	
8	FOURTH FLOOR EAST	FA 3.04E	
9	FOURTH FLOOR WEST	FA 3.04W	
10	FIFTH FLOOR EAST	FA 3.05E	
11	FIFTH FLOOR WEST	FA 3.05W	
12	SIXTH FLOOR EAST	FA 3.06E	
13	SEVENTH FLOOR EAST	FA 3.07E	
14	CALCULATIONS	FA 4.0	
15	DETAILS	FA 5.0	



Revisions		DATE	DESCRIPTION	APPR.
1	REVIEW COMMENTS	8/14/2011		
2	CBF # 0831 & F1 B9	5/18/2012		
3	SPM REVIEW COMMENTS	8/20/2012		
4	CBF # 93.2	1/15/2013		
5	FA & SMOKE CONTROL SPM COMMENTS	4/2/2013		
6	AS-BUILT DRAWINGS	8/23/2013		

DESIGNED BY: Curtis Streever	DATE: 08/23/2013	SCALE:	DRAWING CODE: FA ALL DRAWINGS CPCS
DRAWN BY: Derek Richardson			
CHECKED BY: CURTIS STREEVER, SET INSET IV #102072			
PROJECT ENGINEER: Integral Design Associates INC.			

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CALIFORNIA STATE POLYTECHNIC UNIVERSITY  
SAN LUIS OBISPO, CA  
CSFM #18-40-03-0001



FIRE ALARM FIFTH FLOOR EAST  
SCALE 1/8" = 1'-0"

SHEET NOTES

- PROVIDE FIRE ALARM BEAM DETECTORS TRANSMITTER AND RECEIVER. INTERLOCK WITH SMOKE EVACUATION SYSTEM SUCH THAT WHEN BEAM DETECTOR IS ACTIVATED, SMOKE EVACUATION SYSTEM IS ACTIVATED. REFER TO DETAIL 4 & 5/FA5.0.
- ACTIVATION OF A MANUAL PULL STATION, BEAM DETECTOR OR SPRINKLER WATER FLOW WITHIN THE ATRIUM SHALL ACTIVATE ATRIUM SMOKE EVACUATION SYSTEM. SMOKE EVACUATION SYSTEM SHALL FUNCTION AS DIRECTED BY MECHANICAL DOCUMENTS. REFER TO DETAIL 9/M5.05 FOR ADDITIONAL INFORMATION.
- ACTIVATION OF AN ALARM ANYWHERE WITHIN THE BUILDING SHALL SHUT DOWN ALL AIR HANDLING UNITS.
- ACTIVATION OF THE ATRIUM SMOKE CONTROL SYSTEM SHALL OPEN ALL ATRIUM DOORS WITH MOTORIZED DOOR OPERATORS.

SYMBOL LEGEND

COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #
31	MANUAL PULL STATION	NBG-12LX	7150-0028-0199
73	STROBE ONLY	SW	7320-1653-201
165	SPEAKER/STROBE	SPWS	7320-1653-201
6	SPEAKER ONLY	SPW	7320-1653-201
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653-201
0	HEAT DETECTOR	FST-851	7270-0028-196
18	SMOKE DETECTOR	FSP-851	7272-0028-206
64	SMOKE DETECTOR - DUCT	DNR	3242-1653-209
23	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7280-1728-0121
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-80	7260-1728-0121
1	FIRE ALARM CONTROL PANEL	NFS-640	7165-0028-0240
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028-248
4	FIRE ALARM TERMINAL CABINET	N/A	N/A
22	END OF LINE RESISTOR	N/A	N/A
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028-209
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	ADDRESSABLE MODULE	FRM-1	7300-0028-0219
12	RELAY MODULE	FRM-1	7300-0028-219
16	WATER FLOW SWITCH	N/A	BY OTHERS
10	VALVE TAMPER SWITCH	N/A	BY OTHERS
21	DUAL MONITOR MODULE	FRM-1	7300-0028-0219
64	DUAL RELAY / MONITOR MODULE	FRM-1	7300-0028-0219
12	FIRE FIGHTERS PHONE JACKS	FTM-1	7300-1652-0162
4	DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028-223 7170-0028-224
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028-0219
1	TEN-INPUT MONITOR MODULE	XP10-M	7300-0028-0219

WIRING LEGEND

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4 TS	ANNUNCIATOR	WEST PENN 993
F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX



























1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0





- 1 PROVIDE FIRE ALARM BEAM DETECTORS TRANSMITTER AND RECEIVER. INTERLOCK WITH SMOKE EVACUATION SYSTEM SUCH THAT WHEN BEAM DETECTOR IS ACTIVATED, SMOKE EVACUATION SYSTEM IS ACTIVATED. REFER TO DETAIL 4 & 5/FA5.0.
- 2 ACTIVATION OF A MANUAL PULL STATION, BEAM DETECTOR OR SPRINKLER WATER FLOW WITHIN THE ATRIUM SHALL ACTIVATE ATRIUM SMOKE EVACUATION SYSTEM. SMOKE EVACUATION SYSTEM SHALL FUNCTION AS DIRECTED BY MECHANICAL DOCUMENTS. REFER TO DETAIL 9/MS.05 FOR ADDITIONAL INFORMATION.
- 3 ACTIVATION OF AN ALARM ANYWHERE WITHIN THE BUILDING SHALL SHUT DOWN ALL AIR HANDLING UNITS.
- 4 ACTIVATION OF THE ATRIUM SMOKE CONTROL SYSTEM SHALL OPEN ALL ATRIUM DOORS WITH MOTORIZED DOOR OPERATORS.

# S Y M B O L   L E G E N D W I R I N G   L E G E N D

COUNT	FIRE ALARM SYMBOLS	MODEL #	CSPM LISTING #
31	 MANUAL PULL STATION	NBG-12LX	7150-0028:0199
73	 STROBE ONLY	SW	7320-1653:201
166	 SPEAKER/STROBE	SPWS	7320-1653:201
6	 SPEAKER ONLY	SPW	7320-1653:201
7	 WP SPEAKER - WEATHER PROOF	SPWK	7320-1653:201
9	 HEAT DETECTOR	PST-851	7270-0028:196
18	 SMOKE DETECTOR	PSP 851	7272-0028:206
64	 SMOKE DETECTOR - DUCT	DNR	3242-1653:209
23	 BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728:0121
15	 BR BEAM SMOKE DETECTOR- RECEIVER	OSI-90	7260-1728:0121
1	 FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028:0243
5	 REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028:248
4	 FIRE ALARM TERMINAL CABINET	N/A	N/A
32	 END OF LINE RESISTOR	N/A	N/A
2	 REMOTE ANNUNCIATOR	FDU-80	7120-0028:309
8	 MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	 ADDRESSABLE MODULE	FRM-1	7300-0028:0219
12	 RELAY MODULE	FRM-1	7300-0028:219
16	 WATER FLOW SWITCH	N/A	BY OTHERS
10	 VALVE TAMPER SWITCH	N/A	BY OTHERS
21	 DUAL MONITOR MODULE	FDM-1	7300-0028:0219
64	 DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028:0219
12	 FIRE FIGHTER'S PHONE JACKS	FTM-1	7300-1652:0162
4	 DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028:223 7170-0028:224
1	 SIX RELAY CONTROL MODULE	XP6-R	7300-0028:0219
1	 TEN-INPUT MONITOR MODULE	XP10-M	7300-0028:0219

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4 TS	ANNUNCIATOR	WEST PENN 993
	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

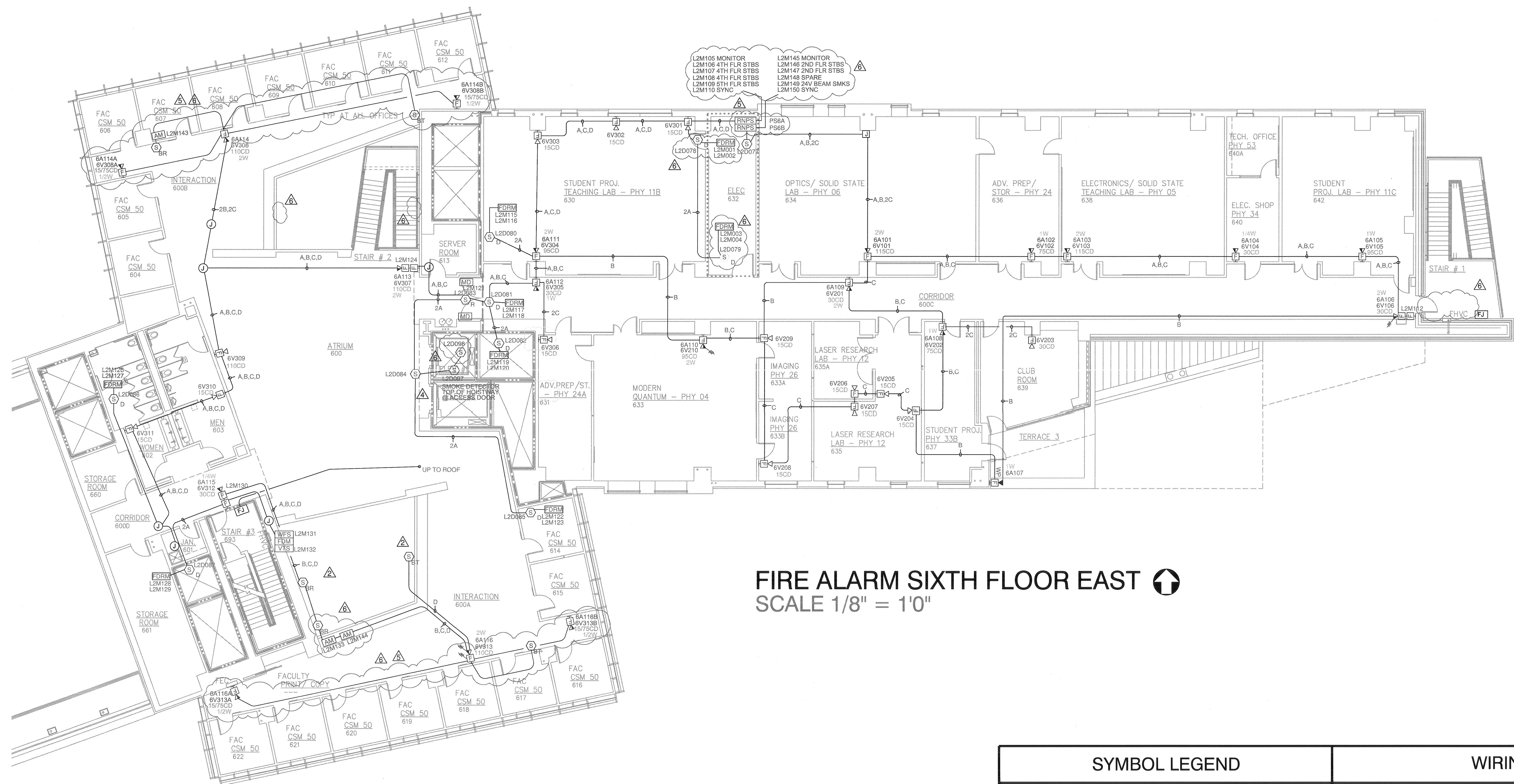
## DRAWING INDEX

1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0



Revisions					
1	REVIEW COMMENTS	8/14/2011	DATE	DESCRIPTION	APPR.
2	CRB # 093.1 & F1 99	9/18/2012			
3	SFM REVIEW COMMENTS	8/20/2012			
4	CRB # 832	11/5/2013			
5	FA & SMOKE CONTROL SFM COMMENTS	4/29/2013			
6	AS-BUILT DRAWINGS	8/23/2013			

DESIGNED BY: Curtis Streeter	DATE: 08/23/2013		
DRAWN BY: Derek Richardson	SCALE: AS SHOWN		
CHECKED BY: CURTIS STREETER, SET NICET IV #102672	DRAWING CODE: FA-ALL DRAWINGS CPCS		
PROJECT ENGINEER: Integral Design Associates INC.			



FIRE ALARM SIXTH FLOOR EAST  
SCALE 1/8" = 1'0"

SHEET NOTES

- 1 PROVIDE FIRE ALARM BEAM DETECTORS TRANSMITTER AND RECEIVER. INTERLOCK WITH SMOKE EVACUATION SYSTEM SUCH THAT WHEN BEAM DETECTOR IS ACTIVATED, SMOKE EVACUATION SYSTEM IS ACTIVATED. REFER TO DETAIL 4 & 5/FA5.0.
- 2 ACTIVATION OF A MANUAL PULL STATION, BEAM DETECTOR OR SPRINKLER WATER FLOW WITHIN THE ATRIUM SHALL ACTIVATE ATRIUM SMOKE EVACUATION SYSTEM. SMOKE EVACUATION SYSTEM SHALL FUNCTION AS DIRECTED BY MECHANICAL DOCUMENTS. REFER TO DETAIL 9/M5.05 FOR ADDITIONAL INFORMATION.
- 3 ACTIVATION OF AN ALARM ANYWHERE WITHIN THE BUILDING SHALL SHUT DOWN ALL AIR HANDLING UNITS.
- 4 ACTIVATION OF THE ATRIUM SMOKE CONTROL SYSTEM SHALL OPEN ALL ATRIUM DOORS WITH MOTORIZED DOOR OPERATORS.

SYMBOL LEGEND

COUNT	FIRE ALARM SYMBOLS	MODEL #	CSFM LISTING #
31	MANUAL PULL STATION	NBG-12LX	7150-0028-0199
73	STROBE ONLY	SW	7320-1653-201
165	SPEAKER/STROBE	SPWS	7320-1653-201
6	SPEAKER ONLY	SPW	7320-1653-201
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653-201
0	HEAT DETECTOR	FST-851	7270-0028-196
16	SMOKE DETECTOR	FSP-851	7272-0028-206
64	SMOKE DETECTOR - DUCT	DNR	3242-1653-206
25	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728-0121
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-90	7260-1728-0121
1	FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028-0243
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028-248
4	FIRE ALARM TERMINAL CABINET	N/A	N/A
32	END OF LINE RESISTOR	N/A	N/A
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028-209
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	ADDRESSABLE MODULE	FMM-1	7300-0028-0219
12	RELAY MODULE	FRM-1	7300-0028-219
16	WATER FLOW SWITCH	N/A	BY OTHERS
10	VALVE TAMPER SWITCH	N/A	BY OTHERS
21	DUAL MONITOR MODULE	FDM-1	7300-0028-0219
64	DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028-0219
12	FIRE FIGHTER'S PHONE JACKS	FTM-1	7300-1652-0182
4	DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028-223 7170-0028-224
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028-0219
1	YEN-INPUT MONITOR MODULE	XP10-M	7300-0028-0219

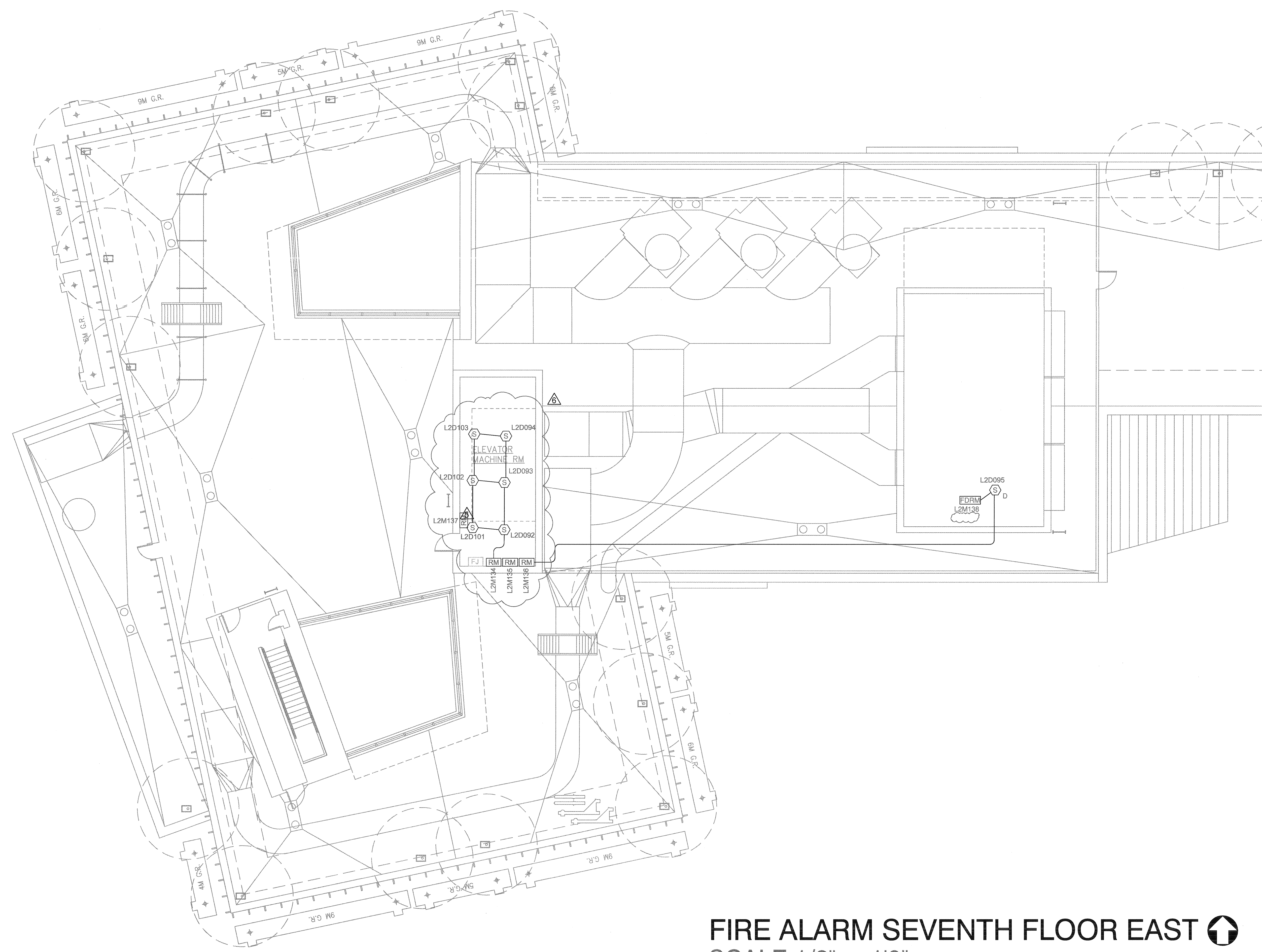
WIRING LEGEND

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
C	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
E	16/4 TS	ANNUNCIATOR	WEST PENN 993
F	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX

1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0





FIRE ALARM SEVENTH FLOOR EAST  
SCALE 1/8" = 1'0"

SYMBOL LEGEND

COUNT	FIRE ALARM SYMBOL	MODEL #	CSFM LISTING #
31	MANUAL PULL STATION	NBG-12LX	7150-0028-0199
73	STROBE ONLY	SW	7320-1653-201
165	SPEAKER/STROBE	SPWS	7320-1653-201
6	SPEAKER ONLY	SPW	7320-1653-201
7	SPEAKER - WEATHER PROOF	SPWK	7320-1653-201
0	HEAT DETECTOR	FST-851	7270-0028-196
18	SMOKE DETECTOR	FSP-B51	7272-0028-206
64	SMOKE DETECTOR - DUCT	DNR	3242-1653-209
23	BEAM SMOKE DETECTOR - TRANSMITTER	OSE-SPW	7260-1728-0121
15	BEAM SMOKE DETECTOR - RECEIVER	OSI-90	7260-1728-0121
1	FIRE ALARM CONTROL PANEL	NFS2-640	7165-0028-0243
5	REMOTE NOTIFICATION POWER SUPPLY	ACPS-610	7315-0028-248
4	FIRE ALARM TERMINAL CABINET	N/A	N/A
32	END OF LINE RESISTOR	N/A	N/A
2	REMOTE ANNUNCIATOR	FDU-80	7120-0028-209
8	MAGNETIC DOOR HOLDER	N/A	BY OTHERS
21	ADDRESSABLE MODULE	FMM-1	7300-0028-0219
12	RELAY MODULE	FRM-1	7300-0028-219
16	WATER FLOW SWITCH	N/A	BY OTHERS
10	VALVE TAMPER SWITCH	N/A	BY OTHERS
21	DUAL MONITOR MODULE	FDM-1	7300-0028-0219
64	DUAL RELAY / MONITOR MODULE	FDRM-1	7300-0028-0219
12	FIRE FIGHTERS PHONE JACKS	FTM-1	7300-1652-0182
4	DIGITAL AUDIO AMPLIFIERS	DAA2	7170-0028-223 7170-0028-224
1	SIX RELAY CONTROL MODULE	XP6-R	7300-0028-0219
1	TEN-INPUT MONITOR MODULE	XP10-M	7300-0028-0219

WIRING LEGEND

LABEL	GAUGE	USE	TYPE (OR EQUIVALENT)
A	16/2 UTP	SLC	WEST PENN D990
B	16/2 TSP	SPEAKER	WEST PENN D991
O	14	NAC VISUAL	THHN
D	14	24 VDC	THHN
T	16/4 TS	ANNUNCIATOR	WEST PENN 993
E	14/2 TSP	FIRE FIGHTERS PHONE	WEST PENN D995

DRAWING INDEX

1	COVER SHEET	FA 0.0
2	RISER DIAGRAM	FA 1.0
3	FIRST FLOOR WEST	FA 3.01W
4	SECOND FLOOR EAST	FA 3.02E
5	SECOND FLOOR WEST	FA 3.02W
6	THIRD FLOOR EAST	FA 3.03E
7	THIRD FLOOR WEST	FA 3.03W
8	FOURTH FLOOR EAST	FA 3.04E
9	FOURTH FLOOR WEST	FA 3.04W
10	FIFTH FLOOR EAST	FA 3.05E
11	FIFTH FLOOR WEST	FA 3.05W
12	SIXTH FLOOR EAST	FA 3.06E
13	SEVENTH FLOOR EAST	FA 3.07E
14	CALCULATIONS	FA 4.0
15	DETAILS	FA 5.0

Revisions	DATE	DESCRIPTION
REVIEW COMMENTS		
CRB #1051 & FI #9	8/20/2012	SPM REVIEW COMMENTS
CRB #32	1/15/2013	FA & SMOKE CONTROL SPM COMMENTS
AS-BUILT DRAWINGS	8/23/2013	AS-BUILT DRAWINGS

DESIGNED BY: Curtis Streeter	DATE: 08/23/2013	SCALE:	DRAWING CODE: FA ALL DRAWINGS CPFS
DRAWN BY: Derek Richardson			
CHECKED BY: CURTIS STREETER, SET NICET IV #102672			
PROJECT ENGINEER: Integral Design Associates, INC.			





## SPEAKER CALCULATIONS

DATE:	08/23/2013
SCALE:	
DRAWING CODE:	FA ALL DRAWINGS CPCFS

CURTIS S  
NICET IV #

**ENCE ANI  
POLYTEC**

CSFM #18-40-03-0001

**SHEET ID**

FA 4.0

SHEET 14 OF 15

[10.14-ling - 10d1 Condaters](#)    [10.10-lang Standard Condaters](#)  
Notes  
Why resistance is disabled in the calculations for two wires (Positive and Negative)  
The voltage calculated in the first device must not be lower than  
[the minimum current limit parameters specified in settings \(8 - rated operating voltage 20.92 VDC\)](#)

[10-10 Aug - Self-Constructors](#)   
 [12-12 Aug - Standard Constructors](#)  
[Notes](#)  
 (For convenience I doubled in the calculations for non-views (Positive and Negative)  
 the values obtained in the last lecture and will not be lower than  
[the minimum values found in the literature](#) (see [this](#) - related operating on page 20-21 of [this](#))

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# EAST

# CALCULUS

# ULATIONS

	11	FIFT
	12	SIXT
	13	SEV
	14	CAL
	15	DET

TH FLOOR WEST	FA 3.05W
TH FLOOR EAST	FA 3.06E
FIFTH FLOOR EAST	FA 3.07E
CULCATIONS	FA 4.0
TAILS	FA 5.0

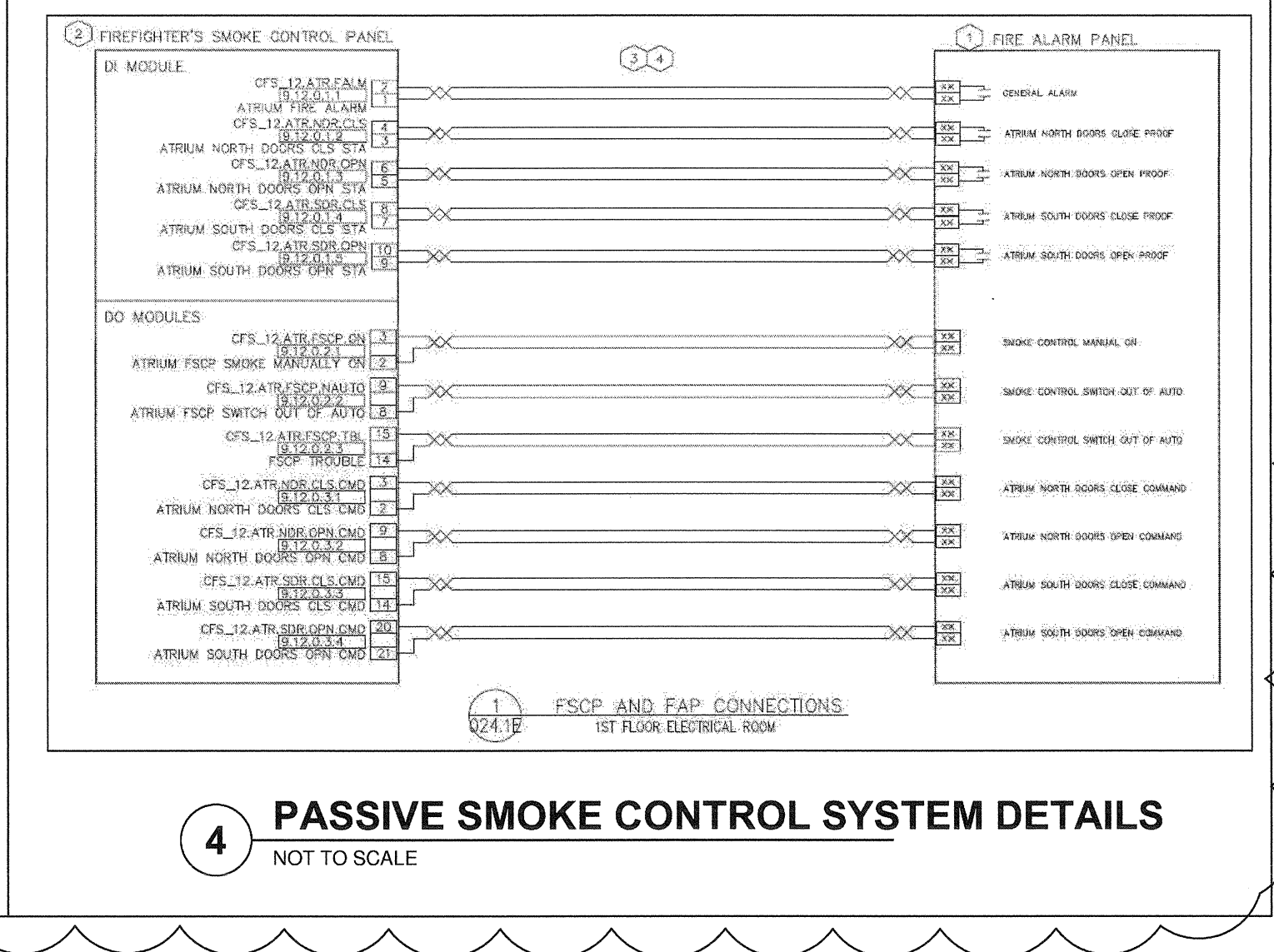
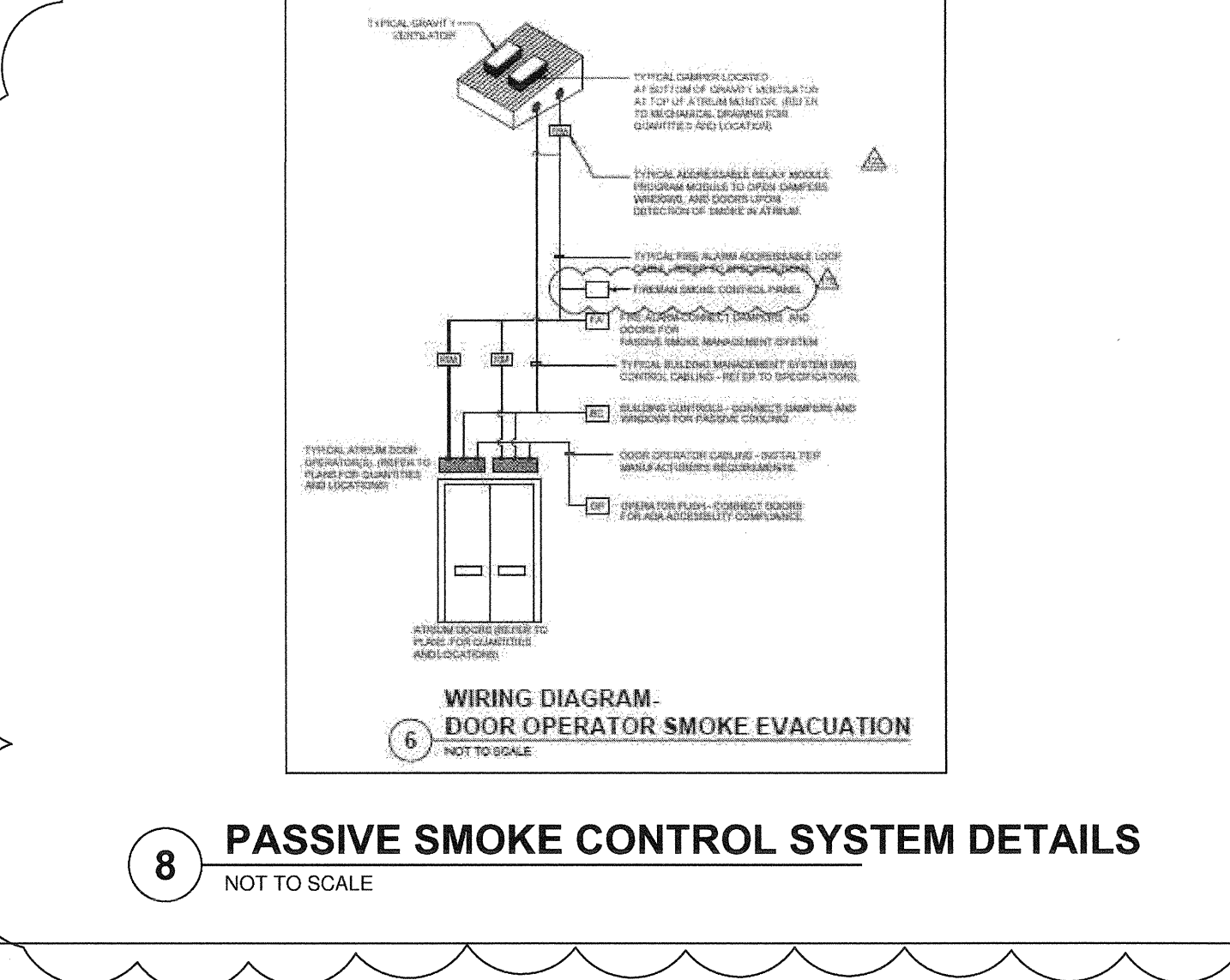
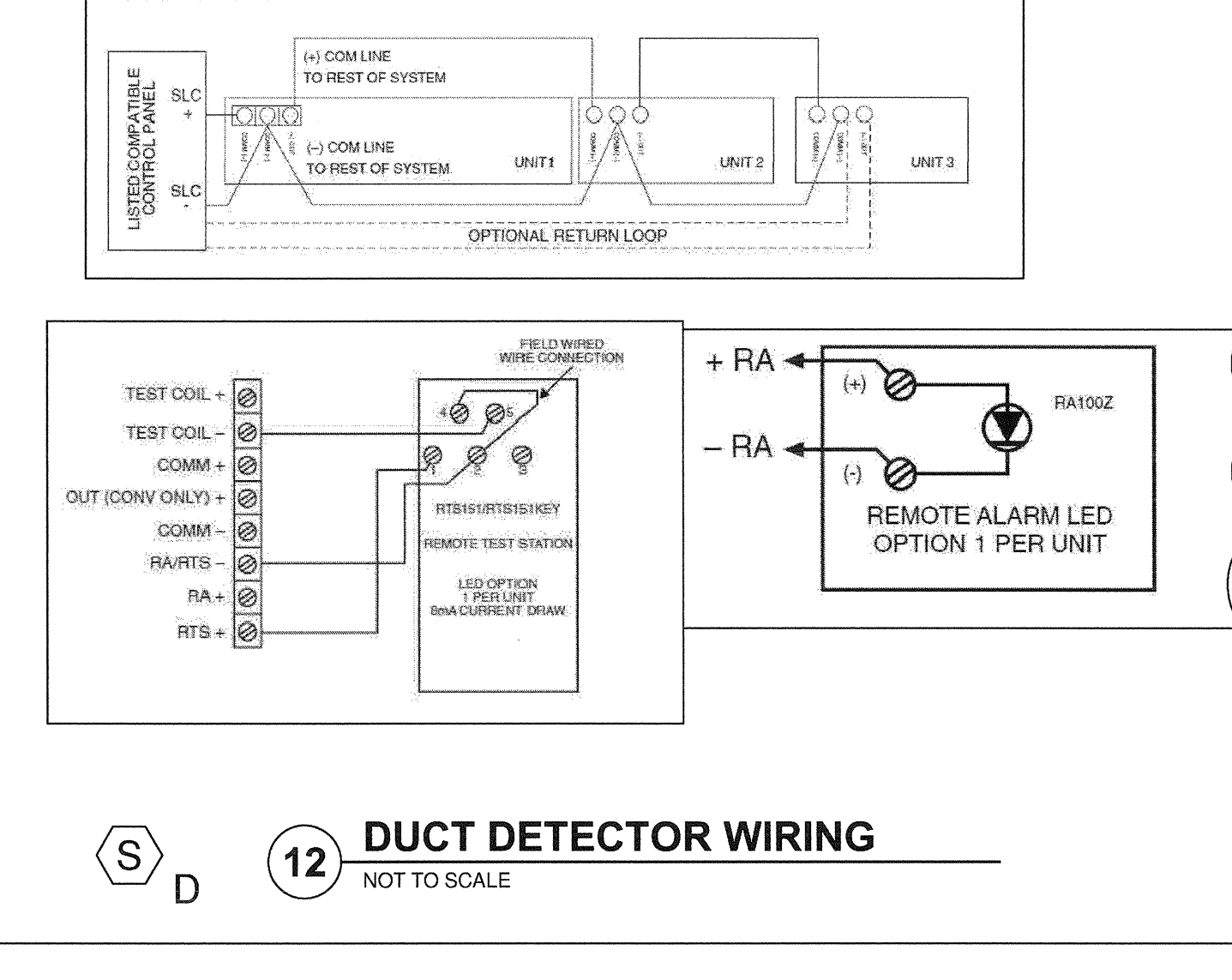
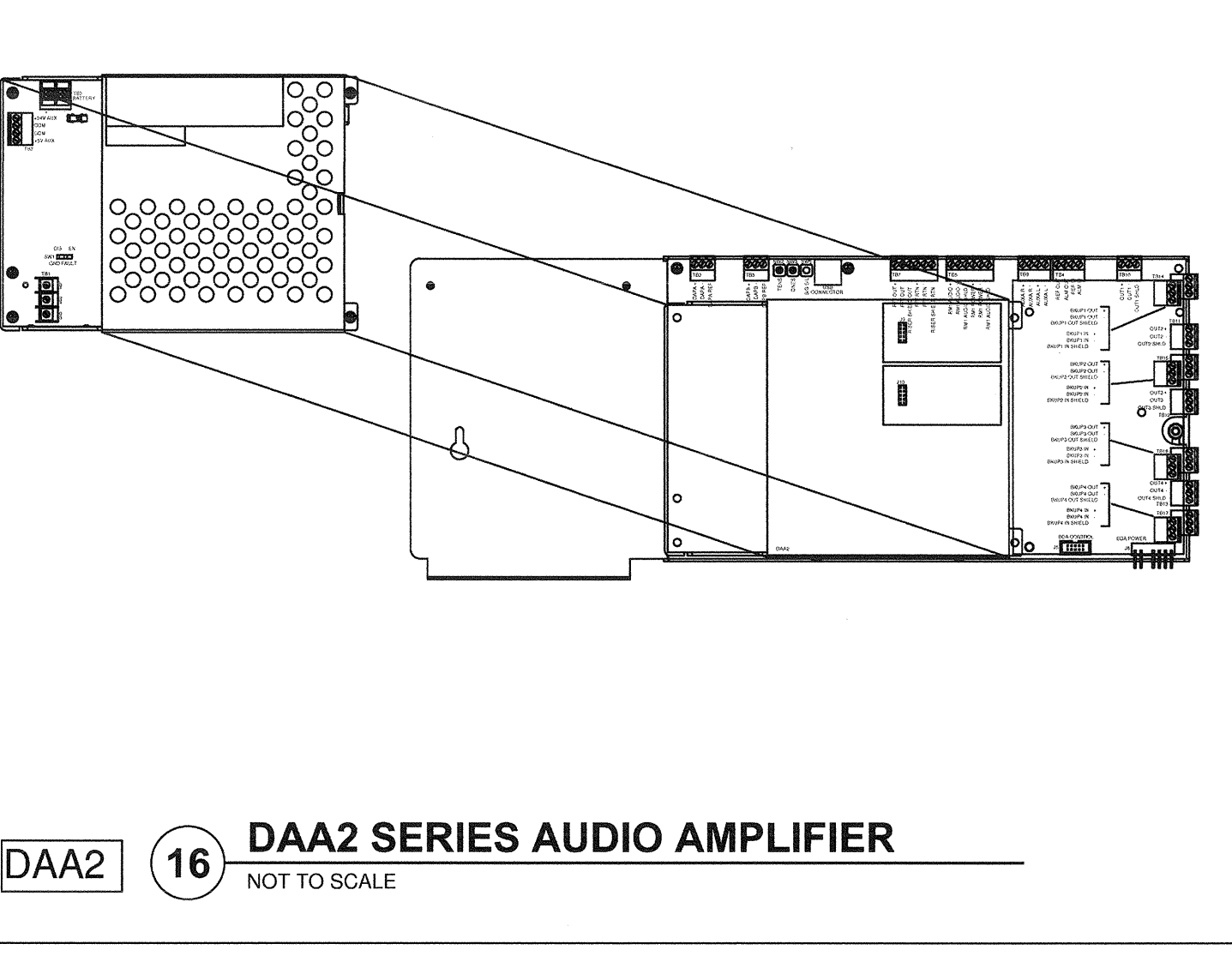
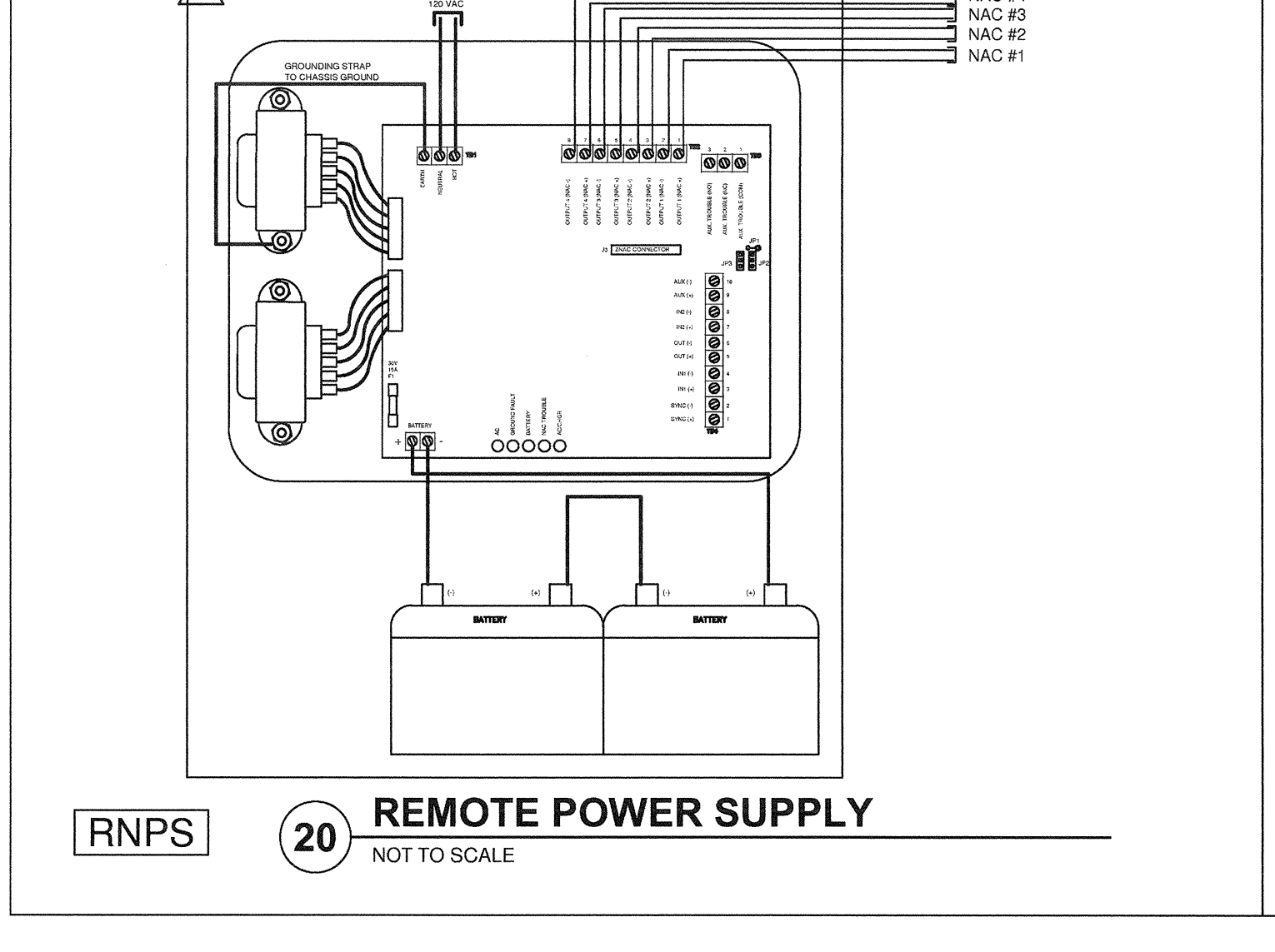
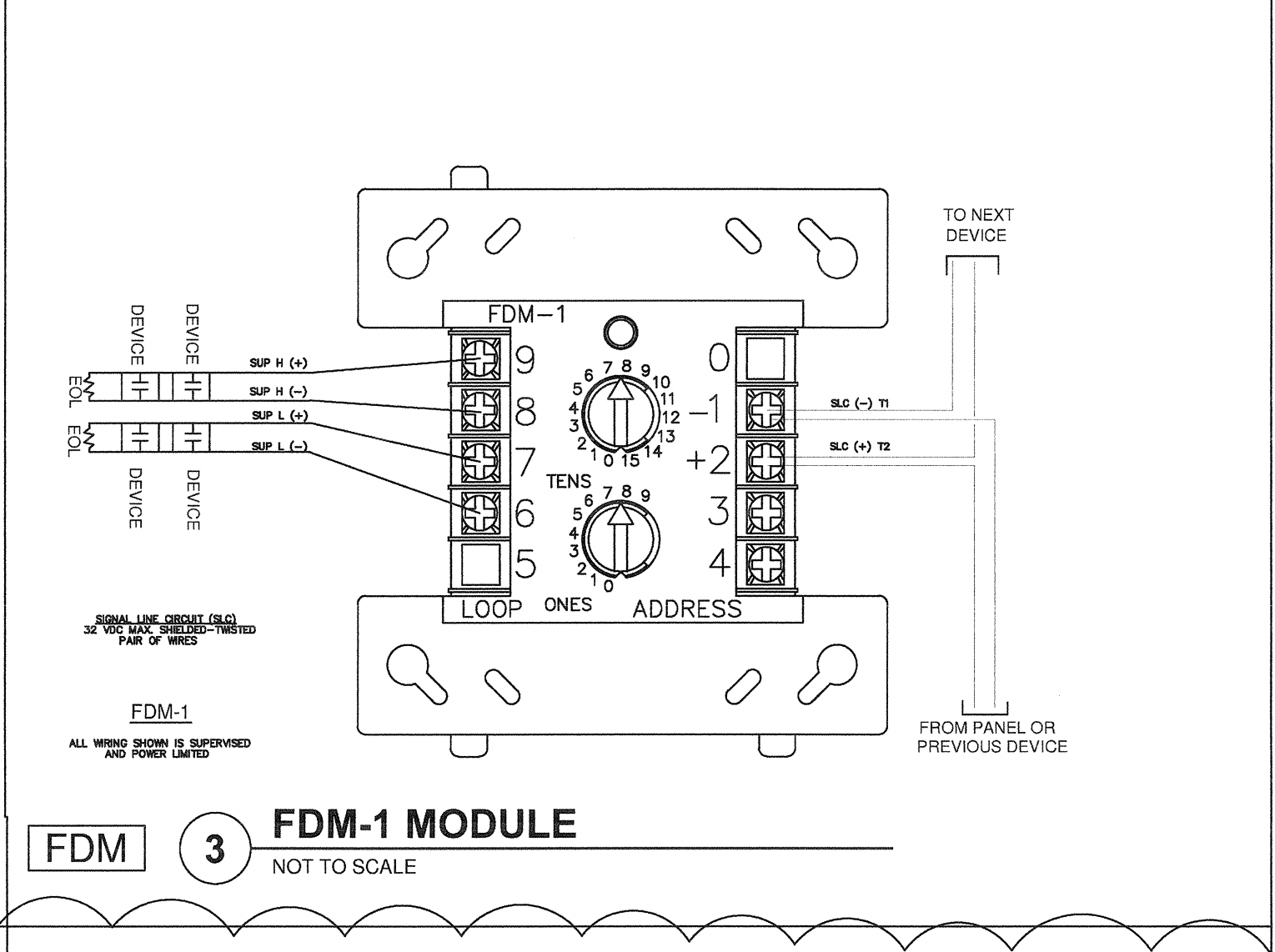
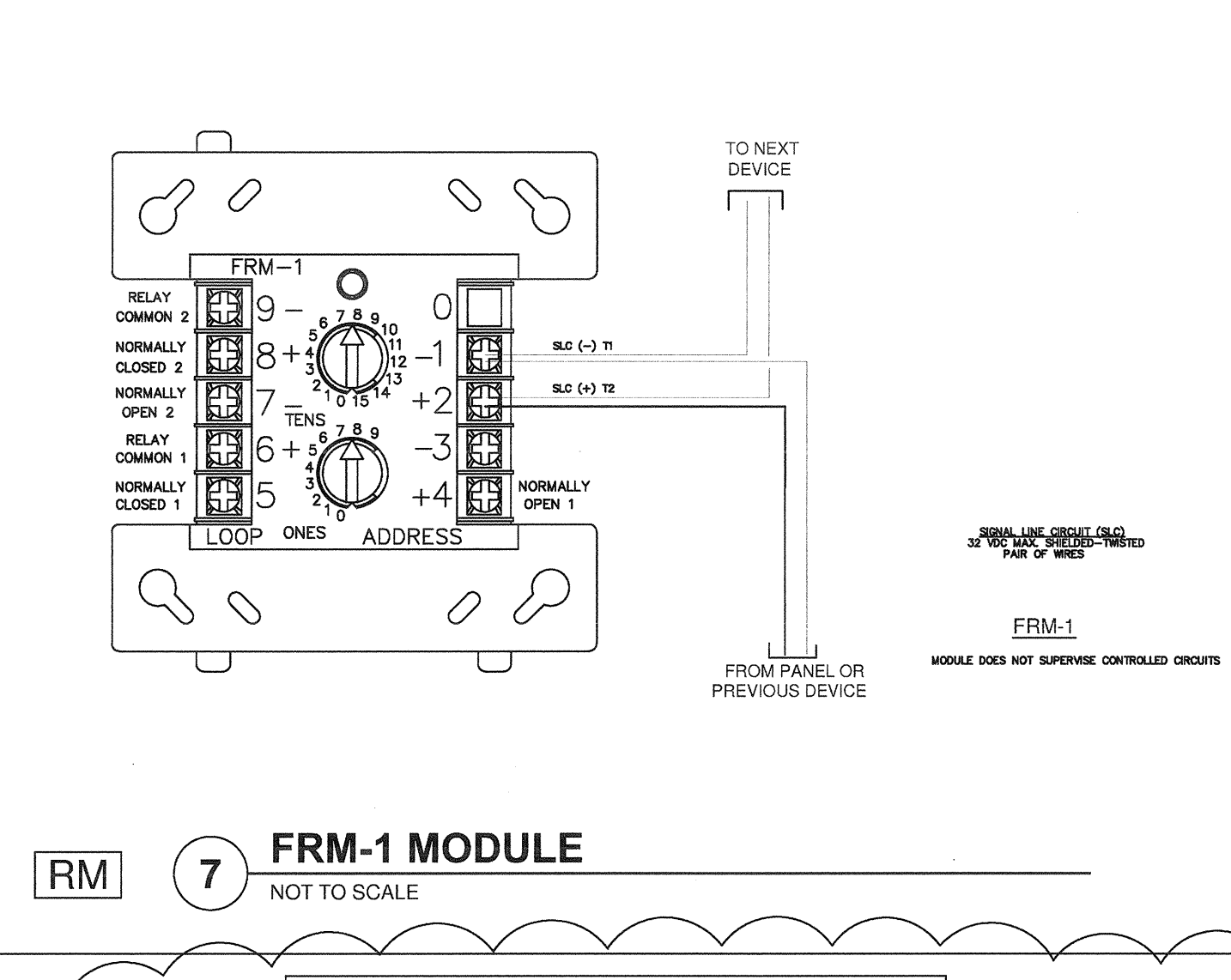
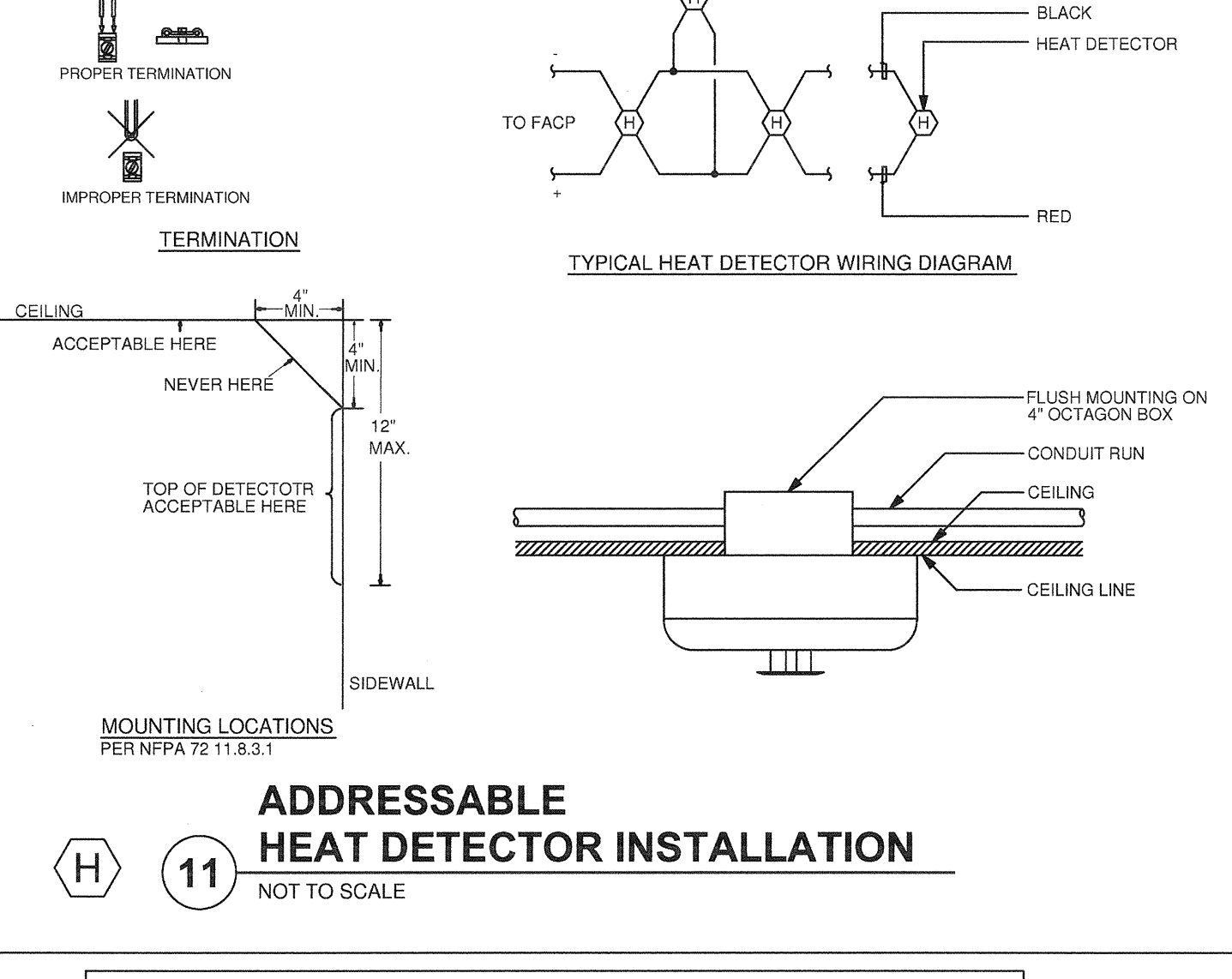
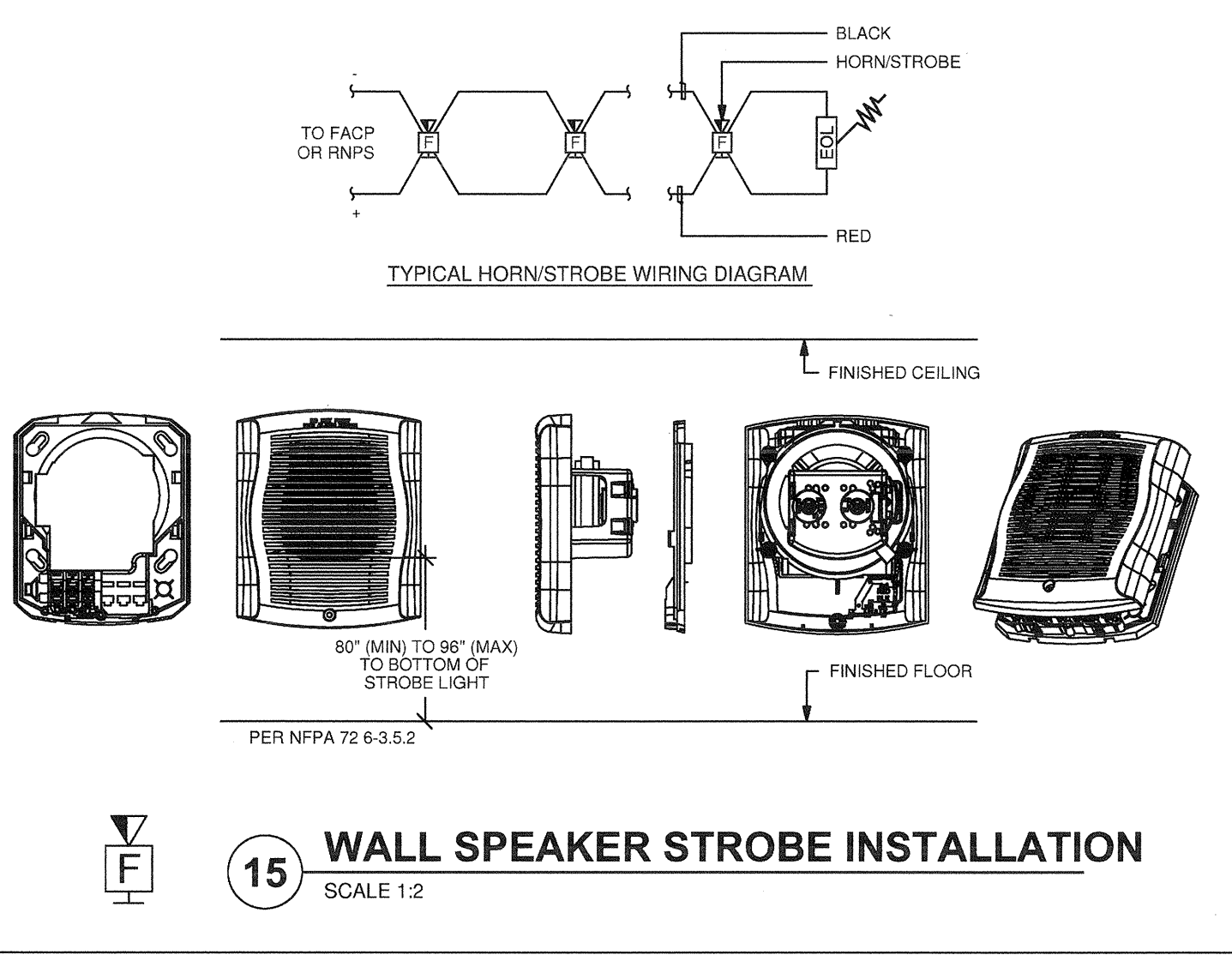
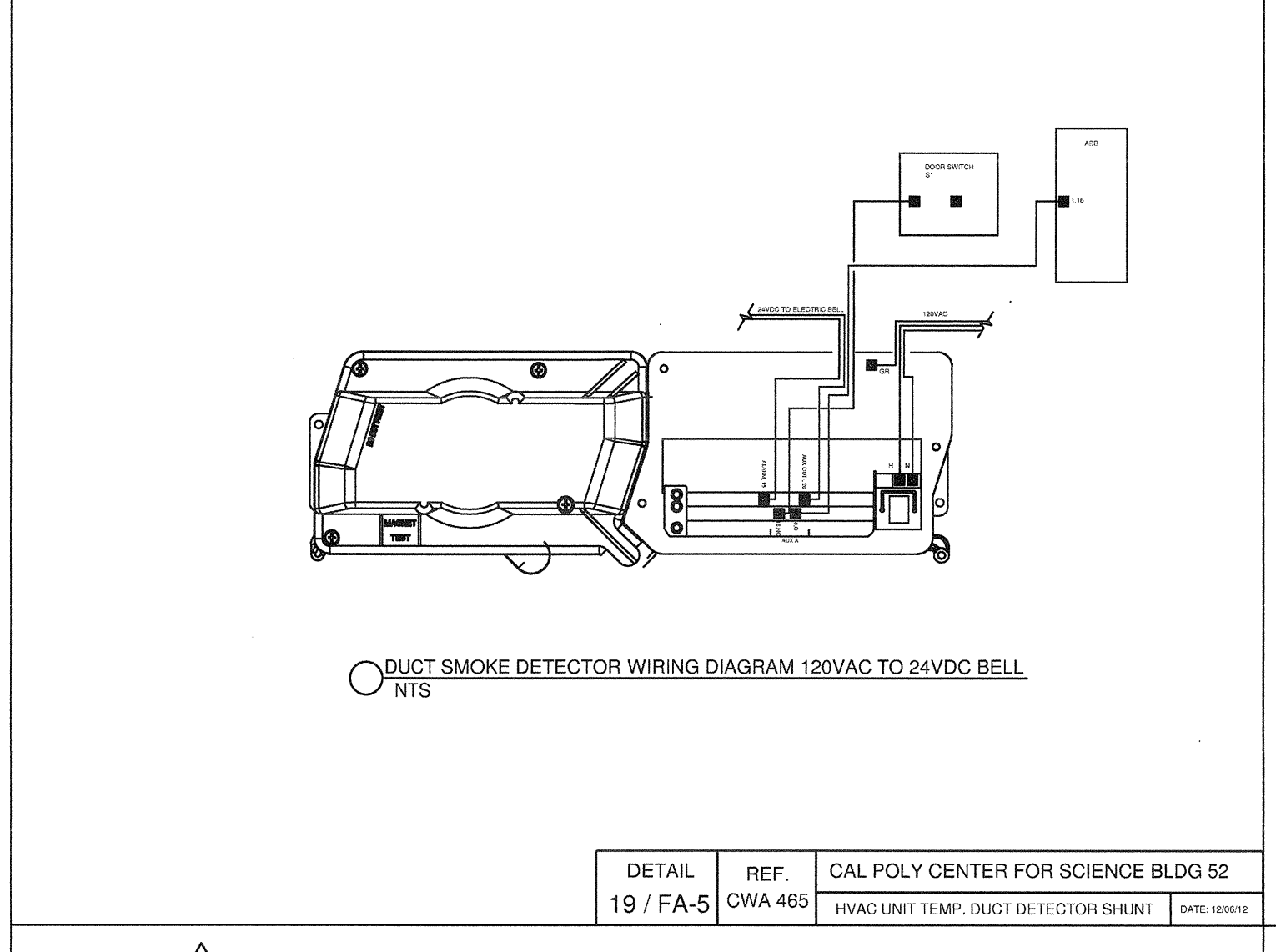
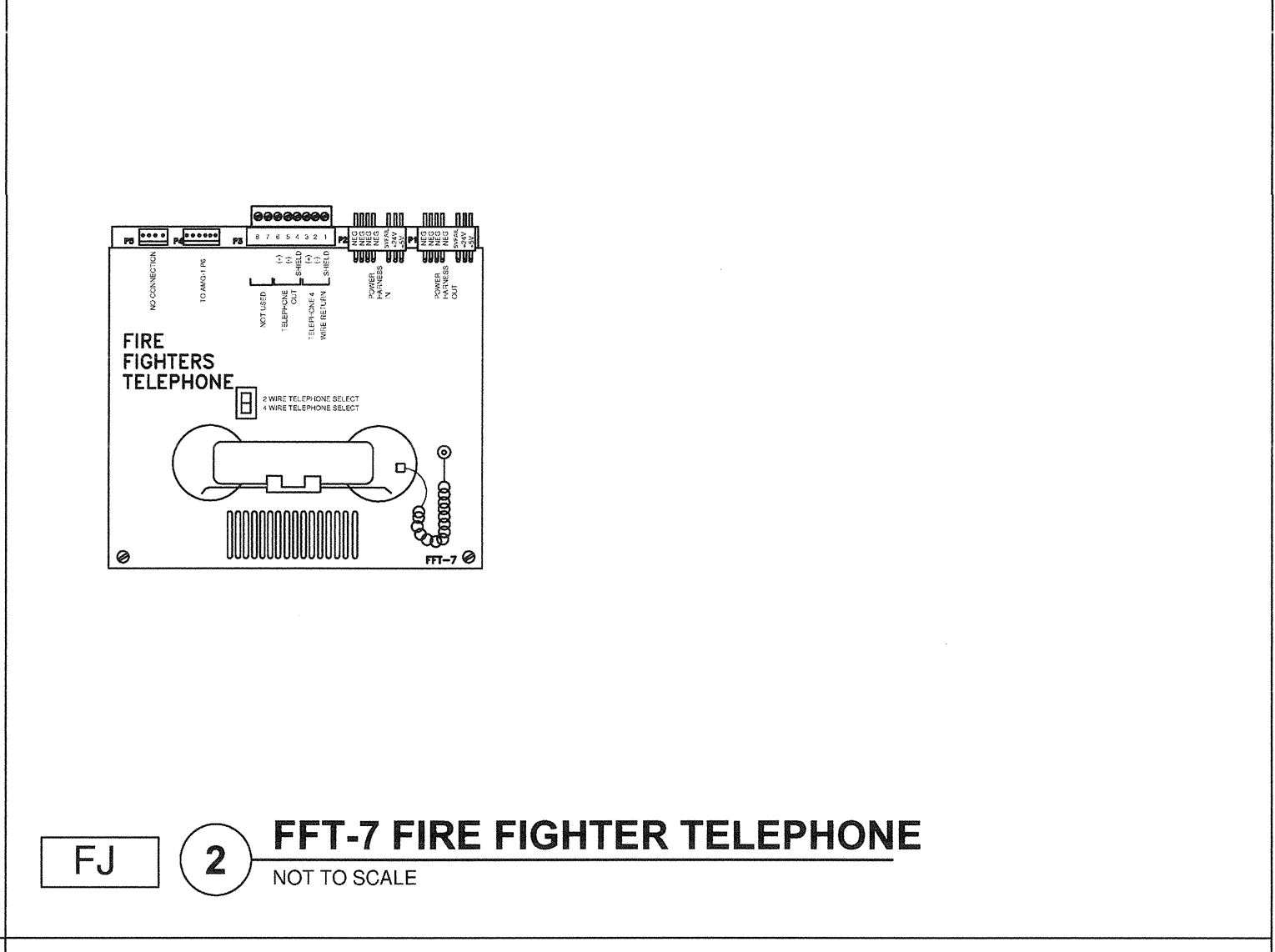
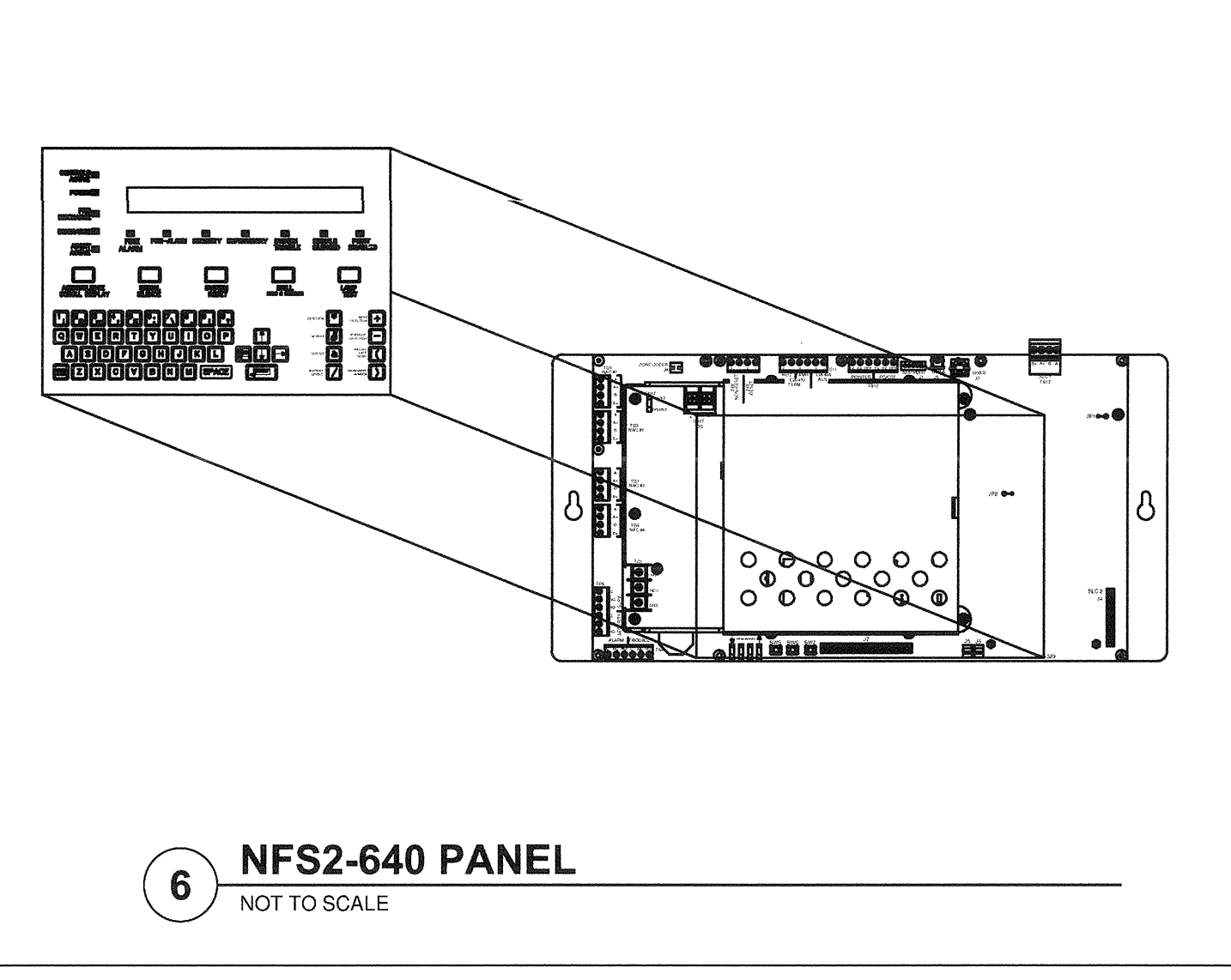
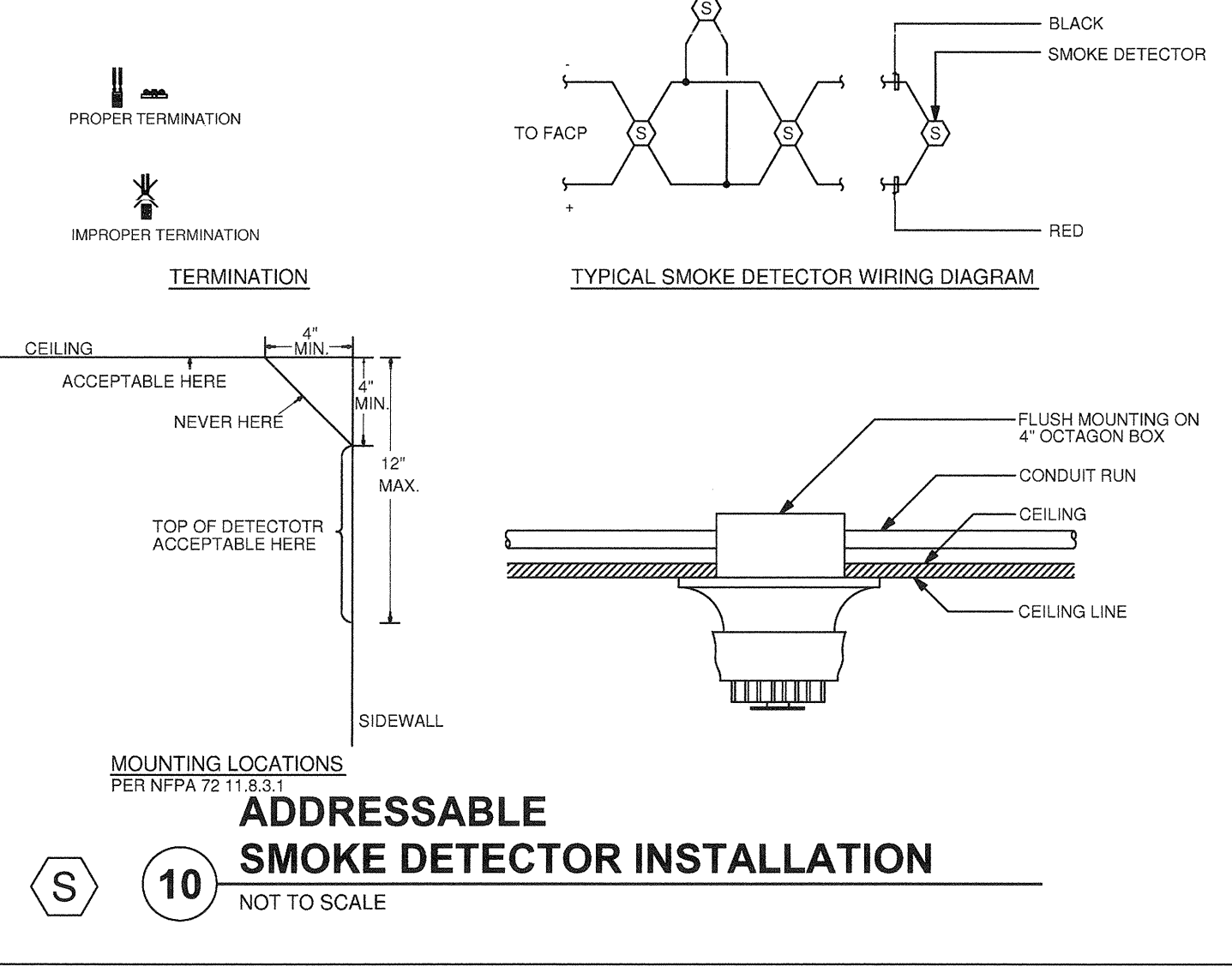
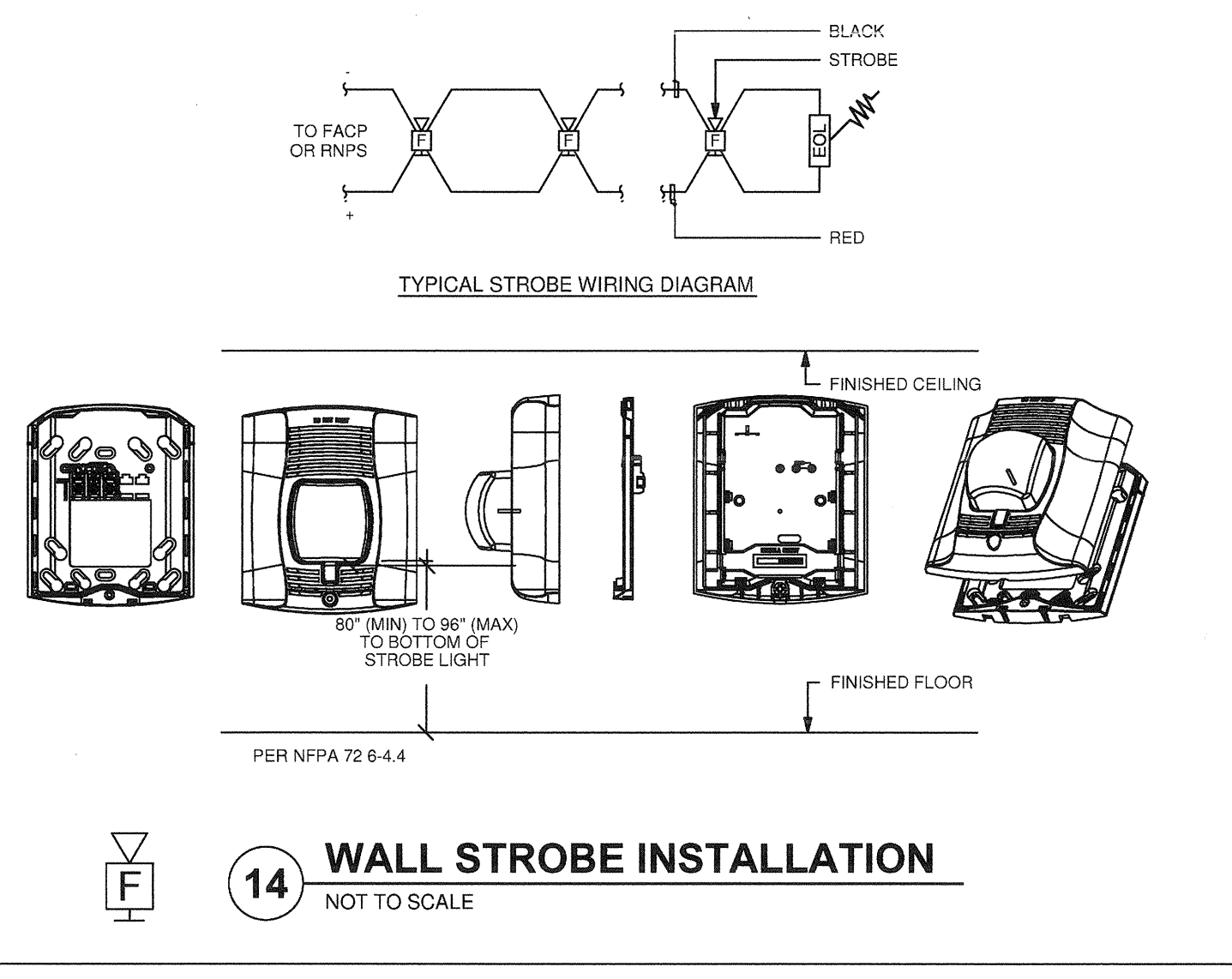
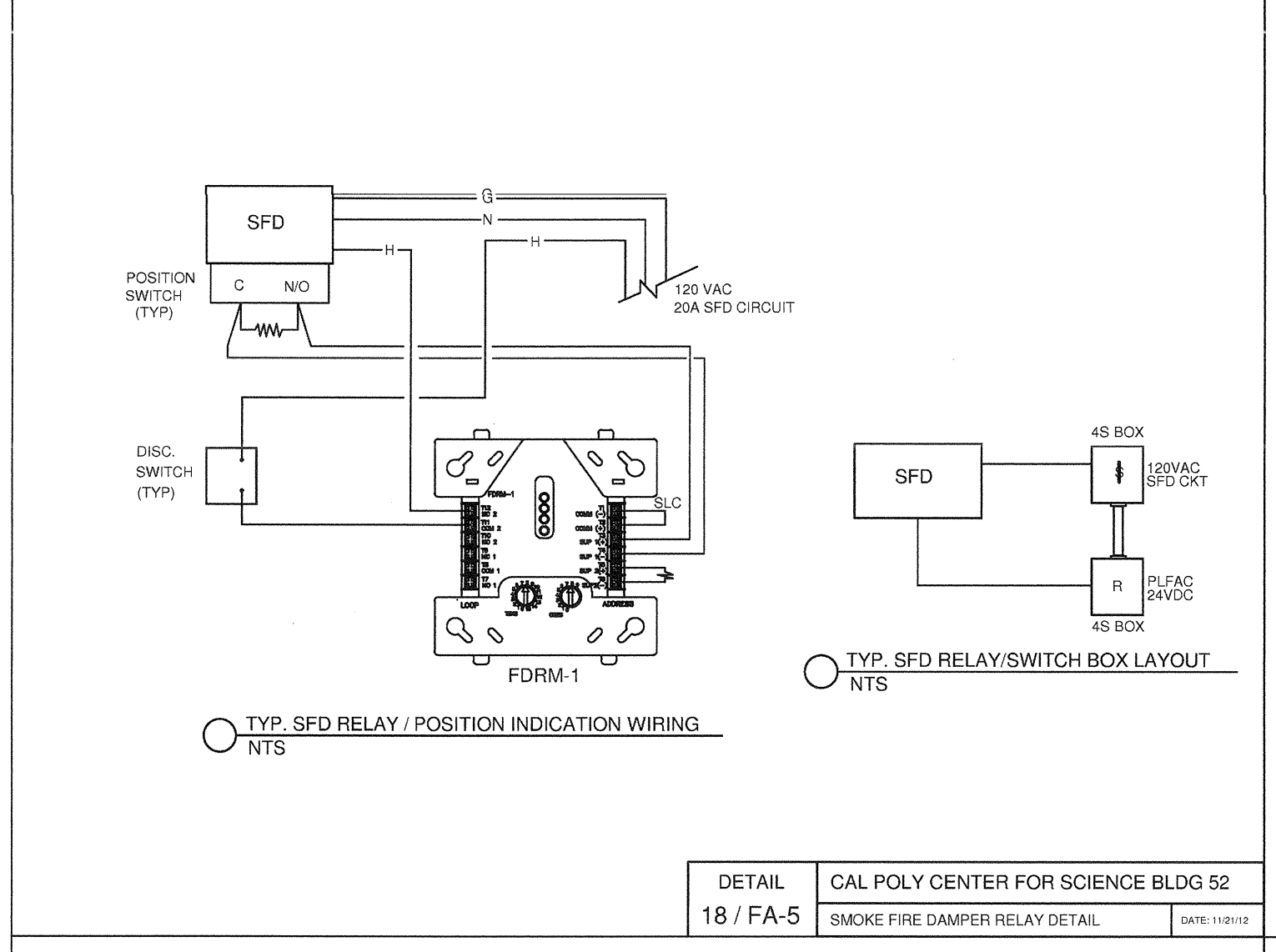
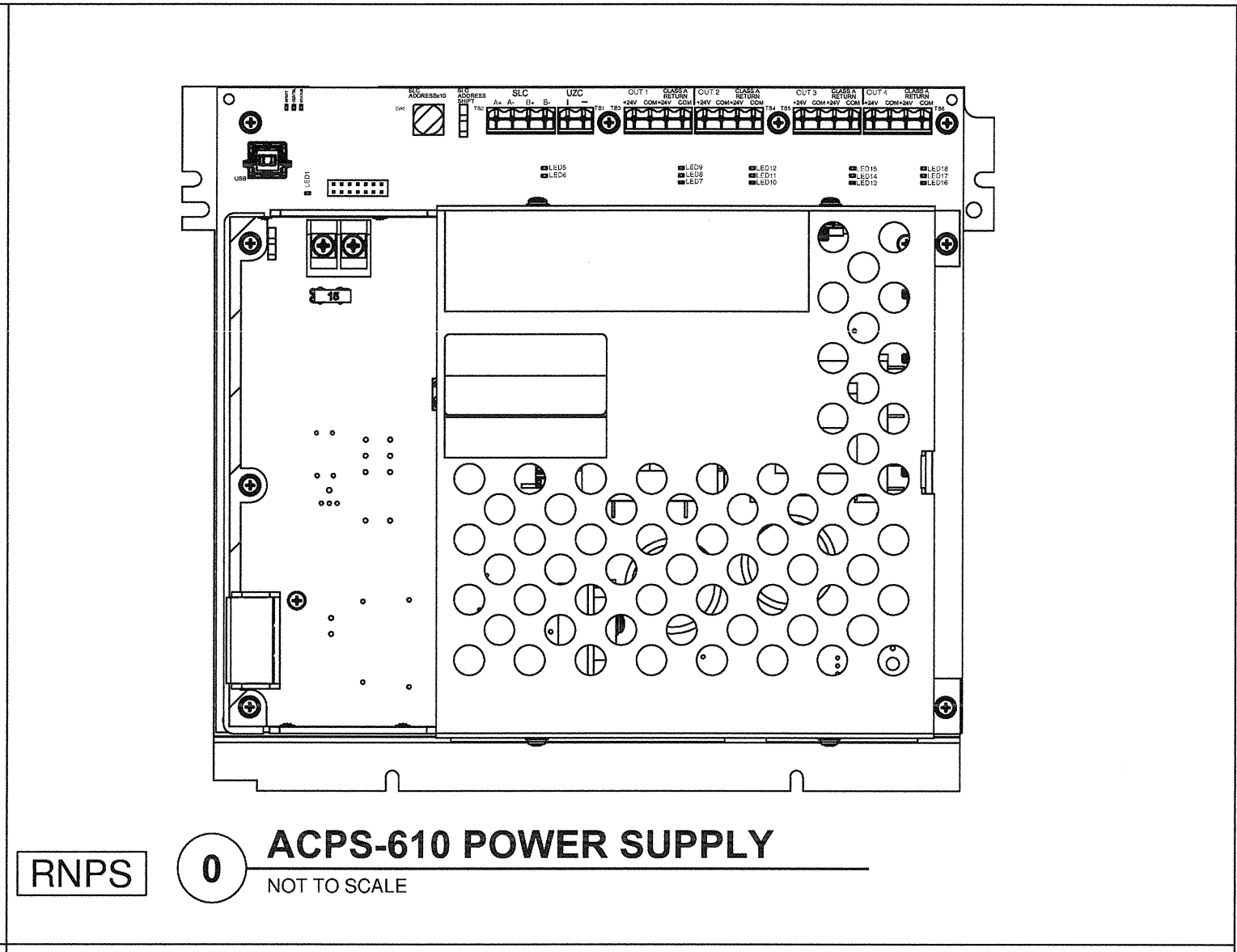
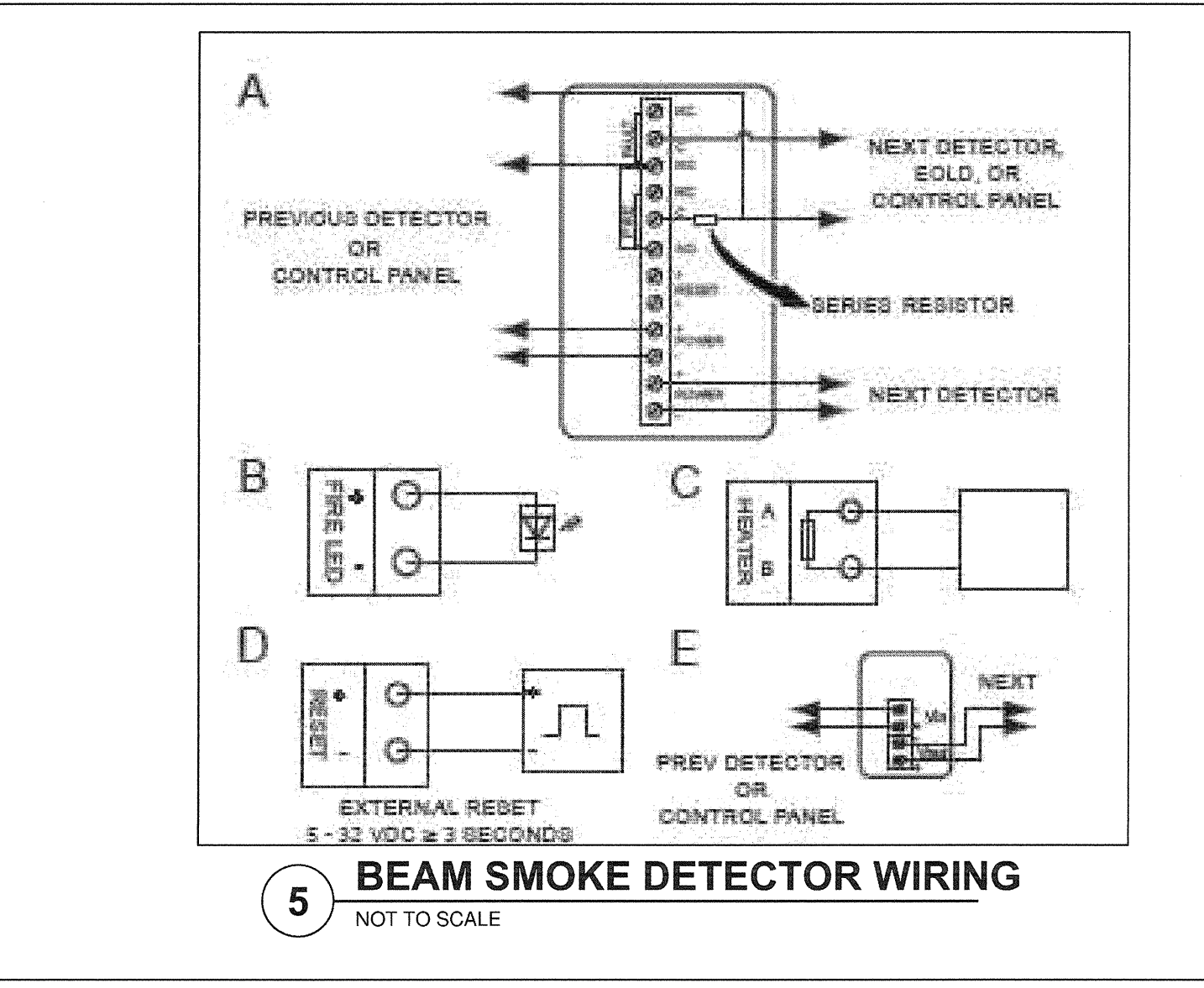
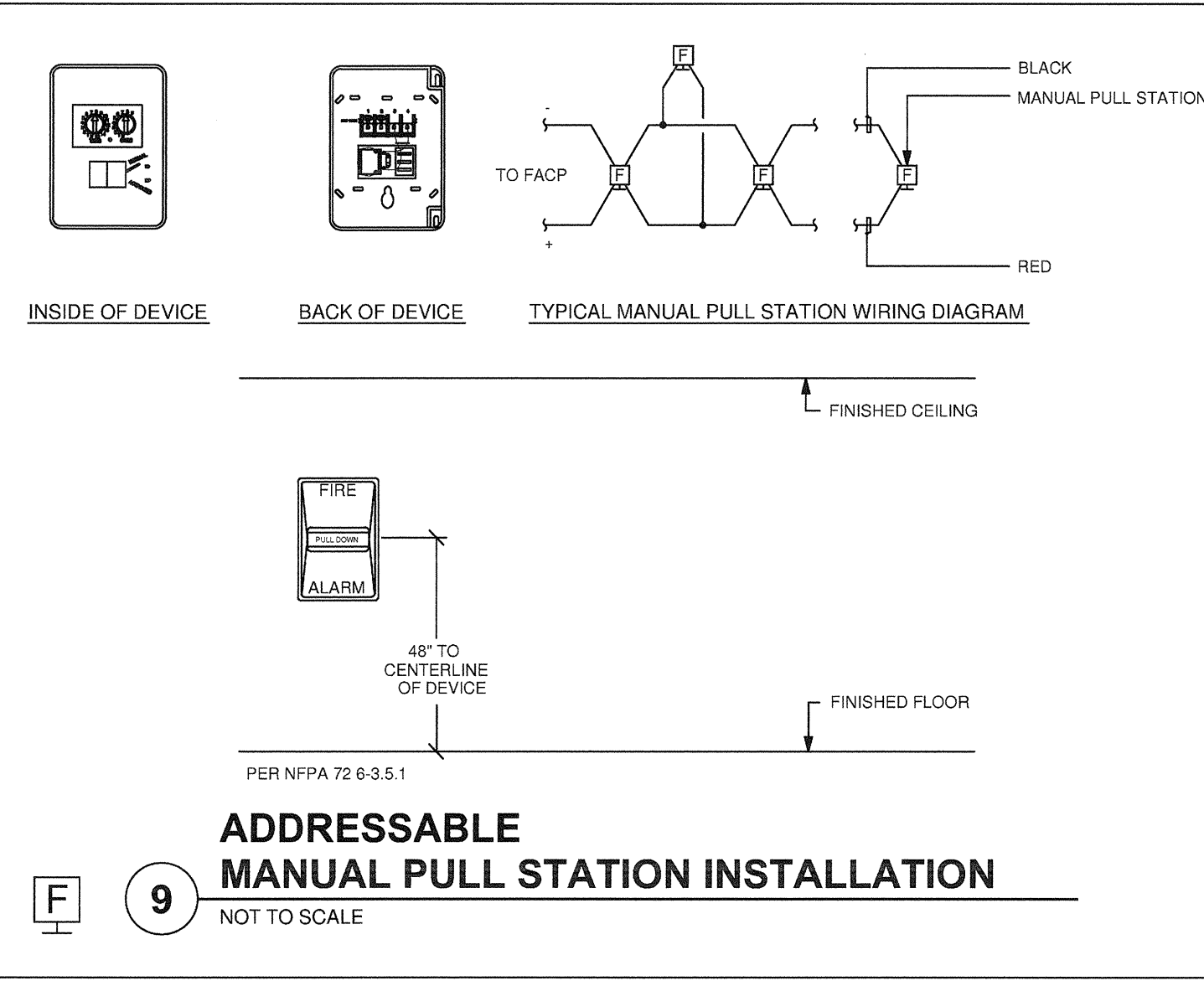
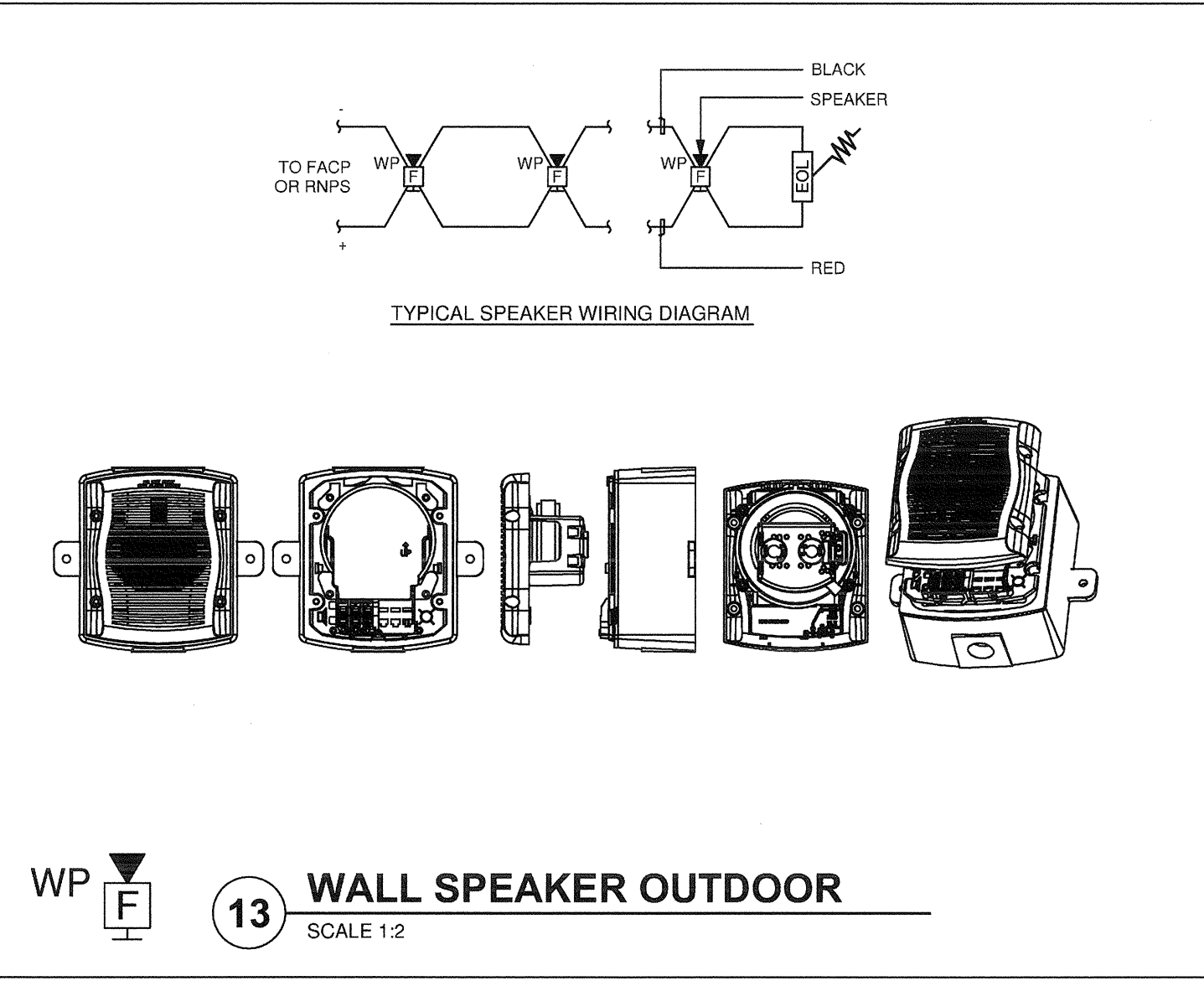
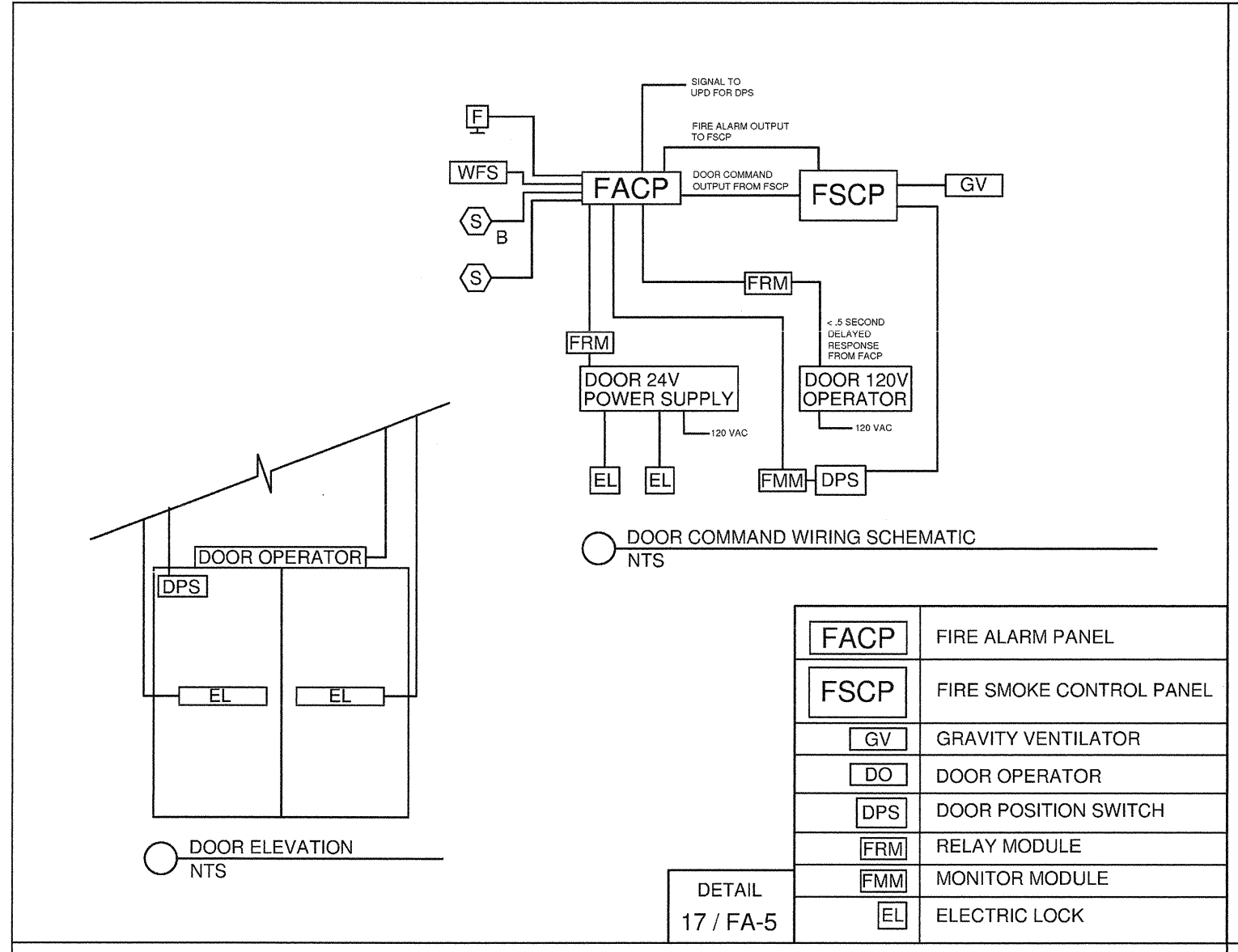
Date	Time	Location	Weather	Wind	Temp	Humidity	Pressure	Remarks

<p>CENTRAL CALIFORNIA</p>	
<p>SHEET ID</p>	
<p>FA 4.0</p>	
<p>SHEET 14 OF 15</p>	



Revisions		DATE	DESCRIPTION	SYMBOL	APPR.
REVIEW COMMENTS	REVIEW COMMENTS				
5/14/2011	CRB # 093.1 & FI 99	5/14/2011			
5/11/2012	SFM REVIEW COMMENTS	8/20/2012			
1/15/2013	CRB 93.2	1/15/2013			
4/23/2013	FA & SMOKE CONTROL SFM COMMENTS	4/23/2013			
8/23/2013	AS-BUILT DRAWINGS	8/23/2013			

DESIGNED BY: Curtis Streeter	DATE: 06/23/2013	SCALE: AS SHOWN	DRAWING CODE: FA ALL DRAWINGS CPCS
DRAWN BY: Derek Richardson			
CHECKED BY: CURTIS STREETER, SET NICET IV #102672			
PROJECT ENGINEER: Integral Design Associates INC.			



DETAILS