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(54) **LOW-POWER-DISSIPATION CMOS
OSCILLATOR CIRCUITS WITH
CAPACITIVELY COUPLED FREQUENCY
CONTROL**

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(US)

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 31 days.

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Primary Examiner—Arnold Kinkead

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(57) **ABSTRACT**

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Methods and apparatus are disclosed for adjusting the frequency tuning range of an oscillator circuit. The oscillator circuit is comprised of at least two MOS devices; a first reactance connecting a drain electrode of a first MOS device to a gate electrode of a second MOS device and a second reactance connecting a drain electrode of the second MOS device to a gate electrode of the first MOS device; and a tank circuit connected to the source and drain electrodes. The first and second reactance may comprise a capacitor or a diode or a combination thereof. In addition, one or more resistors may optionally be connected between a gate electrode of at least one of the MOS device and a power source.

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H03B 1/00 (2006.01)

(52) **U.S. Cl.** **331/117 FE**; 331/117 R;
331/167; 331/185; 331/177 V

(58) **Field of Classification Search** 331/117 FE,
331/117 R, 177 V, 167, 185
See application file for complete search history.

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21 Claims, 4 Drawing Sheets

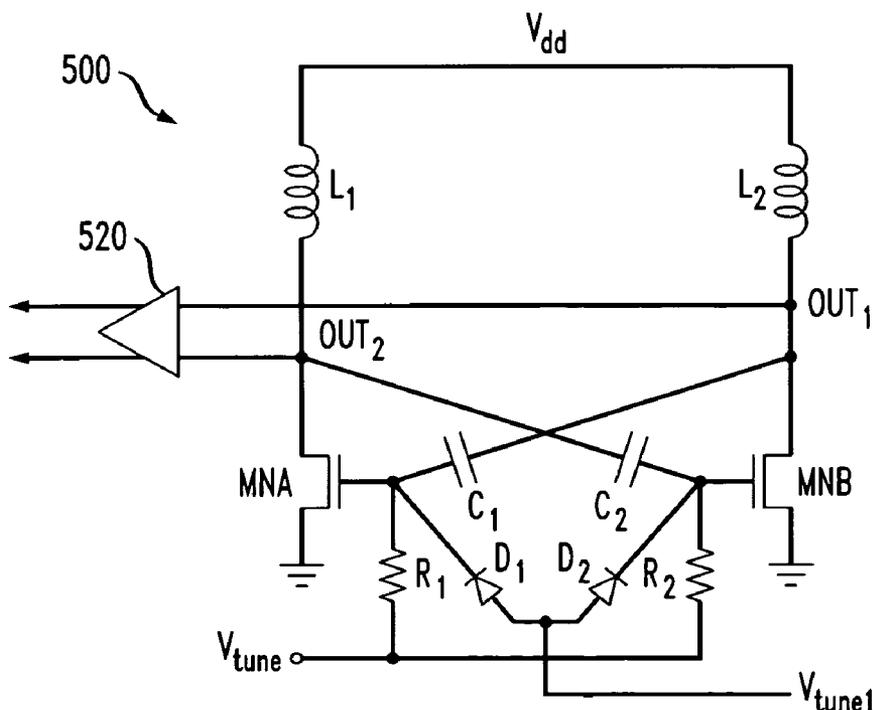


FIG. 1
PRIOR ART

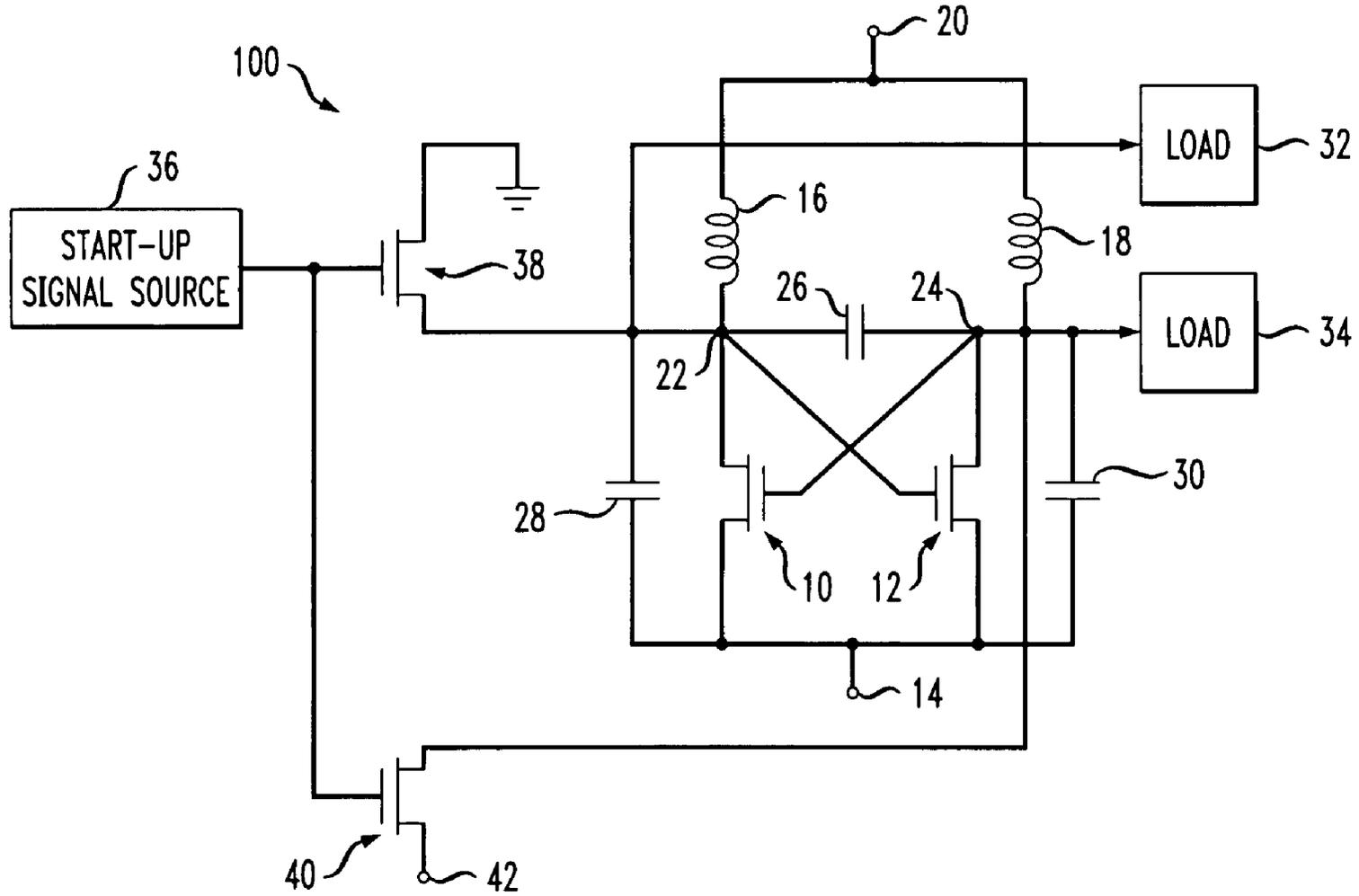


FIG. 2

PRIOR ART

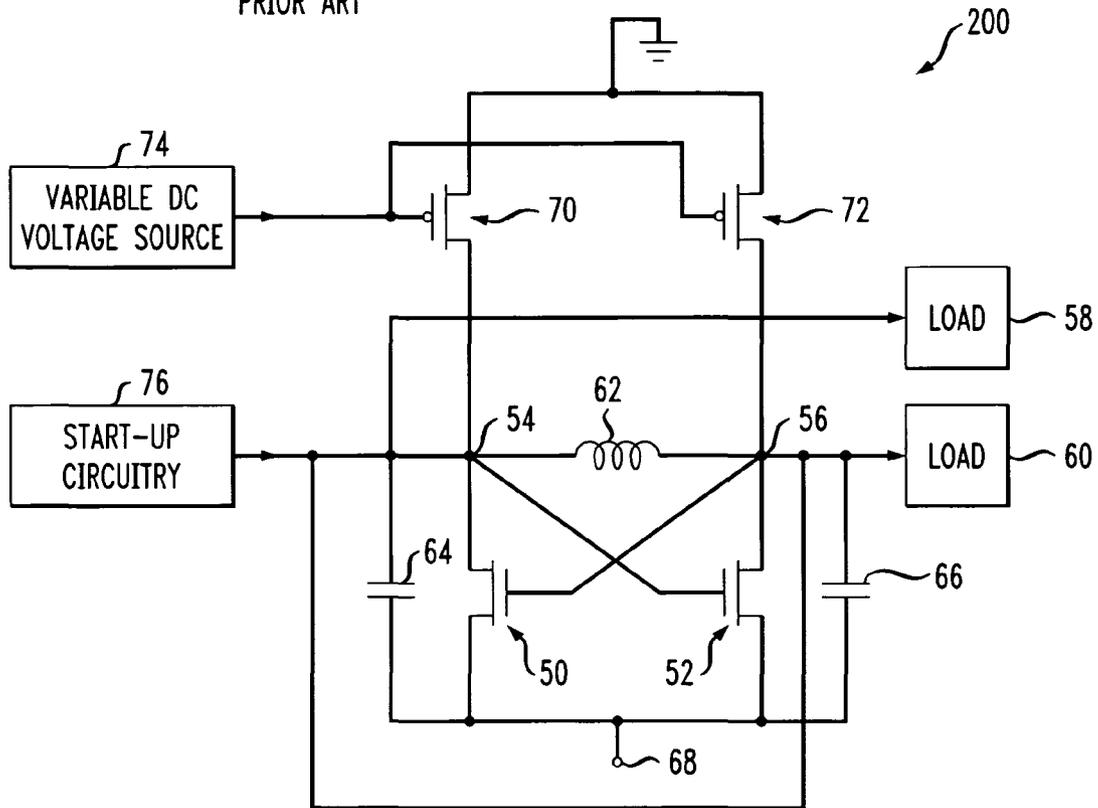


FIG. 3

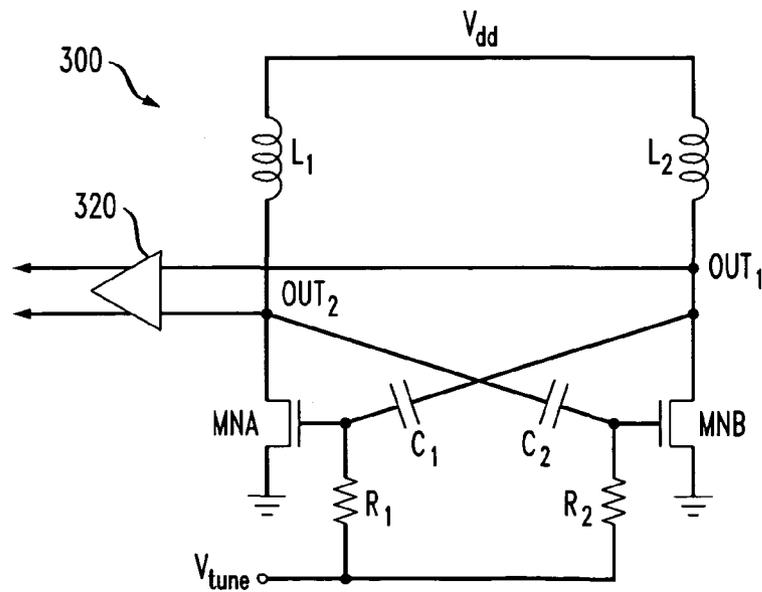


FIG. 6

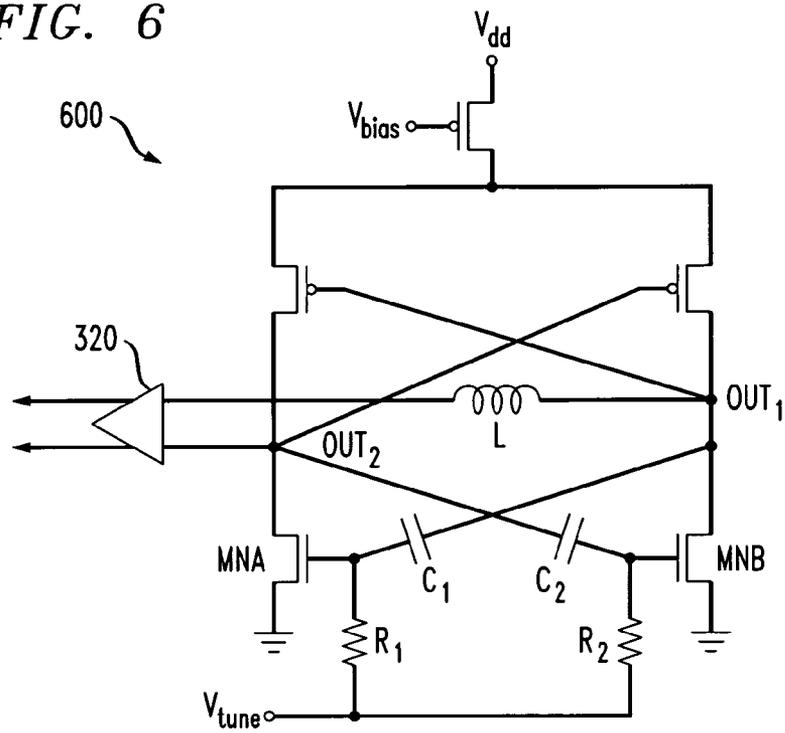
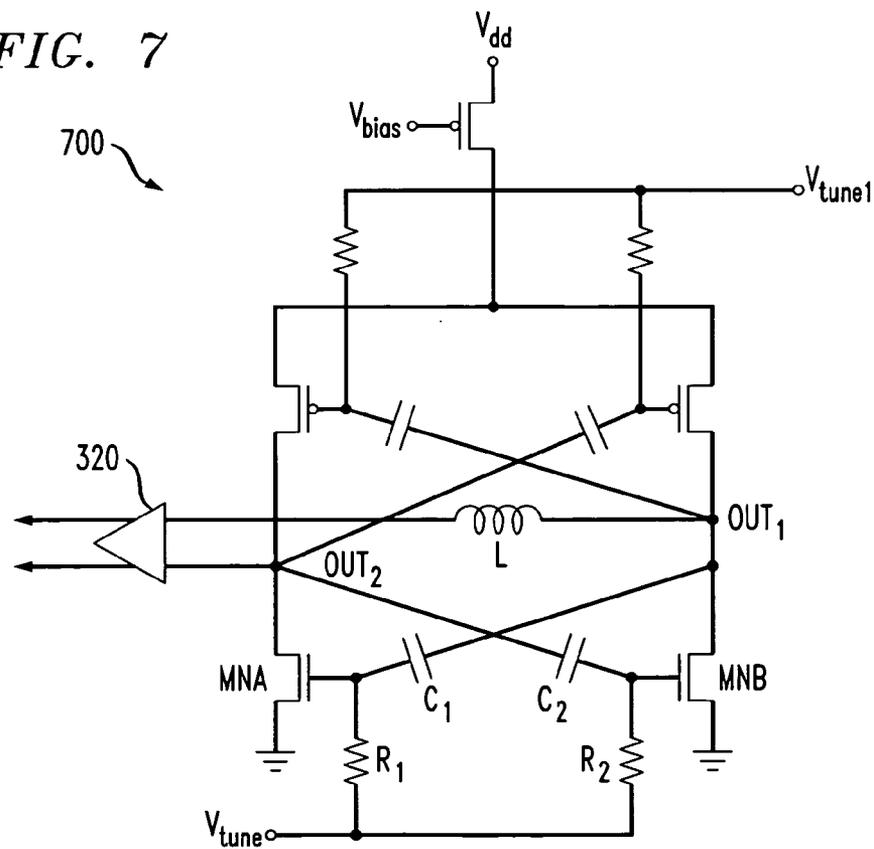


FIG. 7



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**LOW-POWER-DISSIPATION CMOS
OSCILLATOR CIRCUITS WITH
CAPACITIVELY COUPLED FREQUENCY
CONTROL**

FIELD OF THE INVENTION

The present invention is related to low-power-dissipation oscillator circuits and, more particularly, to frequency control techniques for such low-power-dissipation oscillator circuits.

BACKGROUND OF THE INVENTION

Microprocessors, digital signal processors (DSPs) and other synchronous digital logic circuits require a clock signal to maintain synchronization and to control operations. One limitation to the processing power of a processor embodied on an integrated circuit chip is the amount of power the processor can dissipate. Similarly, in portable applications, such as wireless communications, battery capacity can limit the amount of power a chip can consume.

A number of low-power-dissipation oscillator circuits have been proposed or suggested. One popular design is disclosed in U.S. Pat. No. 5,396,195, entitled "Low-Power-Dissipation CMOS Oscillator Circuits," to Gabara, incorporated by reference herein. The disclosed Gabara Oscillator comprises a pair of cross-connected metal-oxide-semiconductor (MOS) devices and an associated inductor-capacitor (LC) tank circuit. Generally, the drain electrode of the first MOS device is directly connected to the gate electrode of the second MOS device and the drain electrode of the second MOS device is directly connected to the gate electrode of the first MOS device.

In addition, a number of techniques have been proposed or suggested for adjusting the frequency tuning range of such low-power-dissipation oscillator circuits. For example, A. Yamagishi et al., Microwave Symposium Digest., 2000 IEEE MTT-S Int'l, Vol. 2, 735-738, (June, 2000) discloses a low-voltage 6-GHz-band CMOS monolithic LC-tank VCO using a tuning-range switching technique. In addition, Liping Zhang and A. A. Sawchuk, Circuits and Systems, 2002. ISCAS 2002. IEEE International Symposium on Circuits and Systems, Vol. 2, II-804-II-806 (May, 2002), discloses a monolithic multi-phase LC-tank VCO.

These representative techniques for adjusting the frequency tuning range of oscillator circuits both employ varactors such that the capacitance is applied directly to the output nodes of the LC tank circuit (which typically contains a certain amount of parasitic capacitance). These parasitic capacitances can be quite large when compared to the capacitance of the varactor. If these parasitic capacitances dominate the capacitance being introduced into the LC tank circuit, then the adjustable frequency range of the varactor control will be reduced. A need therefore exists for methods and apparatus for adjusting the frequency tuning range of oscillator circuits with improved adjustable frequency range.

SUMMARY OF THE INVENTION

Generally, methods and apparatus are disclosed for adjusting the frequency tuning range of an oscillator circuit. The oscillator circuit is comprised of at least two MOS devices; a first reactance connecting a drain electrode of a first MOS device to a gate electrode of a second MOS device and a second reactance connecting a drain electrode of the second MOS device to a gate electrode of the first MOS

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device; and a tank circuit connected to the source and drain electrodes. The first and second reactance may comprises a capacitor or a diode or a combination thereof. In addition, one or more resistors may optionally be connected between a gate electrode of at least one of the MOS device and a power source.

From the process point of view, a method is disclosed for adjusting the frequency tuning range of the oscillator circuit. An oscillating signal is generated using a pair of MOS devices and an associated tank circuit; a voltage is generated at a gate of one or more of the MOS devices using a first reactance connected between a drain electrode of a first MOS device and a gate electrode of a second MOS device and a second reactance connected between a drain electrode of the second MOS device and a gate electrode of the first MOS device; and the frequency of the oscillating signal is adjusted by biasing one or more of first and second the MOS devices.

A more complete understanding of the present invention, as well as further features and advantages of the present invention, will be obtained by reference to the following detailed description and drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic circuit diagram illustrating an exemplary conventional low-power-dissipation oscillator circuit;

FIG. 2 is a schematic circuit diagram illustrating an alternative conventional low-power-dissipation oscillator circuit;

FIG. 3 is a schematic circuit diagram illustrating an oscillator circuit incorporating features of the present invention; and

FIGS. 4 through 7 are a schematic circuit diagrams illustrating alternate oscillator circuits incorporating features of the present invention.

DETAILED DESCRIPTION

The exemplary conventional oscillator circuit **100** shown in FIG. 1 comprises two conventional n-channel MOS devices **10** and **12**. The devices **10** and **12** are assumed to be substantially identical to each other. The lower or source electrode of each of the devices **10** and **12** of FIG. 1 is connected to a source or power supply **14**. The source **14** will be designated herein as V_{SS} and will, illustratively, be assumed to be a direct-current supply having a value of about -5.0 volts. The upper or drain electrodes of the devices **10** and **12** are connected through respective inductors **16** and **18** to a source **20**. Herein, the source **20** will be designated $V_{SS}/2$ and will, for example, be assumed to have a value of about -2.5 volts. The gate electrode of the right-hand MOS device **12** of FIG. 1 is directly connected to the drain electrode of the left-hand MOS device **10** at a node point **22**. Similarly, the gate electrode of the left-hand MOS device **10** is directly connected to the drain electrode of the right-hand device **12** at a node point **24**.

A capacitor **26** is directly connected between the node points **22** and **24** shown in FIG. 1. Two additional capacitors **28** and **30** are indicated as being connected between the node points **22** and **24** and the source **14**. The inductors **16** and **18** and the capacitors **26**, **28** and **30** constitute an LC tank circuit for the depicted oscillator. It is noted that the capacitors **26**, **28** and **30** may include the parasitic capacitance of devices **10** and **12**.

The circuit of FIG. 1 provides a sine-wave voltage output at the node point 22 and a complementary such output at the node point 24. In other words, the sine waves provided at the node points 22 and 24 are 180 degrees out of phase with respect to each other.

The output appearing at the node point 22 of FIG. 1 is connected to a load 32, while the output at the node point 24 is connected to a load 34. Illustratively, both loads are capacitive in nature. Advantageously, the loads 32 and 34 are, for example, MOS devices included in a network which is controlled by the signals generated at the node points 22 and 24.

To ensure reliable operation of the circuit 100, it is advantageous to provide start-up circuitry to drive the depicted circuit into its steady-state oscillatory mode. By way of example, such start-up circuitry includes a start-up signal source 36 and n-channel MOS devices 38 and 40, as shown in FIG. 1. The drain electrode of the device 38 of FIG. 1 is connected to a point of reference potential such as ground, and the source electrode thereof is connected to the node point 22. Further, the source electrode of the device 40 is connected to a source 42 having the same value as that of the source 14, and the drain electrode thereof is connected to the node point 24. And the gate electrodes of both of the devices 38 and 40 are connected to the output of the start-up signal source 36.

The start-up signal source 36 of FIG. 1 applies either V_{SS} (-5.0 volts) or 0 volts (ground) to the gates of the MOS devices 38 and 40. As long as -5.0 volts is applied to their gates, the devices 38 and 40 are nonconductive and the start-up circuitry is in effect disabled.

Initially, with the start-up circuitry disabled but the remainder of the circuit shown in FIG. 1 energized, it is possible that the voltages at the node points 22 and 24 will assume a condition in which they are approximately equal. In that case, the currents through the inductors 16 and 18 will also be approximately equal. As a result, the circuit would remain in a balanced or non-oscillatory steady-state condition. By applying a start-up signal to the circuit 100, the circuit 100 is unequivocally driven into its desired oscillatory state.

The application of the start-up signal to the gates of the MOS devices 38 and 40 causes these devices to be rendered conductive. As a result, the voltage of the node point 22 is driven in a positive direction while the voltage of the node point 24 is driven in a negative direction. At the same time, the current through the inductor 16 decreases while the current through the inductor 18 increases. In this manner, the initially balanced condition of the circuit is altered by the start-up signal.

When the start-up signal returns to the value V_{SS} , the devices 38 and 40 in the start-up circuitry are rendered nonconductive. At that time, the oscillator circuit is in an unbalanced condition, with energy stored in the inductors 16 and 18 and the capacitors 26, 28 and 30. Subsequently, due to the energy stored in the tank circuit and the regenerative feedback action of the cross-connected MOS devices 10 and 12, oscillations build up until an output sine-wave signal appears at the node point 22 and a complementary output sine-wave signal appears at the node point 24.

Each of the sine waves has a maximum value of 0 volts and a minimum value of V_{SS} (-5.0 volts). The mid-point of each sine wave occurs at $V_{SS}/2$. The two sine waves are 180 degrees out of phase with respect to each other.

FIG. 2 is a schematic circuit diagram illustrating an alternative conventional low-power-dissipation oscillator circuit 200. The oscillator circuit 200 shown in FIG. 2 is

similar to the circuit 100 of FIG. 1. Thus, the FIG. 2 arrangement also includes cross-connected n-channel MOS devices, which are designated by reference numerals 50 and 52. In FIG. 2, output nodes 54 and 56 are connected to loads 58 and 60, respectively. An inductor 62 (rather than a capacitor as in FIG. 1) is connected between the output node points. The inductor 62 together with capacitors 64 and 66 constitute the tank circuit of the FIG. 2 arrangement. It is again noted that the capacitors 64 and 66 may include the parasitic capacitance of devices 50, 52 and 72.

Further, the source electrodes of the devices 50 and 52 of FIG. 2, as well as the bottom plates of the capacitors 64 and 66, are connected to a source 68 which is designated V_{SS} . Illustratively, the source 68 has a value of approximately -5.0 volts.

The oscillator circuit 200 of FIG. 2 also includes p-channel MOS devices 70 and 72 respectively connected between a point of reference potential such as ground and the drain electrodes of the devices 50 and 52. By varying the direct-current voltage applied to the gate electrodes of the devices 70 and 72, it is possible to change the frequency at which the depicted circuit oscillates. A source 74 for accomplishing this frequency variation is shown in FIG. 2.

Advantageously, the circuit 200 of FIG. 2 also includes start-up circuitry 76 of the same type described above and included in the FIG. 1 circuit. In this manner, the circuit 200 of FIG. 2 is controlled to achieve a steady-state oscillatory condition.

For a detailed discussion of the fabrication and representative examples of the circuits 100, 200, see U.S. Pat. No. 5,396,195, entitled "Low-Power-Dissipation CMOS Oscillator Circuits," to Gabara, incorporated by reference herein above.

As previously indicated, existing techniques for adjusting the frequency tuning range of oscillator circuits apply the capacitance directly to the output nodes of the LC tank circuit (which typically contains a certain amount of parasitic capacitance). The present invention recognizes that the varactor can be placed in a region where the parasitic capacitance is reduced so that the overall effective variation of the frequency controlling capacitance can be used to adjust the frequency behavior of the LC tank circuit over a larger range. Thus, while it was previously assumed that a direct connection was required to cross-couple the MOS devices 10 and 12, the present invention recognizes that these MOS devices can be connected through a reactance, such as capacitors, diodes, or a combination thereof, that introduces a low impedance in the cross-coupled MOS devices. Essentially, the reactance appears like an open circuit at lower frequencies and a short circuit at higher frequencies (and thus appears like the direct connection of the cross-coupled devices of the Gabara Oscillator).

Generally, the varactor capacitance is placed before the amplifying element, rather than after the amplifying element. In one particular implementation, the amplifying element actually serves as the varactor element. According to one aspect of the invention, the gate of the MOS devices are isolated from the rest of the circuit and the varactor is positioned at this junction.

FIG. 3 is a schematic circuit diagram illustrating an oscillator circuit 300 incorporating features of the present invention. As discussed hereinafter, the oscillator circuit 300 is controlled by MOS varactors MNA and MNB. The MOS varactors MNA and MNB are also the MOS devices that provide the negative resistance in the LC tank circuit to sustain oscillations. Thus, the two MOS devices MNA and MNB serve two functions simultaneously. The two MOS

devices MNA and MNB provide positive feedback and behave as varactors, thereby saving on component usage and reducing the area of the LC tank circuit. The varactor MNA sees the capacitance of C_1 and the parasitic capacitance of resistor R_1 . In addition, the parasitic capacitance of output node OUT_1 is sensed through the series connection of C_1 . Thus, the effect of the parasitic capacitance of output node OUT_1 has a reduced influence on the capacitance of the MOS varactor MNA. In one exemplary implementation, the tuning range at 6 GHz was simulated to be 300 MHz.

Like the oscillator circuit **100** of FIG. **1**, the oscillator circuit **300** comprises the two conventional n-channel MOS devices MNA and MNB that are assumed to be substantially identical to each other. The lower or source electrode of each of the devices MNA and MNB is connected to a point of reference potential such as ground. The upper or drain electrodes of the devices MNA and MNB are connected through respective inductors L_1 and L_2 to a source V_{dd} . Herein, the source V_{dd} will, for example, be assumed to have a value of about +2.5 volts. The gate electrode of the right-hand MOS device MNB is connected through the capacitor C_2 to the drain electrode of the left-hand MOS device MNA at the node point OUT_2 . Similarly, the gate electrode of the left-hand MOS device MNA is connected through the capacitor C_1 to the drain electrode of the right-hand device MNB at a node point OUT_1 . In addition, the two resistors R_1 and R_2 are connected to the gate electrode of each MOS device MNA and MNB, respectively, and a source or power supply V_{tune} that will, for example, be assumed to be a direct-current supply having a value of approximately between -1.0 to +1.0 volts. The inductors L_1 and L_2 , the capacitors C_1 and C_2 and the parasitic gate capacitance of devices MNA and MNB constitute the LC tank circuit for the oscillator **300**.

The circuit **300** of FIG. **3** provides a sine-wave voltage output at the node point OUT_1 and a complementary such output at the node point OUT_2 . In other words, the sine waves provided at the node points OUT_1 and OUT_2 are 180 degrees out of phase with respect to each other.

The outputs appearing at the node points OUT_1 and OUT_2 are connected to a load **320**. Illustratively, the load **320** is capacitive in nature, such as MOS devices included in a network which is controlled by the signals generated at the node points OUT_1 and OUT_2 . It is noted that it may be advantageous to provide start-up circuitry (not shown) to drive the depicted circuit into its steady-state oscillatory mode, in the manner described in U.S. Pat. No. 5,396,195. Initially, with the start-up circuitry disabled but the circuit **300** shown in FIG. **3** energized, it is possible that the voltages at the node points OUT_1 and OUT_2 will assume a condition in which they are approximately equal. In that case, the currents through the inductors L_1 and L_2 will also be approximately equal. As a result, the circuit **300** would remain in a balanced or non-oscillatory steady-state condition. By applying a start-up signal to the circuit **300**, the circuit **300** is unequivocally driven into its desired oscillatory state.

The application of the start-up signal causes the voltage of the node point OUT_1 to be driven in a positive direction while the voltage of the node point OUT_2 is driven in a negative direction. At the same time, the current through the inductor L_1 increases while the current through the inductor L_2 decreases. In this manner, the initially balanced condition of the circuit **300** is altered by the start-up signal.

When the start-up signal is disabled, the oscillator circuit is in an unbalanced condition, with energy stored in the inductors L_1 and L_2 and the capacitors C_1 and C_2 . Subse-

quently, due to the energy stored in the tank circuit and the regenerative feedback action of the cross-connected MOS devices MNA and MNB, oscillations build up until an output sine-wave signal appears at the node point OUT_1 and a complementary output sine-wave signal appears at the node point OUT_2 . Each of the sine waves has a voltage that ranges approximately between 0 volts and 5 volts. The mid-point of each sine wave occurs at $V_{dd}/2$. The two sine waves are 180 degrees out of phase with respect to each other.

Among other benefits, the oscillator circuit **300** has a reduced component count, relative to the oscillator circuits **100**, **200** of FIGS. **1** and **2**, and offers another mechanism to control the frequency of oscillation of a CMOS LC tank circuit. This technique can be used in conjunction with conventional frequency control methods mentioned earlier to further increase the tuning range.

FIG. **4** is a schematic circuit diagram illustrating an oscillator circuit **400** incorporating features of the present invention. The oscillator circuit **400** is implemented in a similar manner to the oscillator circuit **300** of FIG. **3**, except that the resistors R_1 and R_2 of FIG. **3** are replaced by diodes D_1 and D_2 (or varactors). Thus, the MOS devices MNA and MNB are cross-coupled using a combination of the capacitors C_1 and C_2 , and diodes D_1 and D_2 . In this case, the diodes D_1 and D_2 control the biasing of devices MNA and MNB as well as adding an additional capacitance that can be added to the tank circuit.

FIG. **5** is a schematic circuit diagram illustrating an oscillator circuit **500** incorporating features of the present invention. The oscillator circuit **500** is implemented in a similar manner to the oscillator circuit **300** of FIG. **3**, except that the oscillator circuit **500** also includes a pair of diodes D_1 and D_2 that are connected to the gate of the MOS devices MNA and MNB as well as resistors R_1 and R_2 controlled by potential V_{tune} . Thus, the MOS devices MNA and MNB are cross-coupled using a combination of the capacitors C_1 and C_2 , resistors R_1 and R_2 and diodes D_1 and D_2 . Now, there are two relatively independent controls to adjust the frequencies of oscillation, namely, V_{tune1} and V_{tune2} .

FIGS. **6** and **7** are schematic circuit diagrams illustrating oscillator circuits **600**, **700** incorporating features of the present invention. The oscillator circuits **600**, **700** are implemented in a similar manner to the oscillator circuit **300** of FIG. **3**, except that the oscillator circuits **600**, **700** also includes a pair of cross-coupled p-channel devices. The oscillator circuit **700** further includes corresponding capacitors connected to the gates of the top two cross-coupled p-channel devices.

A plurality of identical die are typically formed in a repeated pattern on a surface of the wafer. Each die includes a device described herein, and may include other structures or circuits. The individual die are cut or diced from the wafer, then packaged as an integrated circuit. One skilled in the art would know how to dice wafers and package die to produce integrated circuits. Integrated circuits so manufactured are considered part of this invention.

It is to be understood that the embodiments and variations shown and described herein are merely illustrative of the principles of this invention and that various modifications may be implemented by those skilled in the art without departing from the scope and spirit of the invention.

We claim:

1. An oscillator circuit, comprising:
at least two MOS devices;

a first reactance connecting a drain electrode of a first MOS device to a gate electrode of a second MOS device and a second reactance connecting a drain

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electrode of said second MOS device to a gate electrode of said first MOS device;
 a tank circuit connected to said source and drain electrodes; and
 at least a first diode and a second diode, said at least first and second diodes connected to said tank circuit and wherein said first diode is configured to adjust a biasing of said first MOS device and wherein said second diode is configured to adjust a biasing of said second MOS device.

2. The oscillator circuit of claim 1, wherein each of said first and second reactance comprises a capacitor.

3. The oscillator circuit of claim 1, wherein each of said first and second reactance comprises a diode.

4. The oscillator circuit of claim 1, further comprising one or more resistors connected to a gate electrode of at least one of said MOS device and a power source.

5. The oscillator circuit of claim 1, further including means for connecting said source electrode to a reference potential.

6. The oscillator circuit of claim 1, further including means for connecting said drain electrode to a source of potential.

7. The oscillator of claim 1, wherein said tank circuitry comprises one or more capacitors and inductors.

8. The oscillator circuit of claim 1, further including start-up circuitry.

9. A method for adjusting the frequency tuning range of an oscillator circuit, comprising the steps of:
 generating an oscillating signal using a pair of MOS devices and an associated tank circuit;
 generating a voltage at a gate of one or more of said MOS devices using a first reactance connected between a drain electrode of a first MOS device and a gate electrode of a second MOS device and a second reactance connected between a drain electrode of said second MOS device and a gate electrode of said first MOS device; and
 adjusting a frequency of said oscillating signal by biasing one or more of first and second said MOS devices, wherein said biasing is performed utilizing a first diode that adjusts a biasing of said first MOS device and a second diode that adjusts a biasing of said second MOS device; the diodes also connected to said tank circuit.

10. The method of claim 9, further comprising the step of generating a bias using one or more resistors connected to a gate electrode of at least one of said MOS device and a power source.

11. The method of claim 9, further comprising the step of connecting said source electrode to a reference potential.

12. The method of claim 9, further comprising the step of connecting said drain electrode to a source of potential.

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13. An integrated circuit, comprising:
 an oscillator circuit comprising:
 at least two MOS devices;
 a first reactance connecting a drain electrode of a first MOS device to a gate electrode of a second MOS device and a second reactance connecting a drain electrode of said second MOS device to a gate electrode of said first MOS device;
 a tank circuit connected to said source and drain electrodes; and
 at least a first diode and a second diode, said at least first and second diodes connected to said tank circuit and wherein said first diode is configured to adjust a biasing of said first MOS device and wherein said second diode is configured to adjust a biasing of said second MOS device.

14. The integrated circuit of claim 13, wherein each of said first and second reactance comprises a capacitor.

15. The integrated circuit of claim 13, wherein each of said first and second reactance comprises a diode.

16. The integrated circuit of claim 13, further comprising one or more resistors connected to a gate electrode of at least one of said MOS device and a power source.

17. The integrated circuit of claim 13, further including means for connecting said source electrode to a reference potential.

18. The integrated circuit of claim 13, further including means for connecting said drain electrode to a source of potential.

19. The oscillator of claim 1, wherein said tank circuitry comprises one or more capacitors and inductors.

20. The integrated circuit of claim 13, further including start-up circuitry.

21. An oscillator circuit, comprising:
 at least two MOS devices;
 a first reactance connecting a drain electrode of a first MOS device to a gate electrode of a second MOS device and a second reactance connecting a drain electrode of said second MOS device to a gate electrode of said first MOS device;
 a cross-coupled transistor pair, said cross-coupled transistor pair comprising a third MOS device, a fourth MOS device, a first reactance connecting a drain electrode of said third MOS device to a gate electrode of said fourth MOS device and a second reactance connecting a drain electrode of said fourth MOS device to a gate electrode of said third MOS device, wherein a bias control signal is configured to adjust an average DC value of an output of said oscillator circuit; and
 a tank circuit connected to said drain electrode of said first MOS device and said drain electrode of said second MOS device.

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