PERIOD FORMULAS FOR CONCRETE SHEAR WALL BUILDINGS

By Rakesh K. Goel,¹ and Anil K. Chopra ²

ABSTRACT: Most seismic codes specify empirical formulas to estimate the fundamental vibration period of buildings. Evaluated first in this paper are the formulas specified in present U.S. codes using the available data on the fundamental period of buildings "measured" from their motions recorded during eight California earthquakes, starting with the 1971 San Fernando earthquake and ending with the 1994 Northridge earthquake. It is shown that current code formulas for estimating the fundamental period of concrete shear wall buildings are grossly inadequate. Subsequently, an improved formula is developed by calibrating a theoretical formula, derived using Dunkerley's method, against the measured period data through regression analysis. Also recommended is a factor to limit the period calculated by a "rational" analysis, such as Rayleigh’s method.

INTRODUCTION

The fundamental vibration period of a building appears in the equation specified in building codes to calculate the design base shear and lateral forces. Because this building property cannot be computed for a structure that is yet to be designed, building codes provide empirical formulas that depend on the building material [steel, reinforced concrete (RC), etc.], building type (frame, shear wall, etc.), and overall dimensions. The empirical period formulas for concrete shear-wall (SW) buildings in the 1997 UBC ("Uniform" 1997) and the 1996 SEAOC blue book ("Recommended" 1996) were derived by modifying the ATC3-06 formulas ("Tentative" 1978) during development of the 1988 SEAOC blue book to more accurately reflect the configuration and material properties of these systems ("Recommended" 1988, Appendix 1E2b(1)-T). The period formulas in ATC3-06 ("Tentative" 1978) are based largely on motions of buildings recorded during the 1971 San Fernando earthquake. However, motions of many more buildings recorded during recent earthquakes, including the 1989 Loma Prieta and 1994 Northridge earthquakes, are now available. These recorded motions provide an opportunity to expand greatly the existing database on the fundamental vibration periods of buildings. To this end, the natural vibration periods of 21 buildings have been measured by system identification methods applied to the motions of buildings recorded during the 1994 Northridge earthquake (Goel and Chopra 1997a). These data have been combined with similar data from the motions of buildings recorded during the 1971 San Fernando, 1984 Morgan Hill, 1986 Mt. Lewis and Palm Spring, 1987 Whittier, 1989 Loma Prieta, 1990 Upland, and 1991 Sierre Madre earthquakes.

The objective of this paper is to develop improved empirical formulas to estimate the fundamental vibration period of concrete SW buildings for use in equivalent lateral force analysis specified in building codes. Presented first is the expanded database for "measured" values of fundamental periods of SW buildings, against which the code formulas in present U.S. codes are evaluated; similar work on limited data sets has appeared previously (e.g., Arias and Husid 1962; Housner and Brady 1963; Cole et al. 1992; Li and Mau 1997). It is shown that current code formulas for estimating the fundamental period of concrete SW buildings are grossly inadequate. Subsequently, an improved formula is developed by calibrating a theoretical formula, derived using Dunkerley's method, against the measured period data through regression analysis. Finally, a factor to limit the period calculated by a "rational" analysis, such as Rayleigh's method, is recommended.

PERIOD DATABASE

The data that are most useful, but hard to come by, are from structures shaken strongly but not deformed into the inelastic range. Such data are slow to accumulate because relatively few structures are installed with permanent accelerographs, and earthquakes causing strong motions of these instrumented buildings are infrequent. Thus, it is very important to investigate comprehensively the recorded motions when they do become available, such as during the 1994 Northridge earthquake. Unfortunately, this obviously important goal is not always accomplished, as indicated by the fact that the vibration properties of only a few of the buildings whose motions were recorded during post-1971 earthquakes have been determined. Available data on the fundamental vibration period of buildings measured from their motions recorded during several California earthquakes have been collected (Goel and Chopra 1997a). This database contains data for 106 buildings, including 21 buildings that experienced peak ground acceleration, \( \mu_g \geq 0.15 \) during the 1994 Northridge earthquake. The remaining data come from motions of buildings recorded during the 1971 San Fernando earthquake and subsequent earthquakes (Hart et al. 1975; Hart and Vasudevan 1975; MacVerry 1979; Cole et al. 1992; Werner 1992; Gates et al. 1994; Marshall et al. 1994; Goel and Chopra 1996, 1997a).

Shown in Table 1 is the subset of this database pertaining to 16 concrete SW buildings (27 data points); buildings subject to peak ground acceleration, \( \mu_g \geq 0.15 \) are identified with an asterisk (*). "C" and "N" denote buildings instrumented by the California Strong Motion Instrumentation Program (CSMIP) and National Oceanic and Atmospheric Administration (NOAA) and "ATC" denotes one of the buildings included in the ATC3-06 report ("Tentative" 1978) for which the height and base dimensions were available from other sources, but these dimensions for other buildings could not be discerned from the plot presented in the ATC3-06 report. The number of data points exceeds the number of buildings, because the period of some buildings was determined from their motions recorded during more than one earthquake or was reported by more than one investigator for the same earthquake.

CODE FORMULAS

The empirical formula for the fundamental vibration period of concrete SW buildings specified in current U.S. building codes NEHRP-94 ("NEHRP" 1994) SEAOC-96 ("Recom-
In the direction under consideration, shear should be calculated from

\[ T = C_i H^{1/4} \]  

(1)

where \( H \) is the height of the building in feet above the base; and the numerical coefficient \( C_i = 0.02 \). UBC-97 and SEAOC-96 permit an alternative value for \( C_i \), to be calculated from

\[ C_i = 0.1\sqrt{A_c} \]  

(2)

where \( A_c \), the combined effective area (in square feet) of the shear walls, is defined as

\[ A_c = \sum_{i=1}^{nw} A_i (0.2 + (D_i/H_i)^2) \]

\[ D_i/H_i \leq 0.9 \]  

(3)

in which \( A_i \) is the horizontal cross-sectional area (in square feet); \( D_i \) is the dimension in the direction under consideration (in feet) of the \( i \)th SW in the first story of the structure; and \( NW \) is the total number of shear walls. The value of \( D_i/H \) in (3) should not exceed 0.9.

ATC-3-06 ("Tentative" 1978) and earlier versions of other U.S. codes specify a different formula

\[ T = 0.05H \sqrt{D} \]  

(4)

where \( D \) is the dimension, in feet, of the building at its base in the direction under consideration.

UBC-97 and SEAOC-96 codes specify that the design base shear should be calculated from

\[ V = CW \]  

(5)

in which \( W \) is the total seismic dead load; and \( C \) is the seismic coefficient defined as

\[ C = \frac{C_v}{R} \frac{I}{T}; \quad \frac{0.11C_vI}{R} \leq C \leq \frac{2.5C_vI}{R}; \]

and for seismic zone 4 \( C \geq \frac{0.82ZNC_vI}{R} \)  

(6)

in which coefficients \( C_v \) and \( C_a \) depend on the near-source factors, \( N_0 \) and \( N_a \), respectively, along with the soil profile and the seismic zone factor \( Z \); \( I \) is the importance factor; and \( R \) is the numerical coefficient representative of the inherent overstrength and global ductility capacity of the lateral-load resisting system. The upper limit of 2.5 \( C_vI + R \) on \( C \) applies to very short period buildings, whereas the lower limit of 0.11 \( C_vI \) (or 0.82 \( ZNC_vI + R \) for seismic zone 4) applies to very long period buildings. These limits imply that \( C \) becomes independent of the period for very short or very tall buildings. The upper limit existed, although in slightly different form, in previous versions of UBC and SEAOC blue book; however, the lower limit appeared only recently in UBC-97 and SEAOC-96.

The fundamental period \( T \), calculated using the empirical formula (1) or (4), should be smaller than the "true" period to obtain a conservative estimate for the base shear. Therefore, code formulas are intentionally calibrated to underestimate the period by about 10–20% at first yield of the building ("Tentative" 1978; "Recommended" 1988). The codes permit calculation of the period by established methods of mechanics (referred to as rational analyses in this paper), such as Rayleigh's method or computer-based eigenvalue analysis, but specify that the resulting value should not

### TABLE 1. Period Data for Concrete SW Buildings

<table>
<thead>
<tr>
<th>Building number</th>
<th>Location</th>
<th>ID number</th>
<th>Number of stories</th>
<th>Height (ft)</th>
<th>Earthquake</th>
<th>Peak Ground Acceleration (g)</th>
<th>Period T (sec)</th>
<th>Width (ft)</th>
<th>Length (ft)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Belmont</td>
<td>C8268</td>
<td>2</td>
<td>28.0</td>
<td>Loma Prieta</td>
<td>0.10</td>
<td>0.13</td>
<td>NA</td>
<td>NA</td>
</tr>
<tr>
<td>2*</td>
<td>Burbank</td>
<td>C24335</td>
<td>10</td>
<td>28.0</td>
<td>Northridge</td>
<td>0.10</td>
<td>0.13</td>
<td>NA</td>
<td>NA</td>
</tr>
<tr>
<td>3*</td>
<td>Burbank</td>
<td>C24336</td>
<td>10</td>
<td>28.0</td>
<td>Whittier</td>
<td>0.10</td>
<td>0.13</td>
<td>NA</td>
<td>NA</td>
</tr>
<tr>
<td>4</td>
<td>Hayward</td>
<td>C8488</td>
<td>4</td>
<td>50.0</td>
<td>Loma Prieta</td>
<td>0.10</td>
<td>0.13</td>
<td>NA</td>
<td>NA</td>
</tr>
<tr>
<td>5</td>
<td>Long Beach</td>
<td>C14311</td>
<td>5</td>
<td>71.0</td>
<td>Whittier</td>
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<td>0.13</td>
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<td>NA</td>
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<td>6</td>
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<td>ATC3</td>
<td>12</td>
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<td>San Fernando</td>
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<td>0.13</td>
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<td>0.13</td>
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<td>8*</td>
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<td>C24601</td>
<td>17</td>
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<td>Northridge</td>
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<td>0.13</td>
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<td>NA</td>
</tr>
<tr>
<td>9</td>
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<td>C24601</td>
<td>17</td>
<td>149.7</td>
<td>Sierra Madre</td>
<td>0.10</td>
<td>0.13</td>
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<td>NA</td>
</tr>
<tr>
<td>10*</td>
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<td>N235-5</td>
<td>12</td>
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<td>0.13</td>
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<td>NA</td>
</tr>
<tr>
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<td>San Fernando</td>
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<td>0.13</td>
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<td>NA</td>
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<tr>
<td>12</td>
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<td>Palm Spring</td>
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<td>0.13</td>
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<tr>
<td>13</td>
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<td>Lytle Creek</td>
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<td>0.13</td>
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<td>NA</td>
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<td>N265-5</td>
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<td>San Fernando</td>
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<td>0.13</td>
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<td>NA</td>
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<tr>
<td>15*</td>
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<td>N265-5</td>
<td>10</td>
<td>142.0</td>
<td>San Fernando</td>
<td>0.10</td>
<td>0.13</td>
<td>NA</td>
<td>NA</td>
</tr>
<tr>
<td>16</td>
<td>Piedmont</td>
<td>C8334</td>
<td>3</td>
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<td>Loma Prieta</td>
<td>0.08</td>
<td>0.18</td>
<td>NA</td>
<td>NA</td>
</tr>
<tr>
<td>17</td>
<td>Pleasant Hill</td>
<td>C8348</td>
<td>3</td>
<td>40.6</td>
<td>Loma Prieta</td>
<td>0.08</td>
<td>0.18</td>
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<td>NA</td>
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<td>18</td>
<td>San Bruno</td>
<td>C8394</td>
<td>9</td>
<td>104.0</td>
<td>Loma Prieta</td>
<td>0.11</td>
<td>0.18</td>
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<td>NA</td>
</tr>
<tr>
<td>19</td>
<td>San Bruno</td>
<td>C8394</td>
<td>9</td>
<td>104.0</td>
<td>Loma Prieta</td>
<td>0.11</td>
<td>0.18</td>
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<td>NA</td>
</tr>
<tr>
<td>20</td>
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<td>C75355</td>
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<td>124.0</td>
<td>Loma Prieta</td>
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<td>0.18</td>
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<td>NA</td>
</tr>
<tr>
<td>21</td>
<td>San Jose</td>
<td>C75355</td>
<td>10</td>
<td>124.0</td>
<td>Morgan Hill</td>
<td>0.06</td>
<td>0.18</td>
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<td>NA</td>
</tr>
<tr>
<td>22</td>
<td>San Jose</td>
<td>C75355</td>
<td>10</td>
<td>124.0</td>
<td>Mount Lewis</td>
<td>0.03</td>
<td>0.18</td>
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<td>NA</td>
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<tr>
<td>23</td>
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<td>C75356</td>
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<td>96.0</td>
<td>Loma Prieta</td>
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<td>0.20</td>
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<td>NA</td>
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<td>24</td>
<td>San Jose</td>
<td>C75356</td>
<td>10</td>
<td>96.0</td>
<td>Loma Prieta</td>
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<td>0.20</td>
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<td>NA</td>
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<td>25</td>
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<td>C75356</td>
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<td>96.0</td>
<td>Loma Prieta</td>
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<td>0.20</td>
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<td>NA</td>
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<td>26</td>
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<td>27*</td>
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<td>0.20</td>
<td>NA</td>
<td>NA</td>
</tr>
</tbody>
</table>

Note: *Denotes building with \( u_c \geq 0.15 \); NA indicates data not available; MRF implies moment-resisting frames form the lateral load resisting system; number followed by "C" or "N" indicates the station number and by "ATC" indicates the building number in ATC3-06 report ("Tentative" 1978).
be longer than that estimated from the empirical formula (1) or (4) by a certain factor. The factors specified in various U.S. codes are 1.2 in ATC3-06, 1.3 for high seismic region (Zone 4) and 1.4 for other regions (Zones 3, 2, and 1) in UBC-97 and SEAOC-96, and a range of values with 1.2 for regions of high seismicity to 1.7 for regions of very low seismicity in NEHRP-94. The restriction in SEAOC-88 that the base shear calculated using the rational period shall not be less than 80% of the value obtained by using the empirical period corresponds to a factor of 1.4 (Cole et al. 1992). These restrictions are imposed to safeguard against unreasonable assumptions in the rational analysis, which may lead to unreasonably long periods and hence unconservative values of base shear.

**EVALUATION OF CODE FORMULAS**

For buildings listed in Table 1, the fundamental period identified from their motions recorded during earthquakes (subsequently denoted as “measured” period) is compared with the values given by the code empirical formulas [Figs. 1(a), 2(a), and 3(a)]. Also compared are the two values of the seismic coefficient for each building calculated according to (6), with \( l = 1 \) for standard occupancy structures; \( R = 5.5 \) for concrete shear walls; and \( C_v = 0.64 \) and \( C_v = 0.44 \) for seismic zone 4 with \( Z = 0.4 \), soil profile type \( S_m \), i.e., stiff soil profile with average shear wave velocity between 180 and 360 m/s, and \( N_c = N_s = 1 \) [Figs. 1(b), 2(b), 3(b)].

**Code Formula: (1) with \( C_v = 0.02 \)**

For all buildings in Table 1, the periods and seismic coefficients are plotted against the building height in Fig. 1. The measured periods in two orthogonal directions are shown by circles (solid for \( u_{m} \geq 0.15g \), open for \( u_{m} < 0.15g \)) connected by a vertical line, whereas the code period is shown by a solid curve because the code formula gives the same period in the two directions if the lateral-force resisting systems are of the same type. Also included are the curves for 1.27 and 1.47, representing the limits imposed by codes on a rational value of the period for use in high seismic regions like California. The seismic coefficients (6) corresponding to the measured periods in the two orthogonal directions are also shown by circles connected by a vertical line, whereas the value based on the code period is shown by a solid curve.

Fig. 1 leads to the following observations. For a majority of buildings, the code formula gives a period longer than the measured value. In contrast, for concrete and steel moment-resisting frame buildings, the code formula almost always gives a period shorter than measured value (Goel and Chopra 1996, 1997b). The longer period from the code formula leads to seismic coefficients smaller than the value based on the
measured period if the period falls outside the flat portion of the seismic coefficient spectrum; otherwise, the two periods lead to the same seismic coefficient. For most of the remaining buildings, the code formula gives a period much shorter than the measured value and a seismic coefficient much larger than the value based on the measured period. Because the code period for many buildings is longer than the measured period, limits of 1.2T or 1.4T for the period calculated from a rational analysis are obviously inappropriate.

The building height alone is not sufficient to estimate accurately the fundamental period of SW buildings because measured periods of buildings with similar heights can be very different, whereas they can be similar for buildings with very different heights. For example, in Table 1 the measured longitudinal periods of Buildings 4 and 12 of nearly equal heights differ by a factor of more than three; the heights of these buildings are 50 ft and 50.2 ft, whereas the periods are 0.15 sec and 0.50 sec, respectively. On the other hand, measured longitudinal periods of Buildings 13 and 23 are close even though Building 13 is 50% taller than Building 23; periods of these buildings are 0.71 sec and 0.73 sec, whereas the heights are 142 ft and 96 ft, respectively. The poor correlation between the building height and the measured period is also apparent from the significant scatter of the measured period data [Fig. 1(a)].

Alternate Code Formula: (1) with \( C \), from (2) and (3)

Table 2 lists a subset of nine buildings (17 data points) with their \( \alpha_c \) values calculated from (3) using SW dimensions obtained from structural drawings; for details, see Appendix G of Goel and Chopra (1997a). These dimensions were not available for the remaining seven buildings in Table 1.

In Fig. 2 the alternate code formula for estimating the fundamental period is compared with the measured periods of the nine buildings. The code period is determined from (1)–(3) using the calculated value of \( \alpha_c \) and plotted against \( H + \sqrt{D} \). This comparison shows that the alternate code formula almost always gives a value for the period that is much shorter than the measured periods and a value for the seismic coefficient that is much higher than from the measured periods. The measured periods of most buildings are longer than the code imposed limits of 1.2T and 1.4T on the period computed from a rational analysis. Although the code period formula gives a conservative value for the seismic coefficient, the degree of conservatism seems excessive for most buildings considered in this investigation.

ATC3-06 Formula

In Fig. 3, the ATC3-06 formula for estimating the fundamental period is compared with the measured periods of all buildings listed in Table 1. The code period is determined from (4) using the \( H \) and \( D \) dimensions of the building (Table 1) and plotted against \( H + \sqrt{D} \). This comparison demonstrates that (4) significantly underestimates the period and considerably overestimates the seismic coefficient for many buildings and the ATC3-06 imposed limit of 1.2T is too restrictive.

The ratio \( H + \sqrt{D} \) is not sufficient to estimate accurately the fundamental period of concrete SW buildings because measured periods of buildings with similar values of this ratio can be very different, whereas they can be similar for buildings with very different values of \( H + \sqrt{D} \). For example, in Table 1 the measured transverse period of Building 18 and measured longitudinal period of building 27—two buildings with similar values of \( H + \sqrt{D} \)—differ by nearly a factor of five; \( H + \sqrt{D} = 7.51 \) and 7.87, and measured periods were 1.30 sec and 0.24 sec, respectively. On the other hand, the measured longitudinal and transverse periods of Building 9 are the same, equal to 1 sec, even though the values of \( H + \sqrt{D} \) in the two directions are 16.7 and 9.93. The poor correlation between the ratio \( H + \sqrt{D} \) and the measured periods is also apparent from a large scatter of the measured period data [Fig. 3(a)].

THEORETICAL FORMULAS

The observations in the preceding section clearly indicate that the current code formulas for estimating the fundamental period of concrete SW buildings are grossly inadequate. For this purpose, equations for the fundamental period are derived using established analytical procedures. Based on Dunkerley's method (Jacobsen and Ayre 1958, pages 119–120 and 502–505; Veletsos and Yang 1977; Inman 1996, pages 442–449), the fundamental period of a cantilever, considering flexural and shear deformations, is

\[
T = \sqrt{T_f^2 + T_s^2}
\]  

in which \( T_f \) and \( T_s \) are the fundamental periods of pure-flexural and pure-shear cantilevers, respectively. For uniform cantilevers \( T_f \) and \( T_s \) are given by (Jacobsen and Ayre 1958, pages 471–496; Timoshenko et al. 1974, pages 424–431; Chopra 1995, page 592)

\[
T_f = \frac{2\pi}{3.516} \sqrt{\frac{m}{EI}} H^0
\]  

(8)
TABLE 2. Measured Periods and Areas of Selected Concrete SW Buildings

<table>
<thead>
<tr>
<th>Building number</th>
<th>ID number</th>
<th>Height (ft)</th>
<th>Measured Period</th>
<th>( A_i ) (sq ft)</th>
<th>( A_i ) (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(1)</td>
<td>(2)</td>
<td>(3)</td>
<td>(4)</td>
<td>(5)</td>
<td>(6)</td>
</tr>
<tr>
<td>1*</td>
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<td>88.0</td>
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<td>0.56</td>
<td>83.5</td>
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<td>0.57</td>
<td>0.51</td>
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</tr>
<tr>
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<td>C24468</td>
<td>127.0</td>
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<td>1.62</td>
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</tr>
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<td>4*</td>
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<td>1.00</td>
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<tr>
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<tr>
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<td>96.0</td>
<td>0.63</td>
<td>0.41</td>
<td>60.7</td>
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</table>

Note: * Denotes buildings with \( \mu_e \approx 0.15 \text{ g} \); MRF implies moment-resisting frames form the lateral load resisting system; number followed by "C" indicates the station number.

In (8) and (9), \( m = \text{mass per unit height}; \ E = \text{modulus of elasticity}; G = \text{shear modulus}; I = \text{section moment of inertia}; A = \text{section area}; and \( \kappa \) is the shape factor to account for nonuniform distribution of shear stresses (=5/6 for rectangular sections). Combining (7) to (9) and recognizing that \( G = E + 2(1 + \mu) \), where the Poisson's ratio \( \mu = 0.2 \) for concrete, leads to

\[
T = 4 \sqrt{\frac{m}{kG} A} \quad \text{(9)}
\]

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\[
T = 4 \sqrt{\frac{m}{kG} A} \quad \text{(10)}
\]

with

\[
A_i = \frac{A}{1 + 0.83 \left( \frac{H}{D} \right)^2} \quad \text{(11)}
\]

where \( D \) is the plan dimension of the cantilever in the direction under consideration. Comparing (10) and (11) with (9) reveals that the fundamental period of a cantilever considering flexural and shear deformations may be computed by replacing the area \( A \) in (9) with the equivalent shear area \( A_i \) given by (11).

The period \( T \) from (10) normalized by \( T_r \) is plotted in Fig. 4 against the ratio \( H/D \) on a logarithmic scale. Also shown is the period of a pure-shear cantilever and of a pure-flexural cantilever. Eq. (10) approaches the period of a pure-shear cantilever (9) as \( H/D \) becomes small and the period of a pure-flexural cantilever (8) for large values of \( H/D \). For all practical purposes, the contribution of flexure can be neglected for SWs with \( H/D \leq 0.2 \), whereas the contribution of shear can be neglected for SWs with \( H/D > 5 \); the resulting error is less than 2%. However, both shear and flexural deformations should be included for shear walls with \( 0.2 \leq H/D \leq 5 \).

Eq. (10), based on Dunkerley’s method, provides a highly accurate value for the true fundamental period of a shear-flexural cantilever. This can be demonstrated by recognizing that the exact period is bounded by the periods obtained from Dunkerley’s and Rayleigh’s methods; Dunkerley’s method gives a period longer than the exact value (Jacobsen and Ayre 1938, pages 113–120; Inman 1996, pages 442–449), whereas Rayleigh’s method provides a shorter period (Chopra 1995, page 554). Also shown in Fig. 4 is the period determined by Rayleigh’s method using the deflected shape due to lateral forces varying linearly with height, considering both shear and flexural deformations; details are available in Appendix G of Goel and Chopra (1997a). The resulting period is very close to that obtained from (10), derived using Dunkerley’s method; the difference between the two periods is no more than 3%. Since the exact period lies between the two approximate values, (10) errs by less than 3%.

Now consider a class of symmetric-plan buildings—symmetric in the lateral direction considered—with a lateral-force resisting system comprised of a number of uncoupled (i.e., without coupling beams) SWs connected through rigid floor diaphragms. Assuming that the stiffness properties of each wall are uniform over its height, the equivalent shear area, \( A_i \), is given by a generalized version of (11) (details available in Goel and Chopra 1997a, Appendix G)

\[
A_i = \sum_{i=1}^{n} \left( \frac{H_i}{H} \right)^2 \left[ \frac{A_i}{1 + 0.83 \left( \frac{H_i}{D_i} \right)^2} \right] \quad \text{(12)}
\]

where \( A_i, H_i, \) and \( D_i \) are the area, height, and dimension in the
direction under consideration of the i-th SW; and NW = the number of shear walls. With A, so defined, (10) is valid for a system of SWs of different height.

Eq. (10) is now expressed in a form convenient for buildings

\[ T = 40 \sqrt{\frac{p}{\kappa k G}} \frac{1}{\sqrt{A_i}} H \]  

(13)

where \( p = \) average mass density, defined as the total building mass (=mH) divided by the total building volume (=A_sH−A_a is the building plan area), i.e., \( p = m/A_s \); and \( A_s = \) the equivalent shear area expressed as a percentage of \( A_a \), i.e.,

\[ \bar{A}_s = 100 \frac{A_s}{A_a} \]  

(14)

Eq. (13) applies only to those buildings in which lateral load resistance is provided by uncoupled SWs. Theoretical formulas for the fundamental period of buildings with coupled SWs are available in Rutenberg (1975), and for buildings with a combination of SWs and moment-resisting frames in Heidebrecht and Stafford-Smith (1973) and Stafford-Smith and Crowe (1986). It seems that these formulas can not be simplified to the form of (13).

Sozen (1989) and Wallace and Moehle (1992) also presented a formula for the fundamental vibration period of SW buildings. Their formula was developed based on pure-flexural cantilever idealization of SW buildings and ignored the influence of shear deformations. Furthermore, the numerical constant in their formula was determined based on assumed material properties and effective member stiffness equal to one-half its initial value. In contrast, the formula developed in this paper (13) includes both flexural and shear deformations and the numerical constant is determined directly from regression analysis of measured period data as described in the following sections.

**REGRESSION ANALYSIS METHOD**

Although \( C = 40\sqrt{\frac{p}{\kappa k G}} \) in (13) can be calculated from building properties, it is determined from regression analysis to account for variations in properties among various buildings and for differences between building behavior and its idealization. For this purpose, it is useful to write (13) as

\[ T = C \frac{1}{\sqrt{A}} H \]  

(15)

and recast it as

\[ y = a + x \]  

(16)

in which \( y = \log(T) \); \( a = \log(C) \); and \( x = \log(H + \sqrt{A}) \). The intercept \( a \) at \( x = 0 \) of the straight line in (16) was determined by minimizing the squared error between the measured and computed periods, and then \( C \) was back-calculated from the relationship \( a = \log(C) \). The standard error of estimate is

\[ s = \sqrt{\frac{\sum_{i=1}^{n} (y_i - (a + x_i))^2}{n - 2}} \]  

(17)

in which \( y_i = \log(T_i) \) is the observed value (with \( T_i = \) measured period) and \((a + x_i) = \log(C) + \log(H + \sqrt{A})\) is the computed value of the \( i \)-th data; and \( n = \) the total number of data points. \( s \), represents scatter in the data and approaches, for large \( n \), the standard deviation of the measured period data from the best-fit equation.

This procedure leads to the value of \( \hat{C} \) for (15) to represent the best-fit, in the least-squared sense, to the measured period data. However, for code applications the formula should provide a lower value of the period and this was obtained by lowering the best-fit line (16) by \( s \), without changing its slope. Thus \( \hat{C}_t \), the lower value of \( C \), is computed from

\[ \log(\hat{C}_t) = \log(\hat{C}_a) - s \]  

(18)

Because \( s \), approaches the standard deviation for a large number of samples and \( y \) is lognormal, \( \hat{C}_t \) is the mean-minus-one-standard deviation or 15.9 percentile value, implying that 15.9% of the measured periods would fall below the curve corresponding to \( \hat{C}_t \) (subsequently referred to as the best-fit − 1\( \sigma \) curve). If desired, \( \hat{C}_t \) corresponding to other non-exceedance probabilities may be selected. Additional details of the regression analysis method and the procedure to estimate \( \hat{C}_t \) are available elsewhere (Goel and Chopra 1997a, Appendix F).

As mentioned previously, codes also specify an upper limit on the period calculated by a rational analysis. This limit is established in this investigation by raising the best-fit line (16) by \( s \), without changing its slope. Thus, \( \hat{C}_T \) the upper value of \( C \) corresponding to the upper limit, is computed from

\[ \log(\hat{C}_T) = \log(\hat{C}_a) + s \]  

(19)

Eq. (15) with \( \hat{C}_T \) represents the best-fit + 1\( \sigma \) curve, which will be exceeded by 15.9% of the measured periods.

Regression analysis in the log-log space (16) is preferred over the direct regression on (15) because it permits convenient development of the best-fit − 1\( \sigma \) and best-fit + 1\( \sigma \) curves; both regression analyses give essentially identical values of \( \hat{C}_T \).

**RESULTS OF REGRESSION ANALYSIS**

The formula for estimating the fundamental period of concrete SW buildings was obtained by calibrating the theoretical formula of (15) by regression analysis of the measured period data for the nine concrete SW buildings (17 data points) listed in Table 2. For each building, the equivalent area \( \bar{A}_s \) was calculated from (12) and (14) using dimensions from structural plans (Goel and Chopra 1997a, Appendix H); for SWs with dimensions varying over height, \( A_i \) and \( D \), were taken as the values at the base. Regression analysis gives \( \hat{C}_a = 0.0023 \) and \( \hat{C}_T = 0.0018 \). Using these values for \( C \) in (15) give \( T_a \) and \( T_t \), the best-fit and best-fit − 1\( \sigma \) values of the period, respectively. These period values are plotted against \( H + \sqrt{A} \) in Fig. 5; together with the measured periods shown in circles; the mea-

![FIG. 5. Results of Regression Analysis: All Buildings](image-url)
8 in. (at mid-height), and 7 in. (at the roof), and substituting in (20) gives period values 0.36 sec, 0.42 sec, and 0.45 sec, respectively. Although the mid-height value of $D_t$ gives the period value close to the measured period (0.41–0.43 sec, by different investigators), the base value of $D_t$ provides a shorter period, leading to a conservative value of base shear. This recommendation is consistent with the current codes ("Recommended" 1996; "Uniform" 1997).

CONCLUSIONS AND RECOMMENDATIONS

Based on the analysis of the available data for the fundamental vibration period of nine concrete SW buildings (17 data points), measured from their motions recorded during earthquakes, (20), with $A_t$ calculated from (12) and (14) using wall dimensions at the base, is recommended for conservatively estimating the fundamental period of concrete SW buildings. This formula provides the "best" fit of (15) to the available data; the fit is better than possible from formulas (1–3) in current U.S. codes. Furthermore, the period from rational analysis should not be allowed to exceed the value from the recommended equation by a factor larger than 1.4. Because these recommendations are developed based on data from buildings in California, they should be applied with discretion to buildings in less seismic regions of the United States or other parts of the world where building design practice is significantly different than in California.

Regression analyses led to the recommended formulas should be repeated periodically on larger data sets. The database can be expanded by including buildings, other than those in Tables 1 and 2, whose motions recorded during past earthquakes have, so far, not been analyzed. Period data should also be developed for additional buildings when records of their motions during future earthquakes become available.

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APPENDIX. REFERENCES


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