

Probabilistic Liquefaction Triggering based on the Cone Penetration Test

R. E. S. Moss¹, R. B. Seed², R. E. Kayen³, J. P. Stewart⁴, and K. Tokimatsu⁵

¹Project Engineer, Fugro West, Inc., Ventura, CA; email: rross@fugro.com

²Prof., Dept. Civil and Environmental Engineering, U.C. Berkeley.

³Researcher, US Geological Survey, Menlo Park.

⁴Assoc. Prof., Dept. Civil and Environmental Engineering, U.C. Los Angeles.

⁵Prof., Dept. Civil Engineering and Architecture, Tokyo Institute of Technology.

Abstract

Performance-based earthquake engineering requires a probabilistic treatment of potential failure modes in order to accurately quantify the overall stability of the system. This paper is a summary of the application portions of the probabilistic liquefaction triggering correlations proposed recently proposed by Moss and co-workers. To enable probabilistic treatment of liquefaction triggering, the variables comprising the seismic load and the liquefaction resistance were treated as inherently uncertain. Supporting data from an extensive Cone Penetration Test (CPT)-based liquefaction case history database were used to develop a probabilistic correlation. The methods used to measure the uncertainty of the load and resistance variables, how the interactions of these variables were treated using Bayesian updating, and how reliability analysis was applied to produce curves of equal probability of liquefaction are presented. The normalization for effective overburden stress, the magnitude correlated duration weighting factor, and the non-linear shear mass participation factor used are also discussed.

Introduction

Correlations based on *in situ* index tests are widely used in engineering practice to estimate the potential for liquefaction triggering. The CPT is a reliable *in situ* index test that has found widespread use as a tool for measuring resistance of potentially liquefiable layers. CPT-based liquefaction triggering curves have been suggested by previous researchers (e.g., Shibata & Teparaska, 1988; Seed & De Alba, 1986; Mitchell & Tseng, 1990; Stark & Olson, 1995; Suzuki et al., 1995; Robertson & Campanella, 1985; Robertson & Wride, 1998; Toprak et al., 1999; and Juang et al., 2003). For use in performance-based engineering analysis the triggering correlations must be presented in a probabilistic manner.

This paper summarizes the recent CPT-based probabilistic liquefaction triggering correlations proposed in Moss et al. (2004), portions of which have been presented in Seed et al., (2003) and Moss and Seed (2004). The purpose of this research was to provide as unbiased an assessment of liquefaction triggering as possible using a comprehensive worldwide CPT-based liquefaction case history database compiled for this purpose (Moss et al., 2003).

Careful consideration was given to processing the empirical data. The uncertainties associated with the various load and resistance parameters were quantified using different

statistical techniques. Normalization of the CPT for effective overburden stress was readdressed, applying cavity expansion methods to a previous empirically-based normalization technique.

A Bayesian framework allowed for careful and thorough treatment of all types of uncertainties associated with the vagaries of observed liquefaction/non-liquefaction. This Bayesian framework used structural reliability methods to estimate the probability of liquefaction. The results are curves of equal probability of seismic liquefaction triggering which can be used in performance-based engineering decisions.

Threshold of Liquefaction Triggering

The threshold of liquefaction triggering, or the liquefaction/non-liquefaction boundary, has traditionally been located deterministically by researchers. Based on the position and spread of the liquefaction and non-liquefaction data points, a curve was drawn showing the best estimate of the threshold of liquefaction triggering. In this study the threshold was located using engineering statistics, Bayesian updating, and reliability methods that were formulated for this particular problem (Cetin et al., 2002; Moss et al., 2003).

Figure 1 is a plot of the liquefaction and non-liquefaction data with error bars showing ± 1 standard deviation. The resistance is represented by the normalized CPT tip resistance ($q_{c,l}$) in megapascals (MPa). The load is represented by the equivalent uniform cyclic stress ratio (CSR) as calculated using the simplified technique first proposed by Seed and Idriss (1971);

$$CSR = \frac{\tau_{avg}}{\sigma'_v} = 0.65 \cdot \frac{a_{max}}{g} \cdot \frac{\sigma_v}{\sigma'_v} \cdot r_d \quad (1)$$

In the analysis of the sites that comprise the database of the present model, the equivalent uniform cyclic stress ratio was assumed to be the average or mean of a normally distributed random variable, which can be rewritten as Equation 2. The variance of CSR can be calculated using Equation 3, where the coefficient of variation (δ) is the normalized standard deviation, equal to the standard deviation (σ) divided by the mean (μ). Both Equation 2 and 3 are derived using a first-order Taylor series expansions about the mean point, including only the first two terms.

$$\mu_{CSR} \cong 0.65 \cdot \frac{\mu a_{max}}{g} \cdot \frac{\mu \sigma_v}{\mu \sigma'_v} \cdot \mu r_d \quad (2)$$

$$\delta_{CSR}^2 \cong \delta_{a_{max}}^2 + \delta_{r_d}^2 + \delta_{\sigma_v}^2 + \delta_{\sigma'_v}^2 - 2 \cdot \rho_{\sigma_v \sigma'_v} \cdot \delta_{\sigma_v} \cdot \delta_{\sigma'_v} \quad (3)$$

Equation 3 indicates that the variance of the cyclic stress ratio (CSR), the dependent variable, is a function of the variance and covariance of the independent variables, maximum ground acceleration (a_{max}), total and effective vertical stress (σ_v and σ'_v), and nonlinear shear mass participation factor (r_d). In this study all variables were assumed to be normally distributed and statistically independent unless otherwise noted. Total and effective stress are correlated variables, therefore the correlation coefficient term ($\rho_{\sigma_v \sigma'_v}$) for these two variables was included.

Estimating the variance of the all the independent variables was performed using the most appropriate statistical techniques (i.e., for total and effective stress a Taylor-series expansion, for a_{max} a rational equation based on the quality of the available strong motion data, for moment magnitude a relationship fitted to various reported event magnitudes, and for r_d a statistical analysis by Cetin et al., 2004). A thorough discussion of these statistical techniques can be found in Moss et al. (2004).

The variance of the resistance, $q_{c,1}$ and R_f , was found by calculating the standard deviation of the tip and sleeve measurements throughout the depth of the critical layer. The critical layer was defined as the layer estimated to be the most eminently liquefiable; the layer that either was observed to have liquefied or thought to be the most susceptible to liquefaction. A thorough discussion of critical layer selection and related issues can be found in Moss et al. (2004). All resistance variables were also assumed to be normally distributed and statistically independent unless otherwise noted.

As seen in Figure 1 the variance of the load tends to be greatest in the high CSR range and the variance of the resistance tends to greatest in the high $q_{c,1}$ range. The region where liquefaction and non-liquefaction data points merge can be thought of as a “mixing” zone. In this zone lies the most likely threshold of liquefaction triggering.

Bayesian Framework

Thus far the discussion has outlined the data processing of liquefaction/non-liquefaction case histories; the steps for estimating means and standard deviations of the independent and dependent variables. A great deal of time and effort was invested in the data collection and processing because a correlation is only as good as the quality of its data. The next step was to evaluate the processed data as a whole and develop a correlation

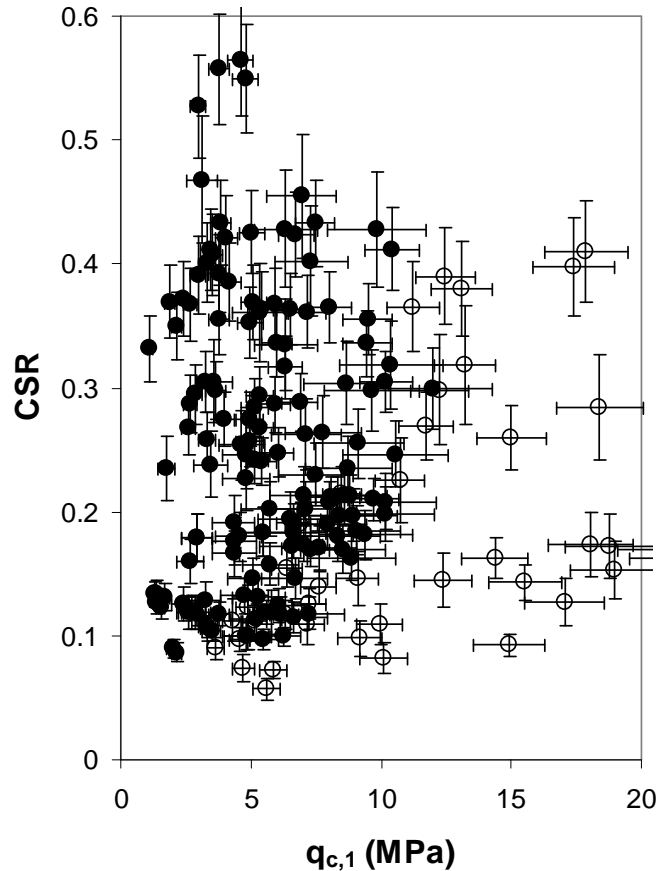


Figure 1. Plot showing liquefaction (dots) and non-liquefaction (circles) data with ± 1 standard deviation error bars, from Moss and Seed (2003).

between the load and resistance variables with respect to observed liquefaction/non-liquefaction.

A Bayesian framework using structural reliability methods was used to develop the correlation. A full discussion of the application of Bayesian methods to liquefaction triggering analysis can be found in Cetin et al. (2002), and Moss et al. (2003). In summary; Bayes rule was used as the foundation of the probabilistic analysis, a likelihood function was formulated to describe the observations of liquefaction/non-liquefaction, a limit-state function was formulated to define the liquefaction/non-liquefaction threshold, Bayesian updating was used to determine the distribution of the unknown model parameters in the limit-state function, and component reliability analysis was used to assess the probability of liquefaction based on the limit-state function with the posterior model parameter distributions. This process can be thought of as a regression-type procedure that has been designed to incorporate all forms of parameter uncertainty as well as model uncertainty, thereby producing a “best” estimate of the means and variances of liquefaction triggering.

Data Screening, Adjustment, and Correction

A thorough and proper treatment of the data required different methods of screening, adjustment, and correction. A revised screening procedure, akin to the “Modified Chinese Criteria” (Wang, 1979; Seed and Idriss, 1982) was used. Presented are corrections to normalize the resistance measurements for effective overburden stress and corrections to *CSR* for the duration of strong ground shaking. Also discussed is the nonlinear shear mass participation factor. All these screening, adjustment, and correction methods were readdressed (with respect to previous studies) to provide an unbiased estimate of liquefaction triggering for performance-based decisions.

Screening

Certain soil types are not susceptible to liquefaction in what we term “classic” free-field liquefaction, but may deform via cyclic softening. These soils can exhibit surface manifestations that appear quite similar to what is observed in “classic” liquefaction, such as lateral spreading, and building tilting, punching, and settlement. However, it has been found (Sancio et al., 2003) that the failure is primarily a function of undrained strength and asymmetrical driving shear stress (K_σ) imposed by a building or sloping ground. These soils tend to have a high percentage of fines, and these fines tend to behave in a plastic manner. Several cases like this were observed following the 2001 Kocaeli, Turkey Earthquake, and the 2001 Chi-Chi, Taiwan Earthquake, and were evaluated during the compilation of the CPT-based case history database (Moss et al., 2003). Since the limit-state function in this study was based on “classic” free-field liquefaction, it was not appropriate to include these cases in the analysis.

The criteria for screening these cases were based on research of fines content and plasticity in relation to liquefaction susceptibility (Andrews & Martin, 2000; Andrianopoulos et al., 2001; Guo & Prakash, 1999; Perlea, 2000; Polito, 2001; Sancio et

al., 2003; Yamamuro & Lade, 1998, Youd & Gilstrap, 1999). Zone A, shown graphically in Figure 2, was the envelope of potentially liquefiable materials used in this study. Using only Zone A is a conservative approach, that eliminated some potentially liquefiable materials in Zone B that require further laboratory testing. Zone A materials, however, exhibit behavior consistent with “classic” free-field liquefaction.

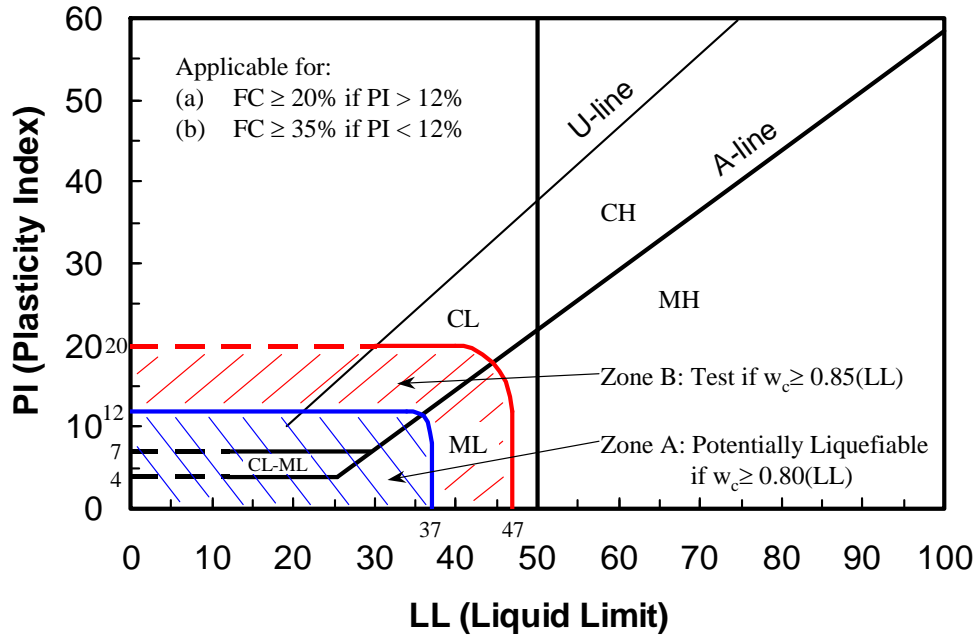


Figure 2. Modified “Atterberg” chart showing recommendations regarding the assessment of soil types considered liquefiable, from Seed et al., (2003).

Normalization

It has been found that effective overburden stress can profoundly influence CPT measurements (Olsen and Mitchell, 1995). This stress effect is typically accounted for by normalizing the tip resistance for the effective overburden to a reference stress level of one atmosphere. A complete discussion of normalization for effective overburden stress can be found in Moss et al. (2004). In that paper cavity expansion methods were used to bolster previously reported field and laboratory results for determining the appropriate level of normalization based on the measured tip resistance and friction ratio. The discussion in this paper is limited, for brevity, to the application of the proposed normalization technique.

Figure 3 shows normalization exponent curves as a function of friction ratio and tip resistance. These curves define the exponent used to normalize the tip resistance for a given level of overburden stress, using the following equation,

$$q_{c,l} = C_q \cdot q_c \quad \text{where } C_q = \left(\frac{P_a}{\sigma_v'} \right)^c \quad (4)$$

In Equation 4; $q_{c,l}$ is the normalized tip resistance (MPa), C_q is the tip normalization factor, q_c is the raw tip resistance (MPa), P_a is the reference stress in compatible units, σ_v'

is the effective overburden stress (kPa), and c is the normalization exponent. The normalization exponent curves in Figure 3 can be approximated by the iterative equation;

$$c = f_1 \cdot \left(\frac{R_f}{f_3} \right)^{f_2} \quad (5)$$

where $f_1 = x_1 \cdot q_c^{x_2}$

$$f_2 = -(y_1 \cdot q_c^{y_2} + y_3)$$

$$f_3 = \text{abs}(\log(10 + qc))^{z_1}$$

and $x_1 = 0.78, x_2 = -0.33, y_1 = -0.32, y_2 = -0.35, y_3 = 0.49, z_1 = 1.21$

In Equation 5; c is the tip normalization exponent, q_c the raw tip resistance (MPa), R_f the friction ratio (%), and $f_1, f_2, f_3, x_1, x_2, y_1, y_2, y_3,$ and z_1 parameters of the equation. To normalize the tip appropriately, an iterative procedure is necessary. The iterative procedure involves the following steps;

- 1) An initial estimate of the normalization exponent is found using raw tip measurements, friction ratio, and Figure 3 or Equation 5,
- 2) The tip is then normalized using Equation 4 (note: friction ratio will not change when tip and sleeve are normalized equivalently),
- 3) A revised estimate of the normalization exponent is found using the normalized tip resistance and Figure 3 or Equation 5, which is compared to the initial normalization exponent estimate,
- 4) The procedure is repeated until an acceptable convergence tolerance is achieved.

This process usually requires only two iterations to converge for most soils. It is recommended that the tip and sleeve be normalized equivalently.

Magnitude Correlated Duration Weighting Factor (DWF_M)

All results presented in this study include the correction of equivalent uniform cyclic stress ratio (CSR) for duration (or number of equivalent cycles) to CSR^* , representing the CSR for a duration typical of an “average” event of $M_w = 7.5$. This was done by means of a magnitude-correlated duration weighting factor (DWF_M);

$$CSR^* = CSR_{M_w=7.5} = \frac{CSR_{M_w=?}}{DWF_{M_w}} \quad (6)$$

This duration weighting factor is somewhat controversial, and has previously been developed using different approaches (cyclic laboratory testing and/or field case history data) by a number of investigators. Cetin et al. (2004), regressed the DWF_M from an SPT-based liquefaction database which included events covering a wide spectrum of moment magnitudes. These results were found to be in good agreement with previously published lower-bound results by Youd et al., (2001), and also consistent with laboratory results published by Idriss (1999) and Liu et al. (2001). This CPT-based study was lacking a wide enough magnitude spectrum to discern accurately the DWF_M in a similar manner, therefore the Cetin et al., (2004) DWF_M results were used in this study. The recommended DWF_M can be represented by the equation,

$$DWF_M = 17.84 \cdot M_w^{-1.43} \quad (7)$$

Equation 7 is valid for moment magnitudes from 5.5 to 8.5.

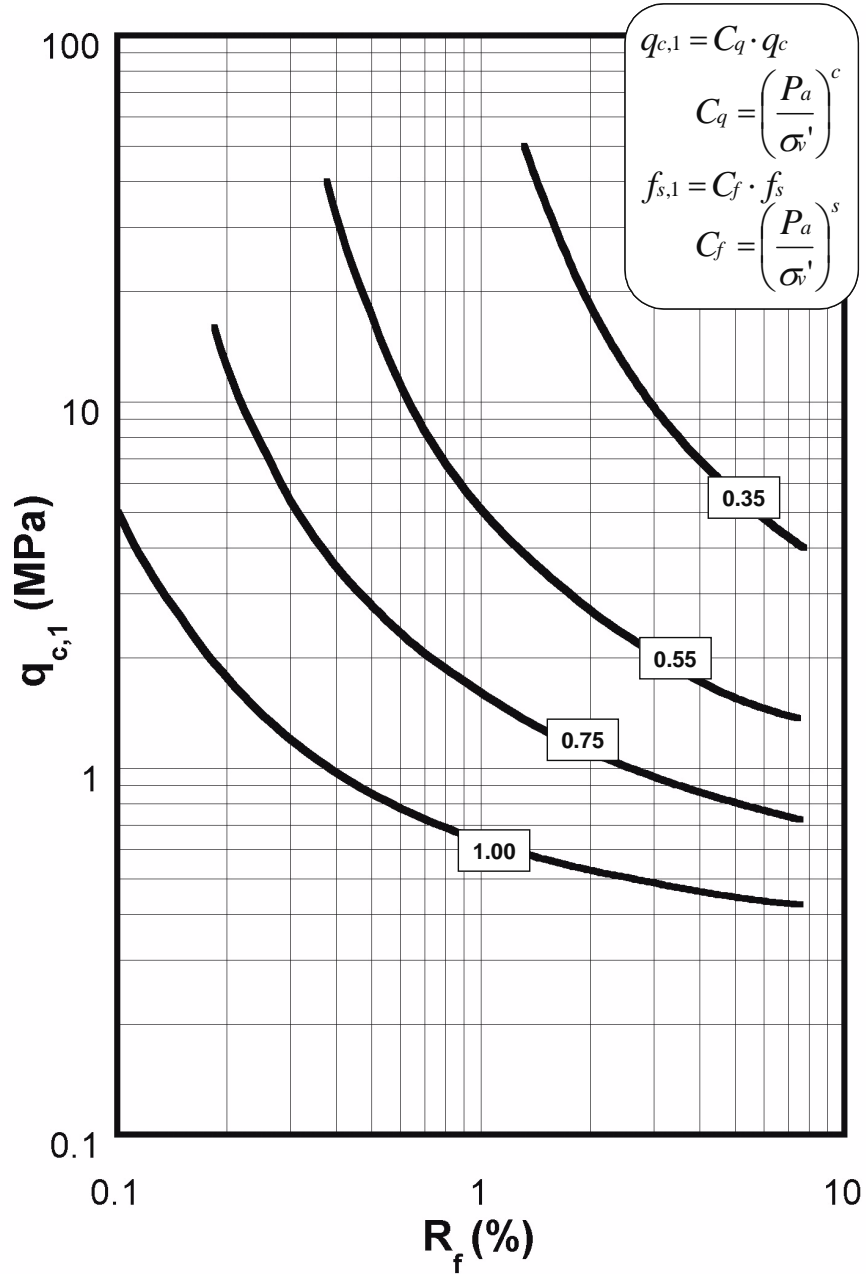


Figure 3. Proposed tip normalization exponent curves. Equation 5 can be used to calculate the normalization exponent, c , in the iterative normalization procedure. It is recommended that tip and sleeve resistance be normalized equivalently ($s=c$). From Moss, Seed, and Olsen (2004).

Non-linear shear mass participation factor (r_d)

The nonlinear shear mass participation factor (r_d) accounts for nonlinear response within a soil column. It reduces the peak ground acceleration from the surface to reflect the ground acceleration that is experienced at the critical depth. This factor, previously proposed by various researchers, has been reassessed by Cetin et al. (2004) using ground response analyses. In this work, 2,153 site response analyses were run using 50 sites and 42 ground motions creating a comprehensive suite of motions and soil profiles. The results of those analyses provided ample information to perform statistical analysis on the median r_d for a given depth, peak ground acceleration, and moment magnitude. The variance was estimated from the dispersion of these simulations. The median r_d results can be represented by the following equations,

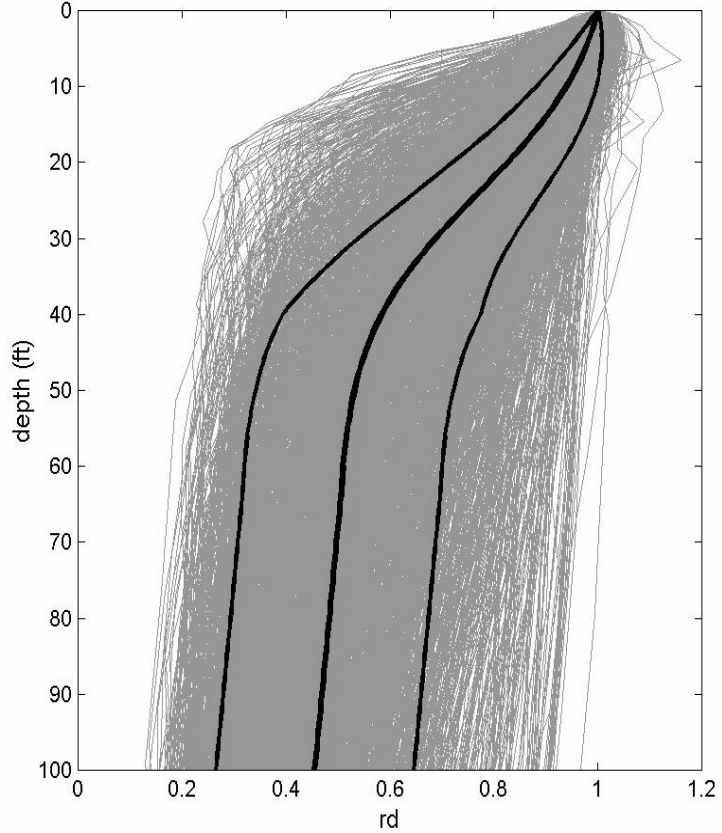


Figure 4. Mean and + 1 Standard Deviation r_d Values for the 2,153 Cases Analyzed, from Seed et al. (2004).

For $d < 20$ meters,

$$r_d(d, M_w, a_{max}) = \frac{\left[1 + \frac{-9.147 - 4.173 \cdot a_{max} + 0.652 \cdot M_w}{10.567 + 0.089 \cdot e^{0.089(-d \cdot 3.28 - 7.760 \cdot a_{max} + 78.576)}} \right]}{\left[1 + \frac{-9.147 - 4.173 \cdot PGA + 0.652 \cdot M_w}{10.567 + 0.089 \cdot e^{0.089(-7.760 \cdot a_{max} + 78.576)}} \right]} \quad (8)$$

And for $d \geq 20$ meters,

$$r_d(d, M_w, a_{max}) = \frac{\left[1 + \frac{-9.147 - 4.173 \cdot a_{max} + 0.652 \cdot M_w}{10.567 + 0.089 \cdot e^{0.089(-d \cdot 3.28 - 7.760 \cdot a_{max} + 78.576)}} \right]}{\left[1 + \frac{-9.147 - 4.173 \cdot a_{max} + 0.652 \cdot M_w}{10.567 + 0.089 \cdot e^{0.089(-7.760 \cdot a_{max} + 78.576)}} \right]} \quad (9)$$

In Equations 8 and 9; d is depth in meters to the midpoint of the critical layer, M_w is moment magnitude, a_{max} is peak ground acceleration in units of gravity.

Correlation

Figure 5 presents one view of the new recommended correlation, in this case a plot of contours of probability of liquefaction (for $P_L = 5\%$, 20% , 50% , 80% , and 95%) as a function of equivalent uniform cyclic stress ratio (CSR^*) and modified normalized CPT tip resistance ($q_{c,1,mod}$). In this figure, equivalent uniform CSR has been corrected for duration effects based on the magnitude correlated duration weighting factor (DWF_M). In Figure 5, the solid dots represent the centroids of probabilistic distributions of the individual case histories for cases wherein liquefaction was judged to have been “triggered” and open circles represent centroids of distributions of field cases wherein liquefaction did not occur. These distributions quantify each individual field case history and its distributed variance. The horizontal axis of Figure 5 represents modification of normalized CPT tip resistances ($q_{c,1}$ values) for the frictional effects of apparent fines content and character. To account for the systematic suppression of liquefiability with increased friction ratio, values of $q_{c,1}$ are adjusted by,

$$q_{c,1,mod} = q_{c,1} + \Delta q_c \quad (10)$$

$$\text{where } \Delta q_c = x_1 \cdot \ln(CSR) + x_2$$

$$\text{and } x_1 = 0.38 \cdot (R_f) - 0.19 \text{ and } x_2 = 1.46 \cdot (R_f) - 0.73$$

In Equation 10; $q_{c,1}$ is in MPa, R_f in percent (%), and the bounds of Δq_c are from $R_f = 0.5$ to 5.0 , where $\Delta q_c = 0$ when $R_f \leq 0.5$, Δq_c reaches its maximum at $R_f = 5.0$, and no data exists for $R_f > 5.0$. This term was regressed from the liquefaction database and represents the change in liquefiability correlated to the change in friction ratio, as a function of CSR .

Figure 6 presents an alternate, deterministic, view of the new correlation. In this case contours of $P_L = 15\%$ are shown for three different values of mean Δq_c spanning the full available range of Δq_c . The curves also represent approximate contours of equal friction ratio.

For exact parameter estimation (assuming mean values), the following equation can be used to calculate the probability of liquefaction,

$$P_L = \Phi \left(\frac{\left(q_{c,1}^{1.045} + q_{c,1}(0.110 \cdot R_f) + (0.001 \cdot R_f) + c(1 + 0.850 \cdot R_f) - 7.177 \cdot \right)}{\ln(CSR) - 0.848 \cdot \ln(M_w) - 0.002 \cdot \ln(\sigma_v') - 20.923} \right) \cdot 1.632 \quad (11)$$

where; $q_{c,1}$ is the normalized tip resistance (MPa), R_f is the friction ratio (%), c is the normalization exponent, CSR is the equivalent uniform cyclic stress ratio, σ_v' is the effective overburden stress (kPa), and Φ and the cumulative normal distribution which can be calculated using the $NORM(P_L, 0, 1)$ function in Excel. The cyclic resistance ratio for a given probability of liquefaction can be calculated from,

$$CRR = \exp \left(\frac{\left(q_{c,1}^{1.045} + q_{c,1}(0.110 \cdot R_f) + (0.001 \cdot R_f) + c(1 + 0.850 \cdot R_f) \right)}{7.177} \right) \left(\frac{-0.848 \cdot \ln(M_w) - 0.002 \cdot \ln(\sigma_v') - 20.923 + 1.632 \cdot \Phi^{-1}(P_L)}{7.177} \right) \quad (12)$$

where the inverse cumulative normal distribution function, $\Phi^{-1}(P_L)$, can be calculated using the $NORMINV(P_L,0,1)$ function in Excel. Comparison of the results with previous deterministic and probabilistic results can be found in Moss et al. (2004). Note that Equation 12 produces results for the input magnitude ($CRR_{M_w=?}$), whereas Figures 5 and 6 produce results for a mean magnitude of 7.5 (CSR^*).

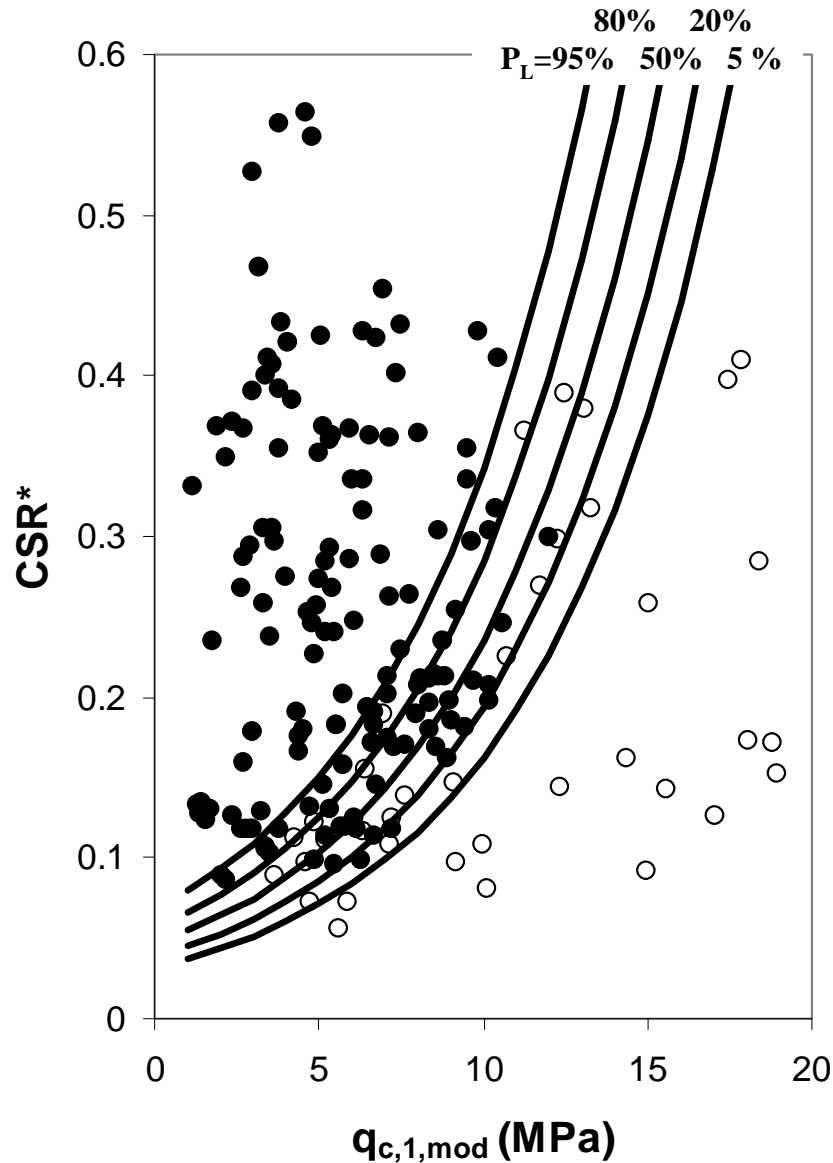


Figure 5. Contours of 5%, 20%, 50%, 80% and 95% probability of liquefaction as a function of equivalent uniform cyclic stress ratio and “fines”-modified CPT tip resistance for $M_w = 7.5$, $\sigma_v' = 1$ atmosphere, from Moss et al., (2004).

The liquefaction triggering results presented in this paper can be used in forward analyses either in a probabilistic or deterministic manner. Normalized tip resistance ($q_{c,1}$) and the normalization exponent (c) were incorporated into the limit-state function for the Bayesian updating and reliability analysis. This resulted in a complete assessment of the influence of effective overburden on CPT measurements and liquefaction. Therefore, using the recommended iterative normalization scheme obviates the need for subsequent K_c corrections commonly used in liquefaction analysis.

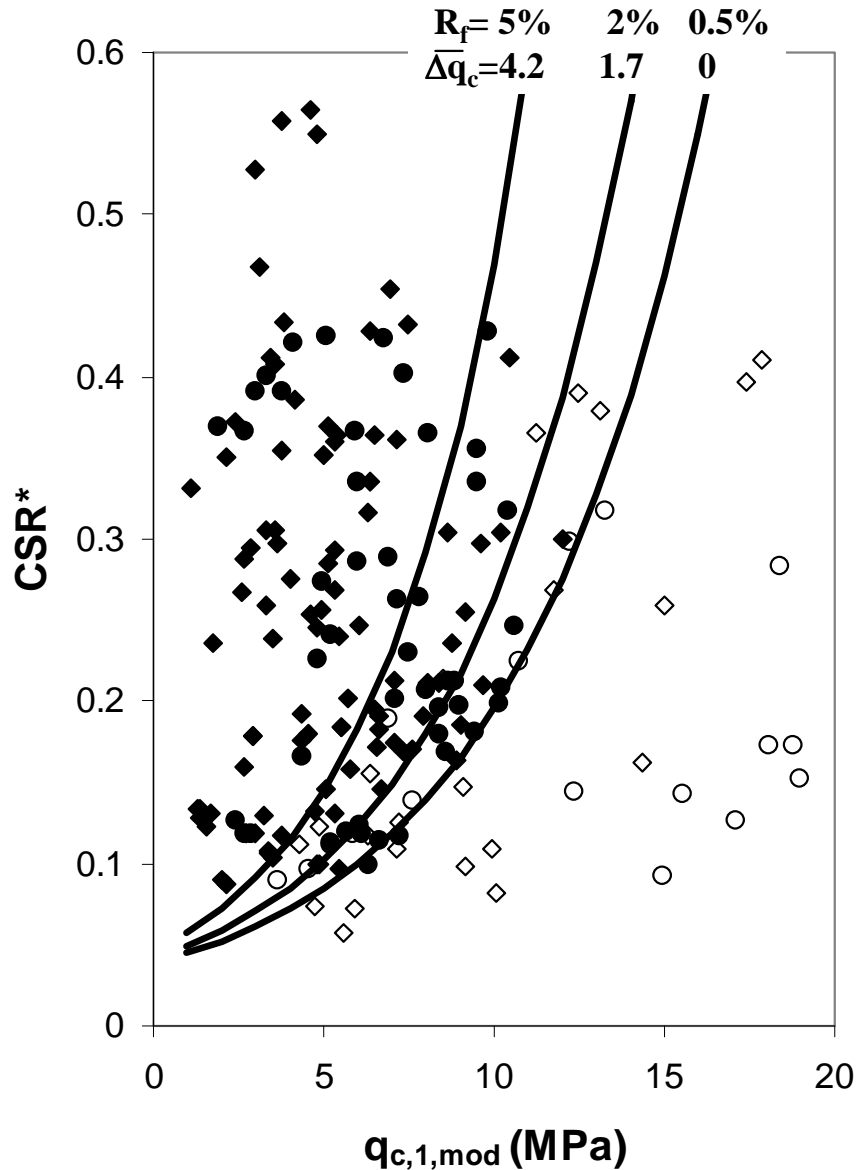


Figure 6. Constant friction ratio triggering curves all shown for $P_L=15\%$. The round data points indicate "clean" sands ($R_f \leq 0.5\%$) and the diamond data points indicate soils of higher "fines" ($R_f > 0.5\%$), for $M_w = 7.5$, $\sigma'_v = 1$ atmosphere, from Moss et al., (2004).

Summary

Presented is a synopsis of the recent CPT-based liquefaction triggering correlations as presented in Moss et al. (2004). These correlations treat the problem of liquefaction triggering as inherently uncertain, and strive to fully capture all forms of uncertainty. The results are presented probabilistically for performance-based engineering applications. Discussed are the steps and procedures necessary for calculating the probability of liquefaction, including; screening procedures for liquefiable material, calculation of the nonlinear shear mass participation factor (r_d), normalization of the CPT measurements for effective overburden, and corrections of *CSR* for magnitude correlated duration (DWF_M). The goal of this work was to provide as unbiased an assessment of liquefaction triggering as possible based on the CPT.

Acknowledgements

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