Models for Predicting the Lower Limit of the Canopy-Air Temperature Difference of Two Cool Season Grasses

D. L. Martin, D. J. Wehner,* and C. S. Throssell

ABSTRACT

Estimation of the lower limit of the canopy-air temperature differential, (Tc-Ta)LL, is required for calculation of an empirically-based crop water stress, index. This research determined the complexity of model needed for accurate estimation of $(T_c - T_a)_{LL}$ for several field grown cultivars of Kentucky bluegrass (Poa pratensis L.) and for creeping bentgrass (Agrostis stolonifera L. var. palustris (Huds.) Farw.). Regression models using vapor pressure deficit of the air (VPD), net radiation load (Rn), and wind speed (WS) were developed for predicting $(T_{\rm c}-T_{\rm a})_{\rm t.t.}$. The best one to three-variable regression models for predicting $(T_c - T_a)_{LL}$ used variable groups of VPD $(r^2 = 0.47)$; VPD and R_n ($R^2 = 0.66$); and VPD, R_n , and WS ($R^2 = 0.82$). Models developed for predicting (T_c - T_a)_{LL} on individual Kentucky bluegrass cultivars, across Kentucky bluegrass, and across both species were tested on a validation data set. Models using only VPD accounted for < 2% of variation in actual $(T_C - T_a)_{LL}$ of nonwater-stressed turf. Models using VPD and R_n developed from pooled Kentucky bluegrass data, individual Kentucky bluegrass cultivars, or Kentucky bluegrass and creeping bentgrass data accounted for an average of 15, 13, and 14% of variation in actual $(T_c - T_a)_{LL}$, while models using VPD, R_n , and WS accounted for an average of 62, 62, and 64%, respectively. On creeping bentgrass, the Kentucky bluegrass model and dual species model introduced a large amount of bias to predicted (Tc - Ta)LL. At sites where environmental conditions are highly variable, the effects of VPD, Rn, and WS must be taken into account to accurately predict $(T_c - T_a)_{1,l.}$ of turfgrass. A single model appears appropriate for prediction of (Tc - Tn)LL across Kentucky bluegrass cultivars; a separate model for creeping bentgrass is required.

As DEMANDS on potable water resources continue to increase it is imperative that all uses of this resource become more efficient. Turfgrass managers often

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face restrictions on the amount of water available for irrigation. Thus, it is critical that they utilize practices that optimize the timing and amount of irrigation applied to an area.

Carrow (1985) grouped turfgrass irrigation programming techniques into four categories: (i) techniques that determine when to irrigate based on soil moisture status, (ii) techniques that use meterological data to determine plant-water requirements, (iii) techniques that determine plant-water status, or (iv) techniques that utilize a combination of the above methods. A subgroup of plantwater status techniques referred to as canopy-temperature based techniques have received increased attention in the literature. One of these methods, known as the Crop Water Stress Index (CWSI) method (Jackson et al., 1981; Idso et al., 1981a,b) was found to have potential in scheduling irrigation of turfgrasses by Throssell et al. (1987). They compared the empirical CWSI method to the stress-degree-day method, irrigation scheduling using a tensiometer, and the critical-point method.

The empirical CWSI method is based on determining the difference in canopy vs. air temperature $(T_c - T_a)$, adjusting the difference for current meteorological conditions that affect the T_c , and then comparing the difference with what would be expected for nonwater stressed plants to generate a CWSI. A detailed discussion of the theory behind the limitations to the CWSI method and its relationship to turfgrass water status has been presented by Martin (1990).

The empirical CWSI method requires determination of the lower and upper limits, referred to as baselines, of $(T_c - T_a)$. The lower limit of $(T_c - T_a)$ is determined on nonwater-stressed turf. Horst et al. (1989), working in Texas with three warm season and one cool season turfgrass (tall fescue, *Festuca arundinacea* Schreb.), found that when $(T_c - T_a)_{LL}$ was plotted as a function of VPD,

Abbreviations: $(T_e - T_a)_{LL}$, lower limit of canopy minus air temperature difference; VPD, vapor pressure deficit; R_a , net radiation load; WS, wind speed; CWSI, crop water stress index; RH, relative humidity; r_a , aerodynamic resistance; r_e , canopy resistance.

the bascline slopes were seasonally as well as species dependent. Earlier work by Horst et al. (1987) suggested that the aerodynamic and canopy resistances associated with turfgrass stands may be species as well as mowing height specific, and thus, a general nonwater-stressed baseline may need modification for each turfgrass under each different cultural regime.

The purpose of this research project was to determine the complexity of model needed to accurately predict the $(T_c-T_a)_{\rm LL}$ for turfgrass growing in Illinois and to determine if a single $(T_c-T_a)_{\rm LL}$ model is appropriate for calculating CWSI values for both Kentucky bluegrass and creeping bentgrass.

MATERIALS AND METHODS

The experiment was conducted at the University of Illinois Ornamental Horticulture Research Center, Urbana, IL. Research was conducted on single plots of 'Penncross' and several Kentucky bluegrass cultivars growing on a Flanagan silt loam (fine, montmorillonitic, mesic aquic argiudoll). The Kentucky bluegrass used were 'South Dakota Common', 'America,' 'Kenblue,' 'Bristol,' and a blend of 'Adelphi,' 'Glade,' 'Parade,' and 'Rugby.' Plot size was 5.2 by 5.2 m.

In 1988, all grasses were fertilized on 3 June, 5 August, and 7 November with 84, 48, and 48 kg N ha⁻¹, respectively. In 1989, 48 kg N ha⁻¹ were applied to all grasses on 18 May, 20 June, 18 July, and 12 October. Mowing was performed two to three times per week as needed at a height of 48 mm for Kentucky bluegrass and every other day at 9.5 mm for creeping bentgrass. Clippings were returned for all grasses.

Water was applied by irrigation to maintain turfgrass evapotranspiration at full potential (nonlimiting soil moisture conditions) for the prevailing environmental conditions. Water was
applied to all plots when soil matric potentials of any plot fell
below -0.04 MPa. Soil matric potentials were monitored by
tensiometers installed at a 5.1-cm depth under Kentucky bluegrass and a 2.5-cm depth under creeping bentgrass. Water was
applied in a quantity that brought tensiometer readings to 0
MPa. No meteorological data was sampled from turf when
tensiometers measured 0 MPa or when tensiometer values fell
below -0.04 MPa.

Canopy temperature of the turfgrass was measured with an infrared thermometer (ST 27 Turfgrass Monitor, Carborundum Co., Solon, OH) with a six-degree field of view. The emissivity setting on the instrument was factory set at 0.99. Twelve T_c readings were taken at 5-s intervals during a 1-min measuring period (six west facing, six east facing) and averaged to provide a mean for the sampling period. The infrared thermometer was held 1.3 m above the turf at an angle of 40 ° from horizontal providing a target area of ≈ 0.05 m².

Air temperature and relative humidity (RH) were measured by an aspirated bead thermistor and an aspirated capacitancetype humidity sensor located in the nose of the infrared thermometer. Sampling of T_a and RH was performed at the same time and frequency as T_c sampling, with averages calculated for each sampling period.

Wind speed was measured over each plot using a three-cup anemometer (R.M. Young Company, Traverse City, MI) positioned at a height of 1.5 m above the canopy. Net radiation load was measured for each plot using a Fritschen type miniature net radiometer (Fritschen and Mulling, 1965) positioned 1 m above the canopy. Voltage outputs from the anemometer and net radiometer were measured every 5 s and averaged for each 1-min sampling period by data logger (Model LI-1000, LICOR, Lincoln, NE).

Three to four 1-min measuring periods were conducted on each plot between 1200 and 1500 h on 17 dates in 1988 and 31 dates in 1989. Meteorological conditions were variable among

the dates, however, data were taken only when solar radiation conditions were stable. Data from 17 dates in 1988 and 16 dates in 1989 were pooled to form Data Set I for construction of models to predict $(T_c - T_a)_{LL}$ of turf. Regression analysis was performed in order to relate $(T_c - T_a)$ to environmental variables such as the (VPD), R_n , and WS. Linear additive equations were investigated.

In order to use the complete energy balance equation to predict (T_c - T_a)_{LL}, estimates of the aerodynamic resistance (r_a) and the canopy resistance (r_c) of the turf were required. Values of r_a for the turf canopies were determined by a method similar to that used by Johns et al. (1983) utilizing the resistance to enthalpy loss by a completely wetted canopy. Turf was sprayed with a 1:200 mixture of wetting agent/water (Hydraflo, Sierra Crop Protection Co., Milpitas, CA) in a quantity to ensure complete wetting. A delay between canopy wetting and the measurement period was practiced to allow for canopy temperature stabilization. The wetting procedure was performed for each 1-min sampling period. Sampling was performed on seven dates in 1988 and nine dates in 1989. Attempts were made to sample during periods that would provide a broad range of WS to the data set (Data Set II). The energy balance equation used by Jackson et al. (1981) was rearranged to solve for r_n when r_n is zero (the case of a completely wetted canopy):

$$r_{\rm a} = [(T_{\rm c} - T_{\rm a}) + \text{VPD}/(\Delta + \gamma)](\Delta + \gamma)(\rho C_{\rm p}/\gamma R_{\rm n}).$$
 [1]

In Eq. [1], r_a = the aerodynamic resistance in seconds per meter, Δ = the slope of the saturation vapor pressure with temperature relationship (kPa °C⁻¹) with Δ calculated at (T_c + T_a)/2, γ = the psychrometric constant (kPa °C⁻¹), ρ = the density of air (g m⁻³), and C_p = the heat capacity of air (J g⁻¹ °C⁻¹). Values of r_a were regressed on the log₁₀ transformation of WS in order to develop equations for predicting r_a as function of WS for each cultivar or species.

To elucidate the relationship between $r_{\rm e}$ and $R_{\rm n}$ for the nonwater stressed grasses, $T_{\rm e}$ and associated meteorological parameters were sampled for two 1-min measuring periods per hour per plot on five dates in 1988 and 10 dates in 1989. Sampling was performed from shortly before sunrise to shortly after sunset provided skies were clear. Samples taken when dew was present or when tensiometer readings fell below -0.04 MPa were discarded. In addition to the data gathered on these 15 dates, data from 10 dates from Data Set I were included in the data set (Data Set III). Values of $r_{\rm e}$ (s m⁻¹) were calculated by the rearranged energy balance equation:

$$r_{c} = r_{a} \left[\gamma r_{a} R_{n} / (\rho C_{p}) - (T_{c} - T_{a}) (\Delta + \gamma) - VPD \right] / \left[\gamma ((T_{c} - T_{a}) - r_{a} R_{n} / (\rho C_{o})) \right]$$
 [2]

Values of r_a required in Eq. [2] were estimated by the regression relationships between r_a and WS. To develop a prediction equation relating r_c (calculated by Eq. [2]) to R_n , the \log_{10} transformation of r_c was regressed on the \log_{10} additively transformed R_n . Since R_n remained negative in sign shortly after sunrise and became negative again shortly before sunset, an additive transformation of R_n (+ 100 W m⁻²) was performed prior to \log_{10} transformation in order to avoid taking the logarithm of a negative number.

An independent data set (Data Set IV) was constructed from data gathered from nonwater-stressed turf between 1200 and 1500 h on 15 of the 31 sampling dates (previously discussed) in 1989. The best one, two, and three-variable empirical models fit to $T_c - T_a$ from Data Set I as well as the complete energy balance approach were tested for their ability to predict ($T_c - T_a$)_{LL} of nonwater-stress turf. An iterative procedure described by Jackson et al. (1981) was used to generate the predicted T_c and Δ at full potential evapotranspiration, as these variables were treated as unknowns. Actual $T_c - T_a$ from Data Set IV was regressed on the predicted ($T_c - T_a$)_{LL} from all equations being tested. Values of R^2 as well as slopes of the fitted lines were used as evaluation criteria.

Table 1. Summary of vapor pressure deficit (VPD),	net radiation (Rn), and windspeed	(WS) statistics for data sets gathered during
the 1988 and 1989 sampling periods.		

Data set			VPD			R _n			WS			
	Year	n	Mini- mum	Maxi- mum	Mean	Mini- mum	Maxi- mum	Mean	Mini- mum	Maxi- mum	Mean	
					 — kРа —			W m-2			m s-2 -	
I.	Lower baseline	1988 1989	391 285	0.84 0.69	4.74 2.41	2.69 1.40	101.9 83.3	752.1 779.6	419.3 476.1	0.20 0.20	8.08 8.30	2.96 3.03
II.	Canopy resistance	1988 1989	541 416	0.38 0.45	4.69 2.33	2.38 1.28	-58.3 -61.5	694.5 683.5	387.2 331.9	0.32 0.20	8.08 5.55	2.77 2.49
III.	Aerodynamic resistance	1988 1989	279 424	0.99 0.49	4.71 1.98	2.42 1.25	116.5 169.2	650.7 615.5	433.5 382.7	0.25 0.20	8.07 5.61	4.25 2.39
IV.	Independent data set	1989	260	0.49	2.63	1.56	138.0	708.2	483.5	0.20	9.13	2.87

RESULTS AND DISCUSSION

Predicting the Lower Limit of the Canopy-Air Temperature Difference of Turf

A summary of the meteorological conditions prevailing during measurement periods for the five data sets are shown in Table 1. A wide range of observed VPD, R_n , and WS were present. Such conditions were desirable when developing prediction equations in order to reduce the probability of biasing the models toward a specific set of environmental conditions.

The coefficients of determination of models fit to T_c - T_a of the various grasses (Table 2 and 3) increased with increasing model complexity. When a single independent variable was considered, VPD provided the best fit with an average $r^2 = 0.47$, compared with 0.10 and 0.12 for equations containing R_n or WS, respectively. The average correlation coefficients between $T_c - T_a$ of nonwater-stressed turf and VPD, R_n , and WS were -0.68, 0.32, and -0.34, respectively. Models containing VPD $+ R_n$ accounted for more variation than those containing VPD + WS, with the average R^2 values being 0.66 and 0.54, respectively. The actual coefficients and intercepts for the three-variable models are shown in Table 3. The three-variable linear model containing VPD + R_n + WS had an average R^2 value of 0.82. Values of R^2 varied little between equations that were fit to data pooled across all grasses or just across Kentucky bluegrass cultivars. In general, R^2 values from equations fit to data pooled across all grasses were intermediate to those fit to data from individual grasses.

Based on coefficient of determination values of empirical equations fit to $T_c - T_a$ of nonwater-stressed turf, the most sound progression in model complexity from one through three variables was to utilize the variable groups VPD; VPD and R_n ; and VPD, R_n , and WS. As discussed later, these three forms of linear equations were tested for predictive capability of an independent data set.

In work performed in Texas on nonwater-stressed bermudagrass [Cynodon dactylon (L.) Pers.], St. Augustinegrass (Stenotaphrum secundatum (Walker) O. Kuntze), tall fescue, and buffalograss [Buchloe dactyloides (Nutt.) Engelm.], Horst et al. (1989) found VPD, R_n , and WS to account for an average of 53, 16, and 7%, respectively, (76% total) of variation in $T_c - T_a$ using multiple additive regression equations. Utilizing the same com-

plexity of model, we found VPD, WS, and R_n to explain an average of 46, 17, and 18%, respectively, (81% total) of variation in $T_c - T_a$ of the six nonwater-stressed turfgrass examined. Whereas the range of WS and the magnitude of the range in VPD measured by Horst et al. (1989) and in our work were similar, VPD measured in our study was generally lower. The range of R_n in this study was 83 to 779 W m⁻² (Table 1) compared with \approx 400 to 700 W m⁻² for the work of Horst et al. (1989). The larger range of R_n in this study may be responsible for R_n having a more equal role with WS in accounting for the variation in $T_c - T_a$.

The complete energy-balance equation suggests VPD, R_n , and WS to be important in influencing $T_c - T_a$ of transpiring turf. Although WS does not appear explicitly in the energy-balance approach as does VPD and R_n , it does affect r_a of the canopy. It is likely that the relative importance of VPD, R_n , and WS in empirical models for predicting $T_c - T_a$ is closely linked to the total range of the three variables measured during the periods of data acquisition.

Predicting Aerodynamic Resistance of Turf

The equations and resulting curves generated for each of the six turfgrasses by regression of predicted r_a and the \log_{10} transformation of WS are presented in Fig. 1. Due to the large number of r_a samples taken, display of r_a values for each grass was impractical. Equations for all grasses were highly significant. Values of r^2 ranged from a high of 0.77 for Penncross creeping bentgrass to a low of 0.57 for South Dakota Common Kentucky bluegrass.

The range of slopes for Kentucky bluegrass cultivars was from -57.3 for South Dakota Common to -75.3 for Kenblue. The slope of the line fit to data from creeping bentgrass was -75.6. The intercept for creeping bentgrass, 100.0 s m⁻¹, was considerably larger than those of equations fit to Kentucky bluegrass cultivars which ranged from 79.3 to 90.9 s m⁻¹.

Aerodynamic resistance decreased with increasing WS. Creeping bentgrass demonstrated a greater predicted $r_{\rm a}$ than any of the Kentucky bluegrass cultivars across the range of WS measured in this study. Creeping bentgrass cut at 9.5 mm would be expected to have a higher $r_{\rm a}$ than Kentucky bluegrass cut at 48 mm due to a smoother canopy surface.

Table 2. Summary of r^2 and R^2 values for equations fitted to the canopy-air temperature differential of nonwater-stressed Kentucky bluegrass and creeping bentgrass.

Variables in model	Blend† Kentucky bluegrass	South Dakota Kentucky bluegrass	America Kentucky bluegrass	Kenblue Kentucky bluegrass	Bristol Kentucky bluegrass	Penncross creeping bentgrass	All grasses pooled	Kentucky bluegrasses pooled		
Vapor pressure deficit (VPD)	0.34**	0.31**	0.47**	0.42**	0.64**	0.60**	0.47**	0.45**		
Net radiation (R_n)	0.21**	0.18**	0.03*	0.06**	0.04*	0.10**	0.10**	0.10**		
Wind speed (WS)	0.07**	0.08**	0.13**	0.16**	0.15**	0.11**	0.12**	0.12**		
VPD + WS	0.40**	0.36**	0.52**	0.56**	0.68**	0.64**	0.54**	0.52**		
$VPD + R_n$	0.63**	0.57**	0.63**	0.58**	0.76**	0.73**	0.66**	0.65**		

^{*,**} Significant at 0.05 and 0.01 probability levels respectively.

Predicted r_a varied among the Kentucky bluegrass cultivars. Relative ranking of the Kentucky bluegrass cultivars by magnitude of predicted r_a varied with WS. The curves for predicted r_a suggest differences of 10 s m⁻¹ may often be present among Kentucky bluegrass cultivars. Factors such as leaf and stem number as well as their position within the turfgrass canopy have been implicated in influencing r_a . A turf with high leaf and stem densities plus substantial horizontal leaf orientation can cause greater impairment of normal upward movement of water vapor and sensible heat leading to a greater r_a (Beard, 1985). We did not characterize the canopy structure of the grasses utilized in this work.

Johns et al. (1983) found St. Augustinegrass to have mean r_a values of 72, 79, and 66 s m⁻¹ at a mean WS of 0.6 m s⁻¹ when cut at heights of 5, 6.5, and 8 cm, respectively. Direct comparison of these values to those found in our work is not appropriate because different species and mowing heights were used in the two studies. In addition, WS was measured at a height of 0.15 m above the turf in the study conducted by Johns et al. (1983) and at 1.5 m above the turf in this study. Wind speed varies with height of measuremnt above the plant canopy (Monteith, 1973). To predict r_a using our regression equations, WS should be measured at 1.5 m or adjustments to the predicted r_a will be necessary.

Predicting Canopy Resistance of Turf

The curves and equations generated by regression of \log_{10} transformation of r_c on \log_{10} transformation of $(R_n + 100 \text{ W m}^{-2})$ are shown in Fig. 2. The form of the

equation was $r_c = 10^b (R_n + 100)^a$, where b and a are the intercept and slope terms after \log_{10} transformation of dependent and independent variables. The equation used to describe the relationship between R_n and r_c was similar to that used by Denmead and Millar (1976) to relate net irradiance with r_c and by Hatfield (1985) to relate incoming shortwave radiation and r_c .

Variability in r_c accounted for by the regression equations ranged from 36% for creeping bentgrass to 62% for the Kentucky bluegrass blend. The r^2 values for our equations were lower than those reported in previous studies. The r^2 values for the references cited were based on data collected over a 1- (Hatfield, 1985) to 4-d period (Denmead and Millar, 1976), whereas we combined data over many dates during the growing season to develop a relationship predicting the seasonal average r_c at a given R_n . Under constant irradiance, the value of r_c of a turfgrass would be expected to cycle between a maximum value immediately following mowing to a minimum value immediately preceding mowing. Mowing reduces the leaf transpirational area which causes r_c to increase (Shearman, 1985).

The slope and intercept for the equation fit to data from creeping bentgrass were smaller than for any of the Kentucky bluegrass. Predicted r_c of creeping bentgrass was lower than any of the Kentucky bluegrass cultivars at R_n below ≈ 160 W m⁻² (Fig. 2). Above this range, America Kentucky bluegrass had the lowest predicted r_c of any of the six turfgrasses. The blend of Kentucky bluegrass exhibited the highest predicted r_c across the entire range of R_n measured in this study. Differences in predicted r_c between grasses appeared to be minimal un-

Table 3. Coefficients, intercepts, and R^2 values for three-variable, first-order equations relating vapor pressure deficit of the air (VPD), windspeed (WS) and net radiation load (R_n) to the canopy-air temperature deficit of six nonwater-stressed turfgrasses.

		Coefficients			
Turfgrass	VPD	WS	R _n	Intercept	R^2
Blend Kentucky bluegrass†	- 1.83	-0.74	0.01	1.73	0.80**
South Dakota Common Kentucky bluegrass	-1.54	-0.82	0.01	1.41	0.78**
America Kentucky bluegrass	-1.80	-0.70	0.01	1.91	0.77**
Kenblue Kentucky bluegrass	-2.04	-1.01	0.01	2.79	0.85**
Bristol Kentucky bluegrass	-2.21	0.69	0.01	2.49	0.86**
Penncross creeping bentgrass	-2.30	-0.92	0.01	3.29	0.87**
Pooled Kentucky bluegrass	~ 1.90	-0.82	0.01	2.11	0.80**
Pooled Kentucky bluegrass + creeping bentgrass	- 1.97	-0.83	0.01	2.32	0.81**

^{**} Significant at 0.01 probability level.

[†] The blend consisted of Adelphi, Glade, Parade, and Rugby Kentucky bluegrasses.

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der conditions of high R_n and maximal under very low R_n .

As with r_a , minimal information on actual measured r_c of turfgrasses is available in the literature. In work by Johns et al. (1981) on St. Augustinegrass, r_c averaged 14, 22, and 43 s m⁻¹ at cutting heights of 8.0, 6.5, and 5 cm, respectively. Incoming shortwave radiation supplied by a metal-halide source in the controlled environmental chamber utilized by Johns et al. (1981) averaged 300 W m⁻². Comparison of the values measured by Johns et al. (1981) with our values is of limited usefulness, as different species and mowing heights were utilized as well as the fact that the spectrum of the metal-halide source varies from that of natural sun light.

Validation of Prediction Equations

Values of r^2 and slopes of equations generated by regression of actual $(T_c - T_a)_{LL}$ of nonwater-stressed turf from the independent data set on predicted $(T_c - T_a)_{LL}$ values for Kenblue Kentucky bluegrass and creeping bentgrass are shown in Table 4. The models that were tested for predictive capability on the independent data set were the best one, two, and three-variable empirical models as well as the energy balance equation. For each level of model complexity, there were three models tested; those developed from pooled Kentucky bluegrass data, from individual cultivars alone, and from

160 ·SD Common KB ···· America KB ··· Kenblue KB 140 $r_a = -57.34 \text{ (Log}_{10} \text{ WS)} + 79.91$ $r_a = -64.92 \text{ (Log}_{10} \text{ WS)} + 88.65$ SD Common KB $r^2 \approx 0.57$ Aerodynamic Resistance (sm⁻¹) r2 = 0.64 120 Kenblue KB = -75.33 (Log₁₀ WS) + 90.95 100 80 60 40 20 0 0 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 160 Blend KB · Penncross CB ---- Bristol KB 140 Blend KB $r_a = -65.37 \text{ (Log}_{10} \text{ WS)} + 79.32$ $r_a = -73.56 \text{ (Log}_{10} \text{ WS)} + 87.08$ Aerodynamic Resistance (sm⁻¹) Bristol KB 120 enncross CB $r_a = -75.59 (Log_{10} WS) + 100.01 r^2 = 0.77^*$ 100 80 60 40 20 0 0 1.0 2.0 5.0 3.0 4.0 6.0 7.0 8.0 Windspeed (ms-1)

Fig. 1. Relationship between predicted aerodynamic resistance and windspeed for South Dakota Common Kentucky bluegrass (KB), America KB, Kenblue KB, a blend of KB, Bristol KB, and Penncross creeping bentgrass (CB).

data pooled across all grasses. The energy balance approach utilized the crop specific components of r_a and r_c calculated by equations developed from the individual cultivar on which the model was being tested.

Models that utilized only VPD to predict $(T_c - T_a)_{LL}$ accounted for an inconsequential amount (from <1 to 2%) of variation in actual $T_c - T_a$ and were not statistically significant at P=0.05. The two-variable models that were derived from pooled Kentucky bluegrass data, individual cultivar data, and data pooled across all grasses accounted for an average of 15, 13, and 14% of variation in actual $(T_c - T_a)_{LL}$. The relationships between actual $(T_a - T_a)_{LL}$ and predicted $(T_c - T_a)_{LL}$ values calculated by the two-variable models were statistically significant at P=0.05 or P=0.01 except for those that were fit to creeping bentgrass. When the three-variable empirical models were employed, predictive capability rose to 62, 62, and 64%, respectively.

Surprisingly, models developed from pooled data slightly outperformed the cultivar specific models across most levels of model complexity. While demonstrating greater predictive capability than the one- or two-variable empirical models, the energy balance approach using cultivar specific r_a and r_c terms accounted for less variation than the three-variable empirical models.

Deviation of the slope of the equation from a value of one is an indication of bias. The average slope of the line relating actual $(T_c - T_a)_{LL}$ to predicted $(T_c - T_a)_{LL}$

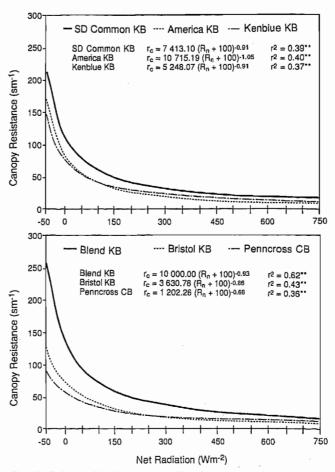


Fig. 2. Relationship between predicted canopy resistance and net radiation for South Dakota Common Kentucky bluegrass (KB), America KB, and Kenblue KB, a blend of KB, Bristol KB, and Penncross creeping bentgrass (CB).

Table 4. Coefficients of determination and slopes of equations generated by regression of actual canopy-air temperature difference of nonwater-stressed turfgrass on values calculated by prediction equations.

		Test cultivar/species								
		· ·	Kenblue Kentucky bluegra	ss	Penncross creeping bentgrass Model type					
			Model type							
Model complexity	Statistic	All bluegrass model	Kenblue model	All turfgrass model	All bluegrass model	Penncross model	All turfgrass model			
apor pressure eficit (VPD)	r² Slope	<0.01 0.10	<0.01 0.10	< 0.01 0.10	0.02 -0.35	0.02 -0.25	0.02 -0.32			
$PD + Net$ adiation (R_n)	r² Slope	0.12* 0.90	0.12* 0.90	0.12* 0.87	0.09 0.98	0.05 0.64	0.08 0.91			
PD + R _n - Windspeed (WS)	r² Slope	0.70** 1.10	0.70** 0.95	0.69** 1.09	0.76** 1.33	0.75** 1.16	0.76** 1.30			
Energy balance quation	r² Slope		0.60** 0.76			0.71** 0.97				

^{*,**} Significant at 0.05 and 0.01 probability levels respectively.

was 1.06 for the three-variable empirical model. On creeping bentgrass, equations developed from data pooled from all grasses or from the five Kentucky bluegrasses caused a higher degree of bias in predicted $(T_c - T_a)_{LL}$ values than those developed specifically from creeping bentgrass data. The bias introduced to predicted (T_c -T_a)_{LL} by the three-variable empirical model was minimal compared with that introduced by the energy balance approach (slope = 0.69). The poor predictive capability of the energy balance approach in combination with the large bias it introduced to predicted $(T_c - T_a)_{LL}$ values was unexpected, and is not easily explained.

In theory, the complete energy-balance approach should provide a more accurate prediction of $(T_c - T_a)_{LL}$, however, our method of use of the equation involves an additional level of calculation than the three first-order regression models that it was measured against. Any errors in calculating r_a are further propagated through calculation of the predictive relationships between r_c and $R_{\rm n}$. The energy-balance approach to predicting ($T_{\rm c}$ -T_a)_{LL} is more theoretically sound than an empirical ap-

proach utilizing least squares regression.

Single-variable models containing VPD as the only independent variable have been the most wide spread type of equations utilized for predicting $(T_c - T_a)_{LL}$ in CWSI calculation. The results of this research concur with those of Horst et al. (1989) and Smith et al. (1986), which indicate that more complex models are necessary for accurate prediction of $(T_c - T_a)_{LL}$ in areas where WS, VPD, and R_n are highly variable. Based on work performed on an independent data set, Smith et al. (1986) found the complete energy-balance approach with r_a and r_c as dynamic components to be more satisfactory in predicting $T_c - T_a$ of nonwater-stressed wheat (Triticum aestivum L. emend. Thell.) than empirical models containing VPD and VPD plus R_n or energy-balance models in which r_c and r_a or only r_a were kept constant at their mean value. We did not find the complete energy-balance model with r_a and r_c dynamic to be more satisfactory than the three-variable linear model involving VPD, $R_{\rm n}$, and WS.

The most powerful model for accurate prediction of $(T_c - T_a)_{LL}$ in this study was the three-variable linear model that used VPD, R_n , and WS. A single model of

this type was satisfactory across five Kentucky bluegrass cultivars. A general model applied across Kentucky bluegrass and creeping bentgrass in this study introduced bias when used on creeping bentgrass, possibly indicating that a separate model was necessary on creeping bentgrass. Work by Horst et al. (1989) suggested that baselines used in an empirical approach to CWSI calculation were likely species × cultural regime × seasonal condition specific. Further testing of the models developed in this study at different locations on various grasses managed under different cultural regimes could provide more information on the limitations of the empirical approach to CWSI calculation on turfgrass.

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